

# **Enhanced Rock Weathering**

Methodology for CO<sub>2</sub> Removal

(Approved pending final copy edits)

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# Enhanced Rock Weathering Methodology for CO<sub>2</sub> Removal

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# **Glossary of Terms**

**REMARK:** This glossary provides only the most important definitions for the current methodology. Please note that further definitions are listed in the Puro Standard General Rules.

**Application site** – a *plot* or a collection of geographically proximate *plots* to which weathering material is applied and that are similar in relevant parameters (see section 11.1) and grouped together for monitoring purposes.

**Base cation** – a positively charged alkali metal or alkaline earth metal ion. For the purposes of this methodology, the base cations are defined as sodium (Na $^+$ ), potassium (K $^+$ ), calcium (Ca $^{2+}$ ), and magnesium (Mg $^{2+}$ ).

**Bicarbonate** – a widely used name for hydrogen carbonate, a polyatomic anion with the chemical formula HCO<sub>3</sub><sup>-</sup>. Bicarbonate can be formed via deprotonation of carbonic acid during weathering.

**Carbonate** – a polyatomic anion with the chemical formula  $CO_3^{2-}$ . The word 'carbonate' can also refer to solid carbonate minerals (See *Solid carbonates*/ *carbonate minerals*), which in this text are consistently referenced as such to distinguish them from the carbonate ions.

**Control site** – a *plot* or a collection of geographically proximate *plots* that are similar in relevant parameters (see section 11.1) and grouped together for monitoring purposes to which no weathering material is applied, but which is otherwise managed and monitored under the same conditions as the *application site*. The control site is used as a reference to assess baseline environmental parameters and isolate the effects of the Enhanced Rock Weathering activity.

CO<sub>2</sub> Removal Supplier – the party authorized to represent the end-to-end supply chain of the enhanced rock weathering activity.

**Deployment Period** – The time interval beginning with an application of weathering material at the Field Site and ending either with the subsequent application of weathering material or with the end of the crediting period. A deployment period may contain one or more monitoring periods used for carbon removal accounting and CORC issuance.

**Eligible activity** – an activity capable of storing carbon dioxide in the form of *carbonate* or *bicarbonate* ions or *solid carbonate minerals* via the application of *weathering material* to one or several *application sites*.

**Enhanced Rock Weathering** – a CO<sub>2</sub> removal method where the application of a *weathering material* to soils results in the storage of carbon dioxide in the form of *carbonate* or *bicarbonate* ions or *solid carbonate minerals*.

**Evaluation Area** – the subset of the *application site* area that is being monitored for C<sub>stored</sub> quantification and validation more densely than the rest of the *application site*.

**Feedstock** – see *Weathering material*.

**Field site** – a field site comprises all the land areas registered under a single Production Facility (i.e., all application sites, control sites, and reserve sites).

**Homogeneous stratum** – a defined area within the Field site that exhibits uniform characteristics relevant to ERW implementation and monitoring as further defined in this methodology.

**Model (process-based)** – process-based models for ERW can be described as a set of functions implemented in computer software that represent biogeochemical processes and that are utilized to make a prediction related to the weathering reactions and the associated carbon dioxide removal depending on a certain number of input parameters. Beyond that, this methodology uses the word model in a wider sense that includes also the subsequent data analysis and interpretation of the results by experts. Process-based models are distinguished from statistical models (e.g., linear regressions, Bayesian models).

**Plot** – a contiguous piece of land (i.e., land that is either connected or separated only by a public or private roadway, waterway, easement, or other right of way) of predetermined area, boundaries, and geographic location. Often, an individual field used for growing agricultural crops.

**Potentially toxic elements (PTEs)** – any substances that are or can reasonably be thought to be present in the weathering material in concentrations high enough to be harmful to living organisms, including plants, animals, and humans. PTEs relevant to this methodology include but are not limited to heavy metals, asbestiform minerals, and radioactive minerals.

**Production facility** – the ensemble of physical assets, infrastructure, and operational processes necessary to perform the end-to-end activities associated with an Enhanced Rock Weathering activity, and subject to the Production Facility Audit as per the terminology defined in the Puro Standard General Rules. See section 2.2 for a detailed description.

**Simulation** – an enhanced rock weathering *model* or the prediction produced by the *model*. See *Model*.

 $t_0$  - the first sampling time point at the beginning of a monitoring period. Depending on the quantification approach, this can occur just before or just after feedstock application.

<sup>&</sup>lt;sup>1</sup> Available in the Puro Standard document library.

 $t_1$  - the final sampling time point at the end of a monitoring period. There is no limit on sampling time points between  $t_0$  and  $t_1$ .

**Tonne (t)** – A unit of mass equivalent to 1000 kg, also known as 'metric tonne'. In this methodology, the word 'tonne' always refers to metric tonnes.

**Solid carbonates/ carbonate minerals** – solid compounds composed primarily of carbonate ions  $(CO_3^{2-})$  and divalent cations such as  $Ca^{2+}$  (as in calcium carbonate,  $CaCO_3$ ) and/or  $Mg^{2+}$  (as in magnesium carbonate,  $MgCO_3$ ).

**Weathering material** – the material being spread to an *application site*, capable of facilitating carbon dioxide storage in the form of *carbonate* or *bicarbonate* ions or *solid carbonate minerals* via chemical reactions. The weathering material can consist of rocks or other suitable materials such as alkaline waste products (e.g. slag or cement kiln dust). Used interchangeably with *Feedstock*.

**Weathering signal** – an empirical measurement (such as the depletion of weathering reagents or the accumulation of reaction products in time) that serves as a direct or proxy indicator of active mineral weathering processes in soils. Reliable sequestration quantification approaches often rely on quantitative and qualitative weathering signals measured over a period of time.

# **Acronyms**

AAS - Atomic Absorption Spectroscopy

CDR - Carbon Dioxide Removal

**CEC** – cation exchange capacity

CORC - CO<sub>2</sub> Removal Certificate

DIC - Dissolved Inorganic Carbon

**DIW** – Deionized Water

**DP** – Deployment Period

ERA – Environmental Risk Assessment

ERW - Enhanced Rock Weathering

FFZ – Far-field zone

**GHG** – Greenhouse gas

ICP-MS – Inductively Coupled Plasma Mass Spectrometry

ICP-OES – Inductively Coupled Plasma Optical Emission Spectrometry

IPCC - Intergovernmental Panel on Climate Change

LCA – Life Cycle Assessment

MP - Monitoring Period

NFZ - Near-field zone

PTE – Potentially Toxic Element

RMSE – Root Mean Square Error

SIC – Soil Inorganic Carbon

**SOC** – Soil Organic Carbon

**TA** – Total Alkalinity

tCO2e – tonnes of CO2 equivalents

XRD - X-ray diffraction

# **Chemical species**

Ca<sup>2+</sup> – Calcium cation

CaCO<sub>3</sub> – Calcium carbonate

CH<sub>4</sub> - Methane

Cl-- Chloride ion

CO<sub>2</sub> – Carbon dioxide

CO<sub>3</sub><sup>2-</sup> – Carbonate ion

H<sub>2</sub>CO<sub>3</sub> - Carbonic acid

HF - Hydrofluoric acid

H<sub>2</sub>O - Water

H<sub>2</sub>SO<sub>4</sub> - Sulfuric acid

HCO₃⁻ – Hydrogen carbonate, also known as bicarbonate

HNO3 - Nitric acid

K⁺ – Potassium cation

Mg<sup>2+</sup> – Magnesium cation

N<sub>2</sub>O – Dinitrogen monoxide, also known as nitrous oxide

Na+ – Sodium cation

NO<sub>3</sub>- – Nitrate

PO<sub>4</sub>3- - Phosphate

SO<sub>2</sub> – Sulfur dioxide

SO<sub>4</sub><sup>2-</sup> - Sulfate

SO<sub>x</sub> – Sulfur oxides in general

# **Minerals**

**Anorthite** – CaAl<sub>2</sub>Si<sub>2</sub>O<sub>8</sub> (calcium aluminosilicate feldspar)

**Albite** – NaAlSi<sub>3</sub>O<sub>8</sub> (sodium aluminosilicate feldspar)

**Kaolinite** – Al<sub>2</sub>Si<sub>2</sub>O<sub>5</sub>(OH)<sub>4</sub> (aluminum silicate hydroxide clay)

Wollastonite – CaSiO<sub>3</sub> (calcium metasilicate)

Calcite – CaCO<sub>3</sub> (calcium carbonate)

Olivine – (Mg,Fe)<sub>2</sub>SiO<sub>4</sub> (magnesium iron silicate)

# Note to the reader

**REMARK:** This methodology provides general information as well as actual requirements that must be met by all projects seeking certification under the Puro Standard. Across the entire methodology, the requirements correspond to numbered rules with formatting conforming to the example below.

0.0.1 This is an example of a numbered rule. The requirements set within numbered rules must be followed by all projects seeking certification under the Puro Standard.

Please note that in addition to the requirements of this methodology document, all projects seeking certification under the Puro Standard must also comply with the Puro Standard General Rules and other Standard Requirements, as well as any applicable local laws, regulations, and other binding obligations.

For Puro Standard documents, see the Puro Standard documents library.

# 1 Introduction

### 1.1 Overview and scope

This methodology sets the requirements for eligibility and quantification of net  $CO_2$  removal achieved through the enhancement of natural chemical weathering processes in soil. By applying eligible weathering materials to terrestrial environments, atmospheric  $CO_2$  is safely sequestered as carbonate minerals in soil or the dissolved inorganic carbon (DIC) species bicarbonate ( $HCO_3$ ) and carbonate ( $CO_3$ ) in the ocean, where the carbon is safe from re-emission to the atmosphere with oceanic residence times of ~10<sup>5</sup> years (Lord et al., 2016; Renforth & Henderson, 2017). These timescales support the claim that ERW can achieve permanence exceeding 1000 years.

In this methodology, Enhanced Rock Weathering (ERW) refers to the overall process of applying finely ground weathering material (e.g., natural silicate- or carbonate-rich rocks or artificial materials such as slags, mine tailings or other alkaline industrial waste materials) to land surfaces such as croplands, grasslands, or other suitable terrestrial environments, for the purpose of durable CO<sub>2</sub> removal.

In broad terms, the scope of this methodology includes the following fundamental components: sourcing, processing, transportation, and application of eligible weathering material, monitoring of weathering rates and CO<sub>2</sub> removal, and verification of long-term carbon sequestration (see also figure 7.1).

# 1.2 Mechanism for CO<sub>2</sub> Sequestration

#### Natural and enhanced weathering

Rock weathering is a natural process estimated to sequester ~1 Gt of atmospheric CO<sub>2</sub> per year (Ciais et al., 2013; Strefler et al., 2018). In the weathering process, atmospheric CO<sub>2</sub> dissolves in water (e.g. rain droplets or river water), forming carbonic acid (H<sub>2</sub>CO<sub>3</sub>), see eq. 1.1. This weak acid reacts with alkaline minerals in silicate and carbonate rocks, generating stable bicarbonate (HCO<sub>3</sub>-) and carbonate (CO<sub>3</sub><sup>2</sup>-) ions from the carbonic acid while releasing base cations (Ca<sup>2+</sup>, Mg<sup>2+</sup>, Na<sup>+</sup>, K<sup>+</sup>) from the mineral. The resulting dissolved inorganic carbon (DIC) species either precipitate as minerals in the soil or are transported via rivers to the ocean, where they may remain in solution over time scales of millennia (Hartmann et al., 2013; Lord et al., 2016). In ERW, the natural weathering process is accelerated by spreading finely ground rocks or other suitable feedstock materials onto soils (for further details, see section 1.4).

#### Weathering reactions

When atmospheric  $CO_2$  dissolves in water, it first undergoes a sequence of reactions that begins with its hydration to form carbonic acid ( $H_2CO_3$ ). Carbonic acid then dissociates into bicarbonate ( $HCO_3^-$ ) and carbonate ( $HCO_3^-$ ) ions, releasing protons ( $H^+$ ) in the process, see eq. 1.1. This reaction lowers the pH and enables further interaction with alkaline minerals.

$$CO_{2 (aq)} + H_{2}O_{(1)} \iff H_{2}CO_{3 (aq)} \iff H^{+}_{(aq)} + HCO_{3 (aq)} \iff 2H^{+}_{(aq)} + CO_{3 (aq)}$$
 (1.1)

Rock weathering occurs when carbonic acid, formed from dissolved CO<sub>2</sub>, reacts with minerals such as calcium or magnesium silicates. This process releases base cations (Ca<sup>2+</sup>, Mg<sup>2+</sup>, Na<sup>+</sup>, K<sup>+</sup>) and forms bicarbonate ions, increasing the total alkalinity of the system. The reaction follows the general pattern:

mineral + aqueous 
$$CO_2 \rightarrow$$
 cations + bicarbonate + secondary silicates/clays (1.2)

For example, the weathering of the calcium-rich feldspar anorthite (CaAl<sub>2</sub>Si<sub>2</sub>O<sub>8</sub>) proceeds as follows:

$$CaAl_2Si_2O_8 (s) + 2 CO_2 (aq) + 3 H_2O (l) \rightarrow Ca^{2+} (aq) + 2 HCO_3^{-} (aq) + Al_2Si_2O_5(OH)_4 (s)$$
 (1.3)

In this reaction, the release of one mole of Ca<sup>2+</sup> is accompanied by the formation of two moles of bicarbonate, each contributing one equivalent of alkalinity.<sup>2</sup> If the CO<sub>2</sub> involved originates from the atmosphere, this results in the net removal of two moles of atmospheric CO<sub>2</sub> per mole of Ca<sup>2+</sup> released. The reactions for CO<sub>2</sub> hydration/dissociation and mineral dissolution occur in parallel, together defining the weathering process.

It is important to recognize that the net carbon removal resulting from the weathering reactions depends on the type of mineral weathered. For instance, the dissolution of calcite results in only *one* mole of atmospheric CO<sub>2</sub> removed per mole of Ca<sup>2+</sup> released and mole of CaCO<sub>3</sub> dissolved (compared to the *two* moles of CO<sub>2</sub> in the anorthite example above in eq. 1.3), thus making calcite weathering 50% less efficient than silicate-mineral weathering in terms of net CO<sub>2</sub> sequestration per mole of Ca<sup>2+</sup> released:

$$CaCO_{3 (s)} + CO_{2 (aq)} + H_{2}O_{(l)} \rightarrow Ca^{2+}_{(aq)} + 2 HCO_{3}^{-}_{(aq)}$$
 (1.4)

However, note that in addition to this stoichiometric CO<sub>2</sub> sequestration potential, the overall suitability of a particular feedstock for ERW depends on several other factors as well, such as the reaction rate and environmental safety of the material (see section 4.5). For example, the dissolution rate of calcite is orders of magnitude faster compared to that of anorthite (White et al., 1999).

# 1.3 Storage of sequestered carbon

#### Fate of the weathering products and storage permanence

As summarized above (see eq. 1.2 and associated text), the weathering process releases base cations, bicarbonate and secondary minerals into the soil system. The durable storage of atmospheric CO<sub>2</sub> comes from two primary pathways. One pathway involves the precipitation of solid carbonate minerals, particularly pedogenic carbonates formed within the soil matrix (see equation 1.5). Pedogenic carbonate formation and dissolution are influenced by site-specific environmental factors

 $<sup>^2</sup>$  Note that under certain conditions such as high pH, elevated concentrations of Ca<sup>2+</sup> and HCO<sub>3</sub><sup>-</sup>, and limited water movement, calcium and bicarbonate can react to form solid calcium carbonate (CaCO<sub>3</sub>), a process known as secondary carbonate formation. This may reduce the net CO<sub>2</sub> removal if the associated CO<sub>2</sub> is re-released during precipitation.

such as soil pH, moisture, mineral saturation states, and biological activity. Once formed in a suitable environment, however, the permanence of carbonated minerals in general and soil carbonates in particular is on the order of millennia or more (Dungait et al., 2018; Metz et al., 2005; Schlesinger, 1985). Pedogenic carbonate formation is by far the less common pathway in ERW and is only feasible and quantitatively viable under certain soil conditions (see below).

The second and main ERW pathway involves the storage of carbon in dissolved ionic form, with bicarbonate being the dominant and most stable form under typical environmental conditions. In the ocean (as well as in other aquatic systems like groundwater), bicarbonate can persist for millennia (Hartmann et al., 2013; Lord et al., 2016).

The trajectory of the ERW dissolution products (bicarbonate and associated cations) towards their ocean storage site begins once they are released into soil pore water and begin moving through the terrestrial environment. Along the way, the transport of these products can be slowed or temporarily interrupted as base cations may be taken up by plants, adsorbed onto cation exchange sites on soil particles or organic matter, or incorporated into secondary minerals (see section 1.6). Over time, the dissolved ERW products undergo leaching (i.e., are carried downward through the soil profile by soil water) and enter the groundwater from where they may be transported via streams and rivers to the ocean (Gastmans et al., 2016).

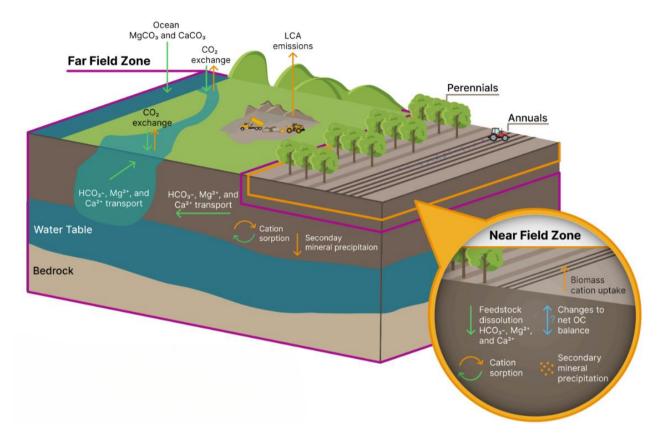
Beyond their role in carbon storage, dissolution products also provide practical means of tracking and quantifying ERW. The concentrations of base cations (e.g., Ca<sup>2+</sup>, Mg<sup>2+</sup>, Na<sup>+</sup>, K<sup>+</sup>), DIC or alkalinity can serve as proxies for the extent and rate of mineral weathering. Because these solutes are conserved during transport, their presence and ratios in soil solutions, river chemistry, and receiving water bodies provide measurable indicators of both weathering progress and the fate of sequestered carbon (Mills et al., 2024).

#### **Near-Field and Far-Field Zones**

This methodology adopts the convention of conceptually dividing the spatial domain of ERW into two non-overlapping spatial zones: the **near-field zone (NFZ)** and the **far-field zone (FFZ)** (Mills et al., 2024). The NFZ corresponds to the upper soil layer where the enhanced weathering of rock feedstocks is empirically quantified (see figure 1.1). The FFZ includes deeper soil layers, groundwater, rivers, and the ocean.

Conceptually, the NFZ depth is the point below which captured CO<sub>2</sub> is safe from re-emission to the atmosphere, i.e., the depth where even diffusive exchange between atmospheric and soil-based CO<sub>2</sub> becomes negligible (Mills et al., 2024). In practice, however, this strict definition is unworkable because CO<sub>2</sub> exchange depends on spatially heterogeneous and temporally dynamic multiphase processes that cannot be generalized and can extend one or more meters below the surface. Therefore, this methodology defines the operational NFZ depth pragmatically and encompasses the portion of the soil profile where the CO<sub>2</sub> Removal Supplier must monitor and measure the enhanced weathering reaction (see section 11.2: sampling depth) to quantify C<sub>stored</sub>, C<sub>baseline-[field]</sub>, and C<sub>loss</sub> (eq. 5.1). Loss pathways from the NFZ include non-carbonic acid weathering, plant uptake of major

cations, cation adsorption to soil particles, secondary carbonate mineral formation, and secondary silicate mineral formation (section 1.6, section 6.2), whereas loss pathways occurring in the FFZ include those associated with carbonate system re-equilibration and carbonate mineral precipitation in surface freshwater or marine systems.



**Figure 1.1**. Diagram adapted from Mills et al. (2024) showing the Near-Field Zone (orange frame), where feedstock weathering occurs and fluxes of weathering products are measured, and the Far-Field Zone (purple frame), where weathering products move toward long-term storage. Green arrows show the fluxes of weathering products generated from ERW. Orange arrows indicate loss pathways and emissions. Blue arrow indicates changes to the net organic carbon due to the variable responses of SOC to alkaline feedstock addition.

#### Secondary (pedogenic) carbonate mineral formation

Under certain soil conditions such as carbonate oversaturation, high pH, and low soil moisture, carbonate minerals, especially calcium carbonates, may precipitate in the soil. In the ERW context, these pedogenic (formed within the soil matrix) carbonates are typically referred to as *secondary carbonates* if they are produced as a result of silicate weathering and are not simply present in the added rock. Increasing soil alkalinity caused by ERW may promote pedogenic carbonate precipitation (Kantzas et al., 2022). Secondary carbonate formation has been observed in several potbased trials and field studies on ERW (Haque et al., 2020; Manning et al., 2013) and can be described by the following general formulation:

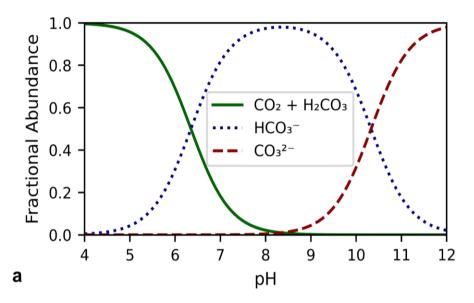
$$Ca^{2+}(aq) + 2 HCO_{3-}(aq) \longrightarrow CaCO_{3}(s) + CO_{2}(aq) + H_{2}O_{(1)}$$
 (1.5)

This reaction results in the release of one mole of CO<sub>2</sub> for every mole of calcium carbonate precipitated, thereby reducing the net carbon capture from silicate-rich feedstock weathering and erasing any previous carbon capture from carbonate mineral dissolution. This "lost" CO<sub>2</sub> could potentially be re-captured if the precipitated CaCO<sub>3</sub> undergoes carbonic acid weathering. Alternatively, if the CaCO<sub>3</sub> dissolves via non-carbonic acid pathways, both moles of sequestered CO<sub>2</sub> could eventually be emitted back to the atmosphere (Hamilton et al., 2007).

Carbonate mineral formation in soils can be measured using methods for quantifying soil inorganic carbon (SIC), including calcimetry and thermogravimetric analysis, as well as using stable and radioactive isotope techniques to determine the source and age of the carbonate minerals, respectively (see section 11.2).

#### Aqueous phase composition and the role of pH in ERW

The role of pH in ERW is complex (Haque et al., 2023). At the near-neutral pH typical of rivers (pH ~7), most dissolved inorganic carbon (DIC) exists in the form of bicarbonate (see figure 1.2). While the optimal pH varies by mineral type, silicate weathering rates generally increase at lower pH. However, low pH (<6) shifts DIC speciation toward CO<sub>2</sub>, which undermines the goal of ERW of storing carbon as bicarbonate. A Bjerrum plot (figure 1.2) illustrates the carbonate speciation as a function of pH in soil porewater. At low pH (about pH < 6.3), most DIC is in the form of CO<sub>2</sub>, whereas at near-neutral pH (pH 7-9, typical of river water) it is HCO<sub>3</sub>- which dominates, and at higher pH, the CO<sub>3</sub><sup>2-</sup> ion gains importance. However, at high pCO<sub>2</sub> and high DIC, even mildly acidic to neutral pH (~5.5-7.5) can lead to CO<sub>2</sub> oversaturation. Oversaturation can lead to CO<sub>2</sub> degassing when the partial pressure of CO<sub>2</sub> (pCO<sub>2</sub>) in pore water is higher than in the surrounding pore air. If the soil column is sufficiently permeable, this CO<sub>2</sub> can escape to the atmosphere and (partially) negate any CDR efforts. However, once the dissolved weathering products (e.g., Ca<sup>2+</sup>) are transported to surface waters, which generally have a higher pH than soil porewater, some of the CO<sub>2</sub> that degassed earlier can be reabsorbed and converted back to bicarbonate, partly offsetting these losses. It is also important to note that the soil system pH can change with degassing. However, if the buffer capacity of the soil is high, the pH might not change significantly. Factors that increase the soil buffer capacity include the presence of alkaline materials, high cation exchange capacity (CEC) and base saturation, as well as the presence of humic and fulvic acids. Finally, another important aspect of pH is the role of non-carbonic acids, which can weather ERW feedstocks without contributing to CO2 sequestration (section 1.6). For this reason, low-pH soils (pH  $\leq$ 5-6) may not provide suitable settings for effective ERW (Holden et al., 2024).



**Figure 1.2.** The carbonate system and its relationship to pH and alkalinity. **a**: Relative abundance of the carbonate system components across the relevant pH range under standard conditions (Stumm & Morgan, 1996).

## 1.4 Operational principles

#### **Enhanced weathering**

In the context of engineered CO<sub>2</sub> removal, accelerating (or *enhancing*) Earth's natural weathering processes has been proposed for over three decades (Lackner et al., 1995; Seifritz, 1990), and ERW shows significant potential for large-scale CO<sub>2</sub> removal (Beerling et al., 2020, 2025; Goll et al., 2021; Hartmann et al., 2009). Note that while ERW can also be carried out in coastal and aquatic environments (Renforth & Henderson, 2017), this methodology only considers the application of weathering material in terrestrial (land-based) environments, more specifically in soil.<sup>3</sup>

In essence, ERW involves three key components to speed up the natural weathering process (Abdalqadir et al., 2024; Andrews & Taylor, 2019; Clarkson et al., 2024):

1. Suitable material selection: Materials containing significant amounts of minerals with high weathering reactivity and appropriate cation content (especially Ca and Mg, but also Na and K) are preferred. These include, among others, mafic and ultramafic rocks that contain the minerals olivine, plagioclase and pyroxene, and metamorphic rocks that contain wollastonite, which not only react efficiently with CO<sub>2</sub> but may also improve soil fertility<sup>4</sup>

<sup>&</sup>lt;sup>3</sup> In the Puro Standard, weathering in controlled industrial conditions for the production of carbonated materials (also known as "accelerated carbonation") is covered by the Puro Standard methodology Carbonated Materials. Enhanced weathering in coastal areas and ocean alkalinization are currently (October 2025) not covered under the Puro Standard.

<sup>&</sup>lt;sup>4</sup> The primary agronomic benefit of ERW applications is pH management, with a strong body of evidence linking reduced soil acidity to improved crop yields. Other potential benefits, such as nutrient contributions from mineral amendments, remain more speculative at present.

(Haque, Chiang, et al., 2019). Other suitable materials include rocks containing silicate minerals that release alkalis and alkaline earth cations when they weather, as well as alkaline industrial wastes, particularly those containing fast-dissolving, cation-rich minerals (Khudhur et al., 2022; Renforth, 2019). Synthetic minerals for CDR are being explored as well (Chen & Kanan, 2025). The feedstock mineralogy and the cations and anions produced during dissolution significantly affect the amount of CO<sub>2</sub> sequestered (see Suitable feedstocks for ERW and table 1.1).

- 2. **Grinding**: Rock crushing and milling increase the reactive surface area by reducing mineral grain size and introducing surface defects (Fischer et al., 2012; Pedrosa et al., 2019), thereby accelerating dissolution rates and enhancing CO<sub>2</sub> uptake. The ideal grain size for ERW remains uncertain, although some studies suggest diminishing returns below certain particle sizes (Amann et al., 2022). Interestingly, recent findings show that grain size is not always a reliable predictor of surface area, as larger particles (2–10 mm) can exhibit similar specific surface area (SSA) to finer grains due to internal porosity and weathering-induced microstructures (Burke et al., 2025). In practice, optimal size also depends on non-chemical factors such as grinding costs, energy efficiency, and handling challenges or health risks associated with very fine dusts.
- 3. Appropriate application settings: Applying the weathering material to locations with optimal soil and climate conditions promotes the rate of weathering reactions. Such locations include e.g., sub-tropical regions with hot and humid climate, relatively low to moderate pH soils (pH ~5.2-7.2) (Bertagni & Porporato, 2022), and good hydrological drainage (Baek et al., 2023). Additionally, root exudates, fungal hyphae (Thorley et al., 2015; Verbruggen et al., 2021), invertebrates (Van Groenigen et al., 2019; Vicca et al., 2022), and soil microbial activity (Epihov et al., 2017; Perakis & Pett-Ridge, 2019)—including symbiotic Rhizobiaceae in leguminous crops-can enhance mineral dissolution (Haque, Santos, et al., 2019). Agricultural land is commonly targeted for ERW for several reasons, including suitable ambient conditions (presence of water and high CO<sub>2</sub> concentrations in the soil), potential cobenefits to crop yields (see section 1.5), and the routine disturbance of soils in croplands that further facilitates mineral mixing and exposure to water. Selecting appropriate soil conditions can further have a practical impact on the ease and effectiveness of the overall MRV process. For example, sandier soils with lower background levels of base cations can be beneficial for resolving weak weathering signals from soil samples, and similarly areas with well constrained hydrology can facilitate analysis of water samples.

#### Suitable feedstocks for ERW

The most effective feedstock materials for ERW are those that combine high reactivity with high CO<sub>2</sub> sequestration potential. Optimal rock candidates contain silicate minerals characterized by low bond strength and enriched in divalent cations (Mg<sup>2+</sup>, Ca<sup>2+</sup>), each binding two moles of bicarbonate per mole of cation. Such minerals are predominantly found in ultramafic and mafic igneous rocks, but sedimentary rocks could also be of potential interest (Q. Zhang & Tutolo, 2022).

The maximum CO<sub>2</sub> removal capacity (CDR<sub>max</sub>) of a rock sample can be calculated using an adapted **Steinour formula** (Lackner et al., 1995; Renforth, 2019) by XRF, or after sample digestion followed by ICP-OES analysis.

$$CDR_{max} = \frac{M_{CO_2}}{100} \times \left(2\frac{w_{CaO}}{M_{CaO}} - 1\frac{w_{CaCO_3}}{M_{CaCO_3}} + 2\frac{w_{MgO}}{M_{MgO}} + 1\frac{w_{K_2O}}{M_{K_2O}} + 1\frac{w_{Na_2O}}{M_{Na_2O}}\right)$$
(1.6)

Where, M is the molecular weight (g/mol) and w is the oxide mass percentage. The CaCO<sub>3</sub> term of the equation corrects for calcium that is present in the form of carbonates, which implies a CDR potential of 1 mol CO<sub>2</sub> per mol CaCO<sub>3</sub> (eq. 1.4) rather than 2 mol CO<sub>2</sub> per mol CaO. This requires carbon content measurements in feedstock (see table 3.1). The equation above assumes complete carbonation of the oxides. This formula can also be used to estimate the sequestration potential of different minerals in their ideal form (table 1.1) but it is important to note that any ERW feedstock rock will be composed of multiple minerals.

**Table 1.1.** Examples of theoretical maximum potential for CO<sub>2</sub> removal by weathering of different minerals based on their ideal formula and oxide composition. Note that the ideal formula for minerals may differ significantly for any given mineral found in nature and the CDR<sub>max</sub> values listed here only apply to the associated ideal formula and cannot straightforwardly form the basis for CDR<sub>max</sub> calculations.

Group or subgroup	Name	Chemical formula (ideal)	CDR <sub>max</sub> (t <sub>CO2</sub> /t <sub>mineral</sub> )
Olivine	Forsterite	(Mg,Fe) <sub>2</sub> SiO <sub>4</sub>	1.260
Pyroxenoid	Wollastonite	CaSiO <sub>3</sub>	0.759
Clinopyroxene	Diopside	CaMgSi <sub>2</sub> O <sub>6</sub>	0.816
Orthopyroxene	Enstatite	Mg <sub>2</sub> Si <sub>2</sub> O <sub>6</sub>	0.883
Orthopyroxene	Augite (Ca: (Mg,Fe) < 1)	(Ca,Na)(Mg,Fe,Al,Ti)(Si,Al)2O6	0.692
Carbonate	Calcite	CaCO <sub>3</sub>	0.440
	Anorthite (An)	CaAl <sub>2</sub> Si <sub>2</sub> O <sub>8</sub>	0.310
	Albite (Ab)	NaAlSi <sub>3</sub> O <sub>8</sub>	0.176
Plagioclase feldspars	Labradorite	Intermediate composition between An and Ab (50-70% An)	0.259
r lagreelace letaepare	Andesine	Intermediate composition between An and Ab (30-50% An)	0.229
	Oligoclase	Intermediate composition between An and Ab (10-30% An)	0.199
Plagioclase	Nepheline	Na3KAl4Si4O16	0.301
feldspathoids	Leucite	KAlSi <sub>2</sub> O <sub>6</sub>	0.202
Mica	Glauconite	(K,Na)(Fe,Al,Mg)2(Si,Al)4O10(OH)2	0.150

While CDR<sub>max</sub> is useful to estimate the weathering potential of a given rock sample, it says little about the potential rate of weathering. The **Goldich dissolution series** (Goldich, 1938) ranks silicate minerals by stability during weathering. It is inversely related to Bowen's reaction series for igneous crystallization, which shows that minerals crystallizing at higher temperatures (e.g. olivine, calciumrich pyroxenes, plagioclases) are less stable at Earth's surface and thus weather faster. This mineral-inherent susceptibility to weathering is then subject to environmental factors affecting the weathering rate, including temperature, pH, moisture, and CO<sub>2</sub> partial pressure.

## 1.5 Positive and negative aspects of ERW

ERW has strong potential for large-scale CO<sub>2</sub> removal due to the global abundance of suitable rocks, compatibility with existing agricultural practices, and possible co-benefits for soil and plant health (Healey et al., 2024; Swoboda et al., 2022). Its implementation typically does not require land use change (Beerling et al., 2020) and can even make use of industrial by-products such as cement kiln dust or recycled concrete (Khudhur et al., 2022; McDermott et al., 2024). When applied to croplands, ERW may improve soil pH, water retention, plant nutrient availability and regional air quality (Beerling et al., 2025), increase plant resistance to stress (Swoboda et al., 2022) while reducing fertilizer dependence and mitigating acidification in surrounding water bodies (Haque, Chiang, et al., 2019; Hartmann et al., 2013).

Despite its benefits, ERW remains a carbon removal technology with limited large-scale validation. While certain aspects of ERW such as deployment of rock dust and analysis of soil samples in agricultural settings are common practice and technologically advanced, monitoring weathering rates and carbon removal under field conditions remains technically challenging due to spatial and temporal variability and complex environmental dynamics (Mills et al., 2024; Power et al., 2025).

One key problem with ERW is that weathering in soils occurs gradually, often over years or even decades (Kanzaki et al., 2025), and is highly dependent on local conditions such as moisture and temperature—factors which may become more variable under climate change (Baek et al., 2023). Nevertheless, scientific field trials, as well as the development of measurement and modelling techniques have gained momentum in recent years (Cipolla et al., 2022; Dietzen & Rosing, 2023; Hasemer et al., 2024; Kanzaki, Chiaravalloti, et al., 2024; Milliken et al., 2025; Reershemius et al., 2023b; Suhrhoff et al., 2024; Te Pas et al., 2025).

Enhanced rock weathering is also associated with several practical and environmental risks that must be properly addressed. For example, fine grinding of rocks improves reactivity, but the generated dust can pose respiratory hazards, creating a critical trade-off between CDR efficiency and human safety. Some rock types may also release potentially toxic elements such as nickel or chromium during dissolution, and the fate of these elements under different risk exposure pathways is not well characterized for the specific conditions of ERW. Certain feedstocks may further contain other hazardous materials such as asbestiform minerals, or naturally occurring radioactive materials (NORMs), posing additional health and environmental risks that require careful assessment and management. Besides the chemical constituents of the feedstock materials, other risks to soil health

include e.g. the risk of soil compaction due to high application rates (versus lime or fertilizer inputs) during narrow seasonal application.

From the point of view of carbon removal, certain feedstock/soil/climate combinations (e.g. coarse material with low cation content in dry, cold, or alkaline environments) pose the risk of emitting CO<sub>2</sub> in the upstream process of deployment without providing CO<sub>2</sub> removal (F. L. Buckingham et al., 2022). Mining, grinding, and transport are also energy-intensive practices and may produce significant emissions, especially if fossil fuels are used, potentially compromising the net carbon benefit (Strefler et al., 2018).

**Table 1.2.** Positive and negative aspects of Enhanced Rock Weathering

Advantages	Limitations
High permanence	Monitoring and modelling challenges due to spatial and temporal variability
Abundant resources: Suitable rocks and application surfaces are widely available.	Air pollution risks from respirable dust during grinding and spreading
Established rock processing and spreading technology	High energy use and emissions from mining, grinding, and transport
Agricultural co-benefits (improved soil health, nutrient supply, pH, water retention)	Potential toxicity from harmful elements released during dissolution
No land use change required	Potentially slow weathering kinetics depending on several factors (e.g., mineralogy, grain size, precipitation, temperature, soil pH, etc.)
Waste utilization (use of industrial by-products)	

# 1.6 Loss pathways associated with Enhanced Rock Weathering

Loss pathways are chemical or biological processes that can reverse the carbon removal achieved through ERW by converting previously sequestered carbon back into CO<sub>2</sub>. Accounting for these losses is essential, especially in cases where the chosen C<sub>stored</sub> quantification approach (see section 11.2) does not implicitly include them. Failing to do so may result in overestimating CDR due to the inclusion of false positives in the measured signal.

#### Non-carbonic acid weathering

ERW CDR is based on the hydrolysis and dissolution of weathering materials by protons derived from carbonic acid originating from dissolved atmospheric or soil-respired CO<sub>2</sub>. This occurs in chemical competition with similar reactions driven by stronger, non-carbonic acids present in the soil environment, generated from biogeochemical and anthropogenic processes, including:

- Nitric acid (HNO<sub>3</sub>) from nitrification or fertilizer inputs.
- Sulfuric acid (H<sub>2</sub>SO<sub>4</sub>) from sulfide oxidation or acid rain.
- Organic acids from microbial metabolism or root exudates.

These acids can also weather feedstock by release of base cations but without sequestering CO<sub>2</sub> in the process. Under certain measurement schemes, this can create a false weathering signal that must be corrected for rather than interpreted as CDR.<sup>5</sup>

#### Secondary carbonate mineral formation

As detailed in section 1.3, secondary (pedogenic) carbonate formation can both sequester and release CO<sub>2</sub>. This is because this process results in 1 mole of stable carbonate mineral but also 1 mole of CO<sub>2</sub> per 2 moles of bicarbonate (eq. 1.5). Thus, the CO<sub>2</sub> created by this reaction may require correction under some circumstances (see rule 6.3.7). Additionally, it should be noted that carbon loss via secondary carbonate formation below the NFZ is also a possibility below the NFZ.

#### Cation adsorption onto soil particles

The export of cations that were weathered from mineral feedstock in the NFZ can be decreased (temporarily) by cation adsorption onto the surface of soil particles, especially clays, organic matter, or oxides. Such cation adsorption can lead to alkalinity decrease and/or acidity increase in the soil porewater or be neutral in both regards, depending on whether the adsorbing cation replaces a cation of same or different valence or a proton. Acidity increase may imply CO<sub>2</sub> evasion and non-carbonic acid weathering. The adsorption of cations onto soil particles is generally reversible but models suggest that the magnitude is larger in soils with low base cation saturation and high cation exchange capacity (Kanzaki et al., 2025). Due to its reversibility, cation adsorption may be more accurately categorized as a "lag term" for ERW but this document categorizes it as a "loss term" for practical purposes because adsorbed cations represent a loss of alkalinity at any given point in time (e.g., end of monitoring period). Cation adsorption can be quantified using mild extraction methods targeting exchangeable cations.

#### Secondary silicate precipitation

The formation of secondary silicate minerals (especially clays) can support the disequilibrium in the soil solution that drives the weathering of feedstock (Maher et al., 2009). However, secondary silicate minerals can also limit feedstock dissolution by shielding the feedstock from the carbonic-acid weathering agent (Maher et al., 2016; Oelkers et al., 2018) as well as by removing base cations (alkalinity) via sorption, co-precipitation and as part of the of the secondary mineral.

There is currently no reliable, commercially viable way to directly quantify low levels of secondary silicate formation in soils, but quantification approaches for C<sub>stored</sub> that measure the decrease of feedstock cations (CAT<sub>Ti</sub>, CAT<sub>WM</sub>) or pore-water based methods (section 11.2) implicitly account for these losses if samples integrate across the entire depth of the NFZ. However, an additional problem can be caused by the tendency of clay minerals formed in upper soil strata (i.e., within the NFZ) to

<sup>&</sup>lt;sup>5</sup> Note that while non-carbonic acid weathering could theoretically result in CDR further downstream by avoiding the outgassing of biogenic CO<sub>2</sub>, it is conservatively treated as a loss term in this methodology due to the significant spatial and temporal uncertainty associated with the quantification of any such removals.

accumulate lower in the soil column (i.e., potentially below the NFZ) (Maher et al., 2009), implying that monitoring within the NFZ is not enough to account for losses from secondary silicate formation. Pore-water measurements below the NFZ, e.g., via deep lysimeters, may currently be the only viable option to assess losses from secondary silicates by estimating the saturation index of such minerals (Mills et al., 2024).

#### Cation uptake by plants

Plant uptake of base cations (Ca<sup>2+</sup>, Mg<sup>2+</sup>, K<sup>+</sup>, and Na<sup>+</sup>) represents a key loss pathway of alkalinity that competes directly with carbon dioxide removal. When biomass is harvested, the base cations taken up by plants are effectively exported from the near-field weathering zone (NFZ), preventing them from contributing to long-term CDR via bicarbonate or carbonate formation. Accurately accounting for this cation flux is therefore essential for determining net CDR in ERW systems. For measurement schemes that do not inherently account for this loss term, this can be done by quantifying cation content in plant biomass and evaluating excess cation uptake in application sites compared to control sites.

#### Downstream carbon loss in rivers and the ocean

The ocean is the final storage site for CO<sub>2</sub> captured by ERW as bicarbonate or carbonate. However, some of this carbon can be lost during transport through rivers and lakes, or after entering the ocean, primarily via two mechanisms: *carbonate mineral precipitation*, and *carbonate system equilibration*. The extent of these losses depends on local water chemistry.

Carbonate mineral precipitation can result in a 50% loss of previously captured  $CO_2$  (eq. 1.5). This occurs when the saturation index of calcite (SI<sub>calcite</sub>) exceeds a threshold:

$$SI_{calcite} = \frac{log_{10}([Ca^{2+}]_a \times [CO_3^{2-}]_a)}{K_{sp}}$$
(1.7)

Where  $[Ca^{2+}]a$  and  $[CO_3^{2-}]a$  are the calcium and carbonate ion activities, respectively, and  $K_{sp}$  is the solubility constant of calcite. The value of  $SI_{calcite}$  increases with higher temperature, higher concentrations of carbonate and calcium, and higher pH. While precipitation theoretically begins at  $SI_{calcite} > 0.0$ , in practice it typically occurs at  $SI_{calcite} > 1.0$ , which is uncommon in most rivers (Harrington et al., 2023; S. Zhang et al., 2025).

Carbonate system equilibration refers to shifts in dissolved inorganic carbon (DIC) speciation due to changes in temperature, salinity, and especially pH (see figure 1.2). In freshwater systems, lower pH can cause degassing of  $CO_2$ , while downstream increases in pH may reverse this and promote resequestration. In the ocean, high pH and salinity favor carbonate ions over bicarbonate, slightly reducing  $CO_2$  uptake efficiency. This is because one mole of  $Ca^{2+}$  or  $Mg^{2+}$  can balance two moles of  $HCO_3^-$  but only one mole of  $CO_3^{2-}$ . Renforth & Henderson (2017) provide an equation to estimate the efficiency of carbon binding (C, in mol) per mole-equivalent of alkalinity (A) as a function of p $CO_2$  (µatm), temperature (T,  $^{\circ}C$ ), and salinity (S, in  $^{\circ}$ ):

$$\frac{{}^{\underline{A}\underline{C}}}{{}^{\underline{A}\underline{A}}} = (S \times 10^{-3.009} + 10^{-1.519}) \ln(pCO_2) - (S \times 10^{-2.100}) - (T \times pCO_2) (S \times 10^{-7.501} - 10^{-5.598}) \\ - (T \times 10^{-2.337}) + 10^{-0.102} \tag{1.8}$$

It is relevant to note that the ocean carbonate system is more complex than suggested by this equation, as vertical and horizontal mixing and advection impact gas exchange between water parcels and the atmosphere (Zhou et al., 2025). Consequently the retention of DIC in the ocean may be far greater than predicted under this (Kanzaki et al., 2023). As CO<sub>2</sub> is more soluble in colder water and bicarbonate dominates at lower salinity, ERW is more effective in cooler, fresher high-latitude oceans (Bertagni & Porporato, 2022).

Loss of excess carbon from rivers downstream of ERW application sites has been assessed using models (Harrington et al., 2023; S. Zhang et al., 2025). Zhang et al. (2025) assumed that 10% of weathering products from a 10 t ha⁻¹ yr⁻¹ application rate enter rivers, estimating ≤5% loss from degassing and precipitation. In contrast, Harrington et al. modeled scenarios with 100% of weathering products entering rivers at 10–50 t ha⁻¹ yr⁻¹, thus representing a high-end case. Surface water chemistry (DIC and organic matter concentration, pH) in the local watershed affects the risk of this loss factor and special care needs to be taken in quantifying it for projects situated in more sensitive catchments.

In the ocean, abiotic carbonate mineral formation is inhibited by the chemistry of seawater (Bialik et al., 2022). Instead, most marine carbonates are formed by shell-forming algae and the majority of these biotic carbonates re-dissolve into seawater (Renforth & Henderson, 2017). However, more research is needed to ensure that marine carbonate formation is indeed a negligible loss term for ERW and not significantly enhanced above baseline levels by additional alkalinity. While earlier modeling studies reported larger estimates for the total ocean loss term (carbonate system equilibration + carbonate mineral formation), a more detailed recent study estimated approximately 9% ocean loss for ERW with silicate mineral feedstock and 19% ocean loss for ERW with carbonate mineral feedstock (Kanzaki et al., 2023).

<sup>&</sup>lt;sup>6</sup> Note that whereas most of the CaCO<sub>3</sub> production in the ocean is biogenic, abiotic CaCO<sub>3</sub> production (so-called "whitening events") has been observed in certain localities, such as the Bahamas or the Persian Gulf, characterized by warming of surface waters combined with prolonged stratification resulting in significant mineral oversaturation (Bialik et al., 2022).

**Table 1.3**: Summary of loss pathways in ERW

Loss Pathway	Mechanism	Impact on CO₂ Removal	Quantification Considerations
Non-Carbonic Acid Weathering	Mineral dissolution by strong acids (e.g., HNO <sub>3</sub> , H <sub>2</sub> SO <sub>4</sub> , organic acids)	Consumes feedstock without CO <sub>2</sub> uptake, warranting correction of false CDR signal under some circumstances	Quantification by soil-carbonate system modeling or soil anion flux measurements and estimations
Secondary Carbonate Formation	Precipitation of pedogenic carbonates from bicarbonate	Releases 1 mol CO <sub>2</sub> per 2 mol HCO <sub>3</sub> <sup>-</sup> ; partial reversal of silicate-feedstock based ERW	Quantification by SIC measurements if monitoring does not cover full NFZ depth
Cation Adsorption	Base cations adsorb to soil particles after weathering	Delays alkalinity export; may release protons and promote CO <sub>2</sub> evasion	Quantified via exchangeable cation extraction; varies with soil CEC and saturation
Secondary Silicate Precipitation	Formation of clays or other silicates incorporating base cations	Reverses weathering and inhibits vertical export of alkalinity	No feasible quantification method but many C <sub>stored</sub> quantification schemes inherently correct for it in NFZ; may also occur below NFZ
Plant Cation Uptake	Plants absorb base cations and release protons	Reverses bicarbonate formation; exported cations reduce long-term CDR	Quantifiable by plant biomass cation content compared between application and control sites.
Riverine Carbon Loss	CO <sub>2</sub> degassing or carbonate precipitation in rivers and lakes	Up to 5% loss under many conditions; higher in high-input cases	Assessed and potentially modeled based on river chemistry data
Oceanic Carbon Loss	Carbonate system equilibration and biogenic carbonate formation	Estimated loss of ~9% (silicates) or ~19% (carbonates)	Modeled using ocean chemistry data; biogenic carbonate formation needs further study

#### 1.7 Counterfactuals

In the context of this methodology, counterfactuals refer to what would have happened to  $CO_2$  fluxes and environmental processes in the absence of the ERW intervention. Establishing accurate counterfactual scenarios is essential to quantify the net carbon removal attributable to ERW, by comparing observed outcomes against realistic baseline conditions without ERW deployment (see section 6.2 and section 11.1).

#### **Agricultural liming**

Applying ground limestone (a rock type containing mostly calcium carbonate) to fields is a common agricultural practice worldwide. It has the purpose of raising soil pH, which can result in a variety of benefits (e.g., decreased metal toxicity, increased nutrient availability). Despite the prevalence of liming, it is not necessarily true that liming should be considered as the counterfactual baseline, because liming can be prohibitively expensive in some farming systems, locales, and years.

From a carbon accounting perspective, agricultural liming has been categorized as a net carbon source to the atmosphere by the IPCC<sup>7</sup>, because the fossil carbon in limestone is a stable form that is brought into a reactive form and setting. At low soil pH, the limestone can be dissolved via reaction

<sup>&</sup>lt;sup>7</sup> 2006 IPCC Guidelines for National Greenhouse Gas Inventories, and 2019 Refinement to the 2006 IPCC Guidelines for National Greenhouse Gas Inventories.

with non-carbonic acids, which would release the carbonate from the limestone as CO<sub>2</sub>. However, if dissolution occurs via carbonic acid weathering, the reaction depicted in eq. 1.4 applies, resulting in the sequestration of 1 mol of CO<sub>2</sub> per mole of calcium carbonate dissolved. Thus, the carbon budget implications of agricultural liming are highly context-specific (Hamilton et al., 2007).

#### **Reduced fertilizer application**

ERW interventions can improve soil pH, nutrient availability, and cation exchange capacity, potentially reducing the need for synthetic fertilizer inputs. Such reductions could, in principle, lead to lower upstream CO<sub>2</sub> emissions from fertilizer production and decreased N<sub>2</sub>O emissions from fertilizer use.

However, the current consensus is that reductions in non- $CO_2$  greenhouse gas emissions, such as  $N_2O$  or  $CH_4$ , should not be included in the net CDR calculation of ERW projects (Mills et al., 2024). While these emission reductions are important for understanding the overall greenhouse gas balance and should be quantified and tracked as part of holistic environmental accounting, they are not considered part of the  $CO_2$  removal to be credited within the scope of this methodology.

#### Counterfactual feedstock weathering

Another relevant counterfactual is the natural weathering of the feedstock material under the scenario in which it was not used for ERW. For example, had the feedstock material not been used for ERW but weathered in its original quarry, waste pile, or natural outcrop, some CO<sub>2</sub> removal by weathering may have occurred anyway.

# 2 Point of creation of the CO<sub>2</sub> Removal Certificate (CORC)

# 2.1 The CO<sub>2</sub> Removal Supplier

- 2.1.1 The CO<sub>2</sub> Removal Supplier is the party authorized to represent the participants necessary to perform the end-to-end activities associated with an Enhanced Rock Weathering activity seeking certification under this methodology (see also section 3.3). Examples of entities which could be identified as the CO<sub>2</sub> Removal Supplier include but are not limited to the following:
  - The operator of the weathering material deployment system.
  - The owner of the weathering material deployment system.
  - The owner of the stored CO<sub>2</sub>.

In particular, the CO<sub>2</sub> Removal Supplier does not need to be the operator of the process creating the CO<sub>2</sub> to be stored (e.g. operating the deployment of the weathering material).

- 2.1.2 The CO<sub>2</sub> Removal Supplier shall be responsible for making end-to-end data available and accessible for 3<sup>rd</sup> party verification. This includes delivering data needed to assess the eligibility of the activity, as well as monitoring and quantifying the net carbon removal. To this extent, the CO<sub>2</sub> Removal Supplier shall establish clear responsibilities and liabilities with its supply-chain partners, external operators, or any other involved party, to enable collection of the necessary data for verification.
- 2.1.3 The CO<sub>2</sub> Removal Supplier shall retain the sole right to claim CORCs from the Enhanced Rock Weathering activity, and contractually agree with any supply chain partners, external operators, or any other involved party that they have no such right. For further details on prevention of double counting, see section 3.5.

# 2.2 Production Facility

The Production Facility is defined as the ensemble of physical assets necessary to perform the endto-end activities associated with an Enhanced Rock Weathering activity, and subject to the Production Facility Audit as per the terminology defined in the Puro Standard General Rules.<sup>8</sup>

- 2.2.1 For the purposes of this methodology, a Production Facility comprises the following components within the activity boundary (see figure 7.1):
  - (a) one or several weathering material sourcing sites;

<sup>&</sup>lt;sup>8</sup> Available in the Puro Standard document library.

- (b) potential additional processing sites or other infrastructure for weathering material processing (such as grinding or comminution);
- (c) a logistics chain for weathering material transportation;
- (d) one or several weathering material application sites;
- (e) one or several control sites (see section 11.1); and
- (f) the weathering material itself.
- 2.2.2 All industrial facilities (i.e. weathering material sourcing and processing sites) under the same Production Facility shall be operational at the time of the Production Facility Audit.
- 2.2.3 The CO<sub>2</sub> Removal Supplier may update the Production Facility definition (see rule 2.2.1) without having to undergo a new Facility Audit provided that such changes are in compliance with the requirements set in this methodology and the Puro Standard, and validated by the auditor during the subsequent Production Facility Audit or Output Audit.
- 2.2.4 Any change in the definition (i.e., components, borders, feedstock sourcing, etc.) of the Production Facility (see rule 2.2.1) requested by the CO<sub>2</sub> Removal Supplier during the Crediting Period will require an update of the Production Facility definition (see rule 2.2.3). These updates shall require validation by the auditor during the subsequent Production Facility Audit or Output Audit.
- 2.2.5 A Production Facility and the associated activity shall be determined as eligible for issuance of CO<sub>2</sub> Removal Certificates (CORCs) once the Production Facility has successfully undergone a third-party verification by a duly appointed Auditor performing a Production Facility Audit.
  - (a) The Production Facility Auditor verifies the conformity of the Production Facility against the requirements of this methodology and other Puro Standard requirements, as well as the proofs and evidence needed from the CO<sub>2</sub> Removal Supplier.
  - (b) The Production Facility Auditor collects and checks the standing data of the CO<sub>2</sub> Removal Supplier and the Production Facility, which includes:
    - (i) a certified trade registry extract or similar official document stating that the CO<sub>2</sub> Removal Supplier's organization legitimately exists;
    - (ii) documentation evidencing that the CO<sub>2</sub> Removal Supplier has registered the Production Facility in the Puro Registry;
    - (iii)locations of the weathering material sourcing sites and weathering material application sites and control sites included in the Production Facility;

- (iv) whether the Production Facility has benefited from public financial support; and
- (v) date on which the Production Facility becomes eligible to issue CORCs.
- 2.2.6 The Crediting Period in this methodology is 10 years starting from the first date of the first Monitoring Period.<sup>9</sup>
  - (a) The Crediting Period may be renewed twice by successfully undergoing a new Production Facility Audit.
  - (b) The Crediting Period shall not overlap with another Crediting Period for the same Production Facility.

#### 2.3 Point of creation

- 2.3.1 The point of creation of the CO<sub>2</sub> Removal Certificates (CORCs) is defined as the earliest point in the CO<sub>2</sub> Removal process when the CORCs can be claimed. For this methodology, the point of creation of the CORC is the moment during the ERW activity when all of the following steps have occurred:
  - 1. the deployed weathering material has chemically reacted to sequester CO<sub>2</sub>, and
  - 2. the weathering proxy (cation or bicarbonate) has either leached out vertically to below the NFZ (for quantification approaches A1-A6, see section 11.2) or formed secondary carbonate minerals (quantification approach A7), and
  - 3. the data records thereof can be verified.
- 2.3.2 The amount of CORCs issued at a given time shall be based on the amount of CO<sub>2</sub> sequestration that *has already occurred* by the time of the Output Audit (i.e., crediting occurs *ex post*).<sup>10</sup>
- 2.3.3 The CO<sub>2</sub> Removal resulting from Enhanced Rock Weathering activities certified under this methodology is considered to be permanent for at least 1000 years.

<sup>&</sup>lt;sup>9</sup> In accordance with the Puro Standard General Rules, the Crediting Period is defined as the period in which verified CO<sub>2</sub> removal Output attributable to a certified Production Facility can result in the issuance of CO<sub>2</sub> Removal Certificates (CORCs), and the Monitoring Period is defined as the time between the first date and last date of the Output Report. For further details and requirements on these periods and the certification process, see the Puro Standard General rules section 2: Certification Process Description (available in the Puro Standard document library).

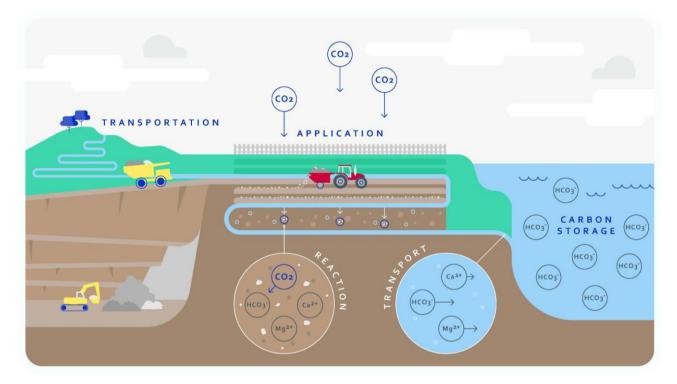
<sup>&</sup>lt;sup>10</sup> The CORCs associated with a given ERW activity are issued gradually over the lifetime of the project, as the deployed weathering material reacts over time to sequester CO<sub>2</sub>. In practice, the speed of the weathering reactions can vary depending on factors such as weathering material composition and soil properties, and it can take several years or even decades for all the deployed weathering material to fully react.

# 3 Eligibility requirements

# 3.1 Overall principles

An eligible activity is capable of permanently sequestering CO<sub>2</sub> of atmospheric or biogenic origin through chemical weathering of mineral feedstocks by safely and durably converting and storing CO<sub>2</sub> as dissolved (bi)carbonate ions or as solid mineral carbonates. In practice, the CO<sub>2</sub> Removal activity consists of spreading weathering materials onto soil (see figure 3.1).

It is important that the requirements for Enhanced Rock Weathering activities ensure durable, robustly quantifiable CO<sub>2</sub> Removal that leads to no net harm<sup>11</sup> to the environment (e.g. contamination by heavy metals), or to society (through e.g. loss of arable land, exposure to hazardous materials or dust, or other health risks).



**Figure 3.1.** A schematic depiction of a CO<sub>2</sub> removal activity within the scope of this methodology.

<sup>&</sup>lt;sup>11</sup> While the ERW activity has significant potential to help mitigate the global effects of climate change, it is paramount that the weathering material sourcing, handling, and spreading activities are conducted in a manner such that the benefits overwhelmingly outweigh the disadvantages.

# 3.2 General eligibility

- 3.2.1 An eligible activity is an activity where eligible feedstock is sourced (see section 3.6) and applied to the soil of eligible application sites (see section 3.9) under conditions that promote CO<sub>2</sub> sequestration as weathering products (primarily in the form of carbonate and bicarbonate aqueous ions), or as reprecipitation of weathering products (primarily as calcium carbonate solids).
- 3.2.2 The CO<sub>2</sub> Removal Supplier shall obtain all permits and other local legal authorizations required to conduct weathering material application activities before the start of application.
- 3.2.3 All installations and operations relating to the Enhanced Rock Weathering activity shall comply with all applicable laws, regulations and other statutory requirements, including but not limited to environmental regulations, and regulations for weathering material processing and handling.
- 3.2.4 All infrastructure and equipment used for weathering material sourcing, processing, transport, and application shall be constructed or installed according to national best practices and in compliance with statutory requirements. All infrastructure shall be approved by local authorities and hold relevant permits for operation. Examples of such installations and equipment include weathering material warehouses and processing facilities (e.g. for screening and grinding).
- 3.2.5 The CO<sub>2</sub> Removal Supplier may utilize shared infrastructure for weathering material sourcing, transport, processing, or deployment. Shared infrastructure may be utilized even if such infrastructure is also utilized for non-eligible activities.
- 3.2.6 The CO<sub>2</sub> Removal Supplier shall provide proof of having the rights necessary to enable appropriate monitoring at any stage within the activity boundary and monitoring period during the lifetime of the Production Facility.
- 3.2.7 The CO<sub>2</sub> Removal Supplier shall demonstrate the baseline carbon removal scenario for their intended Enhanced Rock Weathering approach (see section 6.2).<sup>12</sup>

# 3.3 The CO<sub>2</sub> Removal Supplier

The activities associated with a particular Enhanced Rock Weathering activity can involve multiple site operators collaborating within the project boundary. While the CO<sub>2</sub> Removal Supplier can act as the weathering material sourcing operator, logistics operator and the deployment operator, the responsibility of these operations may also be transferred to external operators (see rule 3.3.2) by contractual agreements.

<sup>&</sup>lt;sup>12</sup> The *baseline* is a conservative scenario of what likely would have happened to the sourced material(s) and the application site(s) without the Enhanced Rock Weathering activity.

- 3.3.1 The CO<sub>2</sub> Removal Supplier shall provide a certified trade registry extract or similar official document stating that it is validly existing and in compliance with the legislation of the host jurisdiction.
- 3.3.2 The CO<sub>2</sub> Removal Supplier must clearly establish and demonstrate ownership of the CO<sub>2</sub> removal activity, either by providing proof of direct ownership or, where applicable, through contractual agreements with external operators.
  - (a) The CO<sub>2</sub> Removal Supplier shall prove with contracts or authorization documents its sole ownership of the durably stored carbon.
  - (b) An external operator refers to any party—such as a logistics provider or the operator of the weathering material sourcing or deployment system—who acts on behalf of and under the direction of the CO₂ Removal Supplier to deliver services related to the Enhanced Rock Weathering activity.
- 3.3.3 When any part of the Enhanced Rock Weathering activity is contracted to an external operator, the CO<sub>2</sub> Removal Supplier shall establish a clear division of responsibilities and liabilities between the CO<sub>2</sub> Removal Supplier and the external operator, which shall—to the applicable extent—at least address:
  - (a) Conducting the required monitoring activities such as sampling, set-up of measurement tools, maintenance, and the monitoring of individual parameters.
  - (b) Preventive and corrective measures taken in case of a reversal event (see section 4.3).
  - (c) Post-deployment and site closure requirements.
- 3.3.4 When any part of the Enhanced Rock Weathering activity is contracted to an external operator, the CO<sub>2</sub> Removal Supplier shall provide the contractual information necessary for assessing compliance with this methodology, the Puro Standard General Rules and other Standard Requirements,<sup>13</sup> as well as any applicable local laws, regulations, and other binding obligations. This information shall at least include:
  - (a) Certified trade registry extracts or similar official documents stating that any and all external operators are validly existing and in compliance with the legislation of the host jurisdiction.
  - (b) Documentation that the CO<sub>2</sub> Removal Supplier is in contractual agreement with the external operator for the purpose of achieving durable CO<sub>2</sub> Removal.

<sup>&</sup>lt;sup>13</sup> Available in the Puro Standard document library.

- (c) In the case of an external weathering material deployment operator, documentation establishing that the weathering material received by the deployment operator will be deployed into eligible application sites.
- (d) Proof of sole ownership to the weathering material sourced, transported or deployed, and attestation of no claim where necessary as per rule 3.5.1.
- (e) Documentation establishing the right to audit the relevant documents and equipment belonging to the external operator for the purposes of CORC Issuance.
- (f) Documentation that the environment, health and safety plan (rule 4.4.5) is applied also to the external operator.
- 3.3.5 The CO<sub>2</sub> Removal Supplier shall ensure that sufficient data is available and accessible for auditing and verification that the Enhanced Rock Weathering activity is compliant with the requirements of this methodology and other applicable Puro Standard Requirements.<sup>14</sup> This includes but is not limited to delivering the necessary data to assess the eligibility of the activities, and quantify the net carbon removal. In particular, the CO<sub>2</sub> Removal Supplier shall provide all calculation functions and parameters utilized for the quantification of net CO<sub>2</sub> Removal in a clear and consistent manner (see section 13).

## 3.4 Additionality

One of the key requirements in the Puro Standard is to ensure that the credited CO<sub>2</sub> Removal is additional, meaning that it would not have occurred in the absence of the incentive provided by carbon credits. Additionality assessment is essential for the integrity and credibility of the carbon crediting program, as it ensures that the credits represent real and additional CO<sub>2</sub> Removal that contributes to mitigating climate change. Additionality is comprised of three different aspects:

- Regulatory additionality: the project is not required by existing laws, regulations, or other binding obligations.
- Baseline/carbon additionality: the activity results in higher volumes of carbon removals
  than the likely baseline alternatives.
- **Financial additionality**: the CO<sub>2</sub> removals are a result of the incentive provided by carbon credits.

<sup>&</sup>lt;sup>14</sup> Available in the Puro Standard document library.

3.4.1 The CO<sub>2</sub> Removal supplier shall demonstrate additionality in accordance with the Puro Additionality Assessment Requirements. <sup>15</sup> This entails demonstrating that the Enhanced Rock Weathering activity is not required by existing laws, regulations, or other binding obligations, that the CO<sub>2</sub> removals are a result of carbon finance, and that the removal activity is carbon net-negative.

## 3.5 Prevention of double-counting

The purpose of preventing double counting is to exclude the possibility of more than one CORC being issued for the same volume of CO<sub>2</sub> Removal, and that an issued CORC represents the sole proof of ownership of the CORC itself, as well as the associated CORC Attributes.

3.5.1 The CO<sub>2</sub> Removal Supplier shall demonstrate prevention of double counting in accordance with the requirements in the Puro Standard General Rules.<sup>16</sup>

## 3.6 Feedstock eligibility and characterization

- 3.6.1 An eligible weathering material shall consist primarily of natural minerals and rocks, or other similar substances (e.g. alkaline waste materials such as slags, mine tailings, recycled concrete, or cement kiln dust) capable of undergoing carbonic acid weathering to sequester CO<sub>2</sub> as (bi)carbonate ions or solid carbonate minerals.
  - (a) The weathering material may further contain incidental associated substances from the sourcing or processing of materials (e.g. clays or other non-weathering materials, or innocuous impurities), as well as tracers or other substances added to assist in the monitoring and verifying of the CO<sub>2</sub> sequestration process.
  - (b) The overall chemical composition of the weathering material (i.e. including the weathering material as well as any impurities and other substances) shall comply with all applicable local laws, regulations, and other statutory requirements, as well as all requirements imposed by relevant external operators or contract partners (e.g. logistics operators or land owners, see section 3.3).
- 3.6.2 The CO<sub>2</sub> Removal Supplier shall undertake physical, chemical and mineralogical analyses of the weathering material in order to determine its constituents and relevant properties, and to provide evidence that the concentrations of potentially toxic elements (PTEs) in the feedstock do not exceed the limits defined in the applicable local, regional, national or international legislation (table 4.3, rules 4.5.2 and 4.5.4).

<sup>&</sup>lt;sup>15</sup> Available in the Puro Standard document library.

<sup>&</sup>lt;sup>16</sup> Available in the Puro Standard document library. In the current version of the Puro Standard General Rules (version 4.2), the relevant requirements are found in section 3.5 PREVENTING DOUBLE COUNTING.

- (a) The geochemical assay shall be conducted at least once annually or after every 5000 tonnes of weathering material applied, whichever comes first. Additionally, the testing shall be conducted whenever *at least one* of the following conditions is fulfilled:
  - (i) Weathering material is spread to the field site of a new Production Facility (i.e. beginning of project).
  - (ii) Weathering material is sourced from a new sourcing site (e.g. a new quarry or supplier).
- (b) The analysis shall cover at least the measurements listed in table 3.1.
- (c) The analyses shall be performed for a statistically representative sample of the entire deployed feedstock as follows:
  - (i) The measurements shall be conducted by using appropriate, peerreviewed scientific best practices or appropriate standard methods (examples referenced in table 3.1). Appropriate, certified reference material shall be used for calibration.
  - (ii) The measurements shall be conducted in laboratories that comply with the general quality control requirements detailed in rule 10.3.4, as well as any utilized international testing standards (e.g. ASTM, ISO, AS, D).
- (d) The analyses shall be used to properly identify and name the feedstock rock based on international protocols approved by the International Union of Geological Sciences (Maitre et al., 2005).
- (e) The analyses shall be used to carry out conservative mass balance calculations that account for PTE concentrations in soils, PTE concentrations in feedstocks, feedstock application rate, and soil bulk density to calculate the maximum PTE load if all feedstock is dissolved and no heavy metals leave the soil. Results from these calculations shall be compared against local regulations (rule 4.5.8).

**Table 3.1.** Overview of required measurements for feedstock characterization.

Measurement	Analytical method with reference	Requirement
Moisture content	Measured shortly before application to field (e.g., ISO 11465:1993)	Required
Specific surface area	-	Recommended (where particle size distribution alone does not sufficiently inform potential reaction kinetics)
Particle size distribution	Sieving (ISO 9276-1:1998, lower precision) or laser diffraction (ISO 13320:2020, higher precision)	Required
Major element oxide composition (at least: CaO, MgO, K <sub>2</sub> O, Na <sub>2</sub> O, P <sub>2</sub> O <sub>5</sub> , SO <sub>4</sub> , SiO <sub>2</sub> , Al <sub>2</sub> O <sub>3</sub> , Fe <sub>2</sub> O <sub>3</sub> , MnO/Mn <sub>3</sub> O <sub>4</sub> , TiO <sub>4</sub> )	XRF (Oyedotun (2018)/ISO 12677:2011), or ICP-MS (ISO 17294-1:2024), ICP-OES (ISO 11885:2007) or AAS (ISO 26845:2008) after acid digestion (EPA 3050B)	Required
Heavy metal content (listed in table 4.3)	XRF (Oyedotun (2018)/ISO 12677:2011), ICP-MS (ISO 17294-1:2024) or ICP-OES (ISO 11885:2007) or AAS (ISO 26845:2008) after acid digestion (EPA 3050B)	Required
Carbon content	Dry combustion (ISO 10694:1995) Coulometry (Paulo et al., 2021)	Required
Loss on ignition	Weight loss from loss of carbonates, water (from hydrated minerals or clays), and organics upon heating a pre-weighed sample to 900-1000 °C	Recommended (to assess weathering potential)
Quantitative mineral composition (relative amounts)	X-ray diffraction (XRD) coupled with e.g. Rietveld refinement (Ali et al., 2022)	Required
Asbestos	(TEM, ISO 13794:2019) or Scanning Electron	Required if feedstock consists of serpentine minerals (chrysotile) or amphibole minerals (e.g., tremolite, actinolite)
Radionuclides	ICP-MS (ISO 17294-2:2023)	Required if feedstock consists of phosphate rocks, granite, pegmatites, tectonically altered or volcanic rocks, mine tailings or industrial byproducts

# 3.7 Feedstock processing and deployment

3.7.1 The CO<sub>2</sub> Removal Supplier may, where necessary, process the sourced weathering material prior to deployment to enhance the weathering rate of the material, or to render it otherwise more suitable for the ERW activity. For example, such processing can include additional grinding, mixing with other sourced feedstocks, and other similar processing steps.

- 3.7.2 The CO<sub>2</sub> Removal Supplier shall evidence that within each field, the weathering material is deployed evenly in accordance with the targeted feedstock application density (tonnes of weathering material deployed per hectare) and utilizing suitable equipment (such as a spreader).
- 3.7.3 The CO<sub>2</sub> Removal Supplier shall keep records of weathering material deployment, which shall include at least the following information:
  - (a) The exact dates and times of each weathering material deployment to the application site.
  - (b) Precise geographic records (GPS coordinates, GIS mapping) of all weathering material application sites used in the project.
    - (i) Each deployment event shall be linked to its specific location within the field site to enable accurate monitoring and verification of carbon storage over time.
    - (ii) The accuracy of geographic mapping should be sufficient to inform monitoring and sampling efforts.
  - (c) The feedstock application density for each deployment with precise reference to time and location.
    - (i) Feedstock density estimates may be based on agricultural spreading logs or direct measurements of e.g., cation concentrations before and just after feedstock application in representative soil samples.

The exact location, boundary, and timeline records shall be securely archived and readily available as required for compliance, monitoring, reporting, and verification purposes. Any changes to the storage site locations, boundaries, or deployment schedules shall be documented and reported to the Issuing Body. The records shall be made available to the Auditor.

# 3.8 Feedstock sustainability and traceability of origin

- 3.8.1 The CO<sub>2</sub> Removal Supplier shall demonstrate and keep records (i.e. traceability, chain of custody) of the origin and type of the feedstock(s) used as weathering material, as further detailed in subrules a-c.
  - (a) For each batch of feedstock, the origin and type records shall include at minimum:
    - (i) Unique identification number or equivalent identifying information;
    - (ii) Description of the material based on the geochemical characterizations specified in table 3.1;

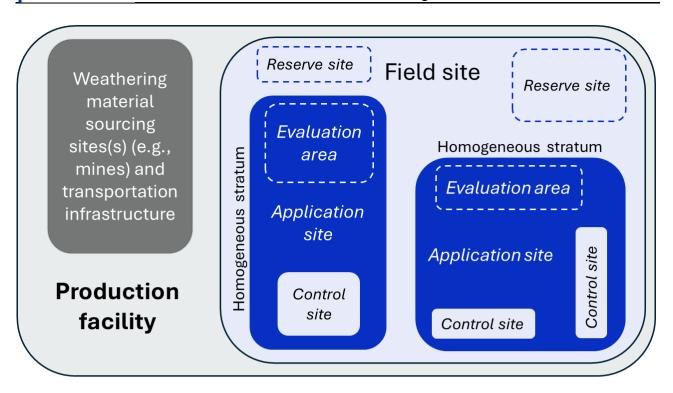
- (iii) Date of delivery and production;
- (iv) Mass of material received;
- (v) Name and location of the entity producing the material (e.g. quarry, industrial plant);
- (vi)Geographic location of origin of the material, including permitted total extractable rock and extraction area with supporting documentation issued by relevant agency; if available, post-closure reclamation plan and reclamation surety bond (see rule 8.2.2).
- (b) If feedstock is sourced from multiple origins (e.g. different quarries), records shall be maintained separately for each source and must indicate the proportion of the total material supplied from each source.
- (c) Any share of the weathering material for which origin or type records cannot be evidenced is not considered eligible, and thereby its share of CO<sub>2</sub>e shall be excluded from the quantification of CORCs.
- 3.8.2 The CO<sub>2</sub> Removal Supplier shall evidence that all weathering materials are sourced from operations that comply with the following criteria:
  - (a) The extraction, production, processing, handling, and transfer of the material shall comply with all applicable national and local laws and regulations, including those governing mining, waste management, industrial by-products, labor, occupational health and safety, and environmental protection.
  - (b) For quarried or mined rock feedstocks, the supplying entity shall hold valid extraction permits and licenses and shall operate in compliance with all environmental and safety regulations in the jurisdiction of origin.
  - (c) For industrially derived feedstocks (e.g., slags, ashes, fines, mine tailings, or other alkaline industrial waste materials), the producing entity shall demonstrate legal authorization to generate, manage, and transfer the material, and the material shall not be classified as hazardous waste under applicable regulations.
  - (d) Any material for which the supplier cannot provide verifiable documentation of legal origin, authorization, or non-hazardous classification shall be considered ineligible. If ineligible material is deployed in the application site, the corresponding share of CO₂e shall be calculated and excluded from the quantification of CORCs.

# 3.9 Field site eligibility and characterization

- 3.9.1 The Enhanced Rock Weathering activity shall take place at an eligible land-based field site (see rule 3.9.2).
  - (a) The field site shall not contain land areas that have been converted from forested land or wetland (or otherwise cleared of native ecosystems) since December 31st, 2020.<sup>17</sup>
    - (i) The CO<sub>2</sub> Removal Supplier shall provide proof of eligible land use, such as land use records issued by competent authorities, or geolocated timestamped aerial/satellite images.
  - (b) Weathering material shall not be applied to seas, lakes, rivers, and other bodies of water including their immediate vicinities such as shorelines, beaches and other similar coastal regions where the weathering material is or can reasonably be expected to be in constant or nearly constant direct contact with a body of water.
    - (i) The weathering material may be applied to irrigated land.
  - (c) Field sites with mean soil organic carbon (SOC) concentrations >5 wt% SOC (see rule 4.5.1) prior to the commencement of the ERW activity (i.e. as measured before or at the beginning of the first crediting period) shall not be eligible for crediting under this methodology.
    - (i) This rule only applies to the first crediting period at any given field site.
    - (ii) Field sites shall not become ineligible in cases where the mean SOC concentration was ≤5 wt% prior to the first crediting period but has since risen over the limit.<sup>18</sup>

<sup>&</sup>lt;sup>17</sup> This date is chosen in alignment with the cut-off dates for land use conversion or management practices defined in the Puro Standard Biomass Sourcing Criteria (available in the Puro Standard document library).

 $<sup>^{18}</sup>$  The purpose of this rule is to preclude field sites with a risk of significant SOC loss, which would counteract the CO<sub>2</sub> removal from the ERW activity. Therefore, limiting eligibility in cases with increasing SOC stocks would be counterproductive.



**Figure 3.2.** The Production Facility (light grey) and its subunits. A field site (light blue) contains homogeneous strata (defined after pre-application soil characterization), which contains control sites (light blue; one or several plots) and an application site (dark blue; one or several plots). Optionally, a more densely sampled evaluation area can be defined within the application site. Note that the field site may have parts (reserve sites) that are dormant with respect to ERW during some or all portions of the crediting period and therefore not part of homogeneous strata.

- 3.9.2 An eligible **field site** shall consist of any number of plots of land with similar characteristics (rule 3.9.3), and utilized in the Enhanced Rock Weathering activity as further defined in subrules a-e.
  - (a) The field site is defined as comprising all the land areas registered under a single Production Facility (i.e. all application sites, control sites, and reserve sites).
  - (b) A plot of land is defined as a contiguous piece of land (i.e. land that is either connected or separated only by a public or private roadway, waterway, easement, or other right of way) of predetermined area, boundaries, and geographic location.
  - (c) An **application site** is a plot or collection of geographically proximate plots that are similar in relevant parameters (see rule 11.1.1), that are grouped together for monitoring purposes, and to which weathering material is applied.
    - (i) An application site can consist of physically separated plots and need not be contiguous.
    - (ii) An **evaluation area** represents the areal subset of the application site area that needs to be monitored as further specified in rule 11.1.3.

- (d) A **control site** is a plot or collection of geographically proximate plots that represent the *business-as-usual* (or *baseline* or *counterfactual*) scenario, and are monitored in order to serve as a baseline reference for quantification of Enhanced Rock Weathering in application sites.
  - (i) A control site can consist of physically separated plots and need not be contiguous.
  - (ii) A control site shall have similar characteristics with regards to monitoring and agricultural management as the associated application site as defined in section 11.1, especially rule 11.1.1.
- (e) A **reserve site** is a former or future application site or control site, which is not in use during the active monitoring period, but has either been utilized as an application or control site in past monitoring periods or is destined for such use in future monitoring periods.
- 3.9.3 The field site, comprising all the land areas registered under a Production Facility, shall have consistent:
  - (a) Geographic location (at least within a single country and within the same major catchment, i.e., not divided by a continental watershed).<sup>19</sup>
  - (b) Climatic conditions (spanning at most three Köppen-Geiger climate zones (Beck et al., 2018)).

# 3.10 Positive sustainable development goal impacts

The Puro Standard General Rules and the associated SDG Assessment Requirements<sup>20</sup> contain the general requirements related to describing and evidencing positive impacts on Sustainable Development Goals (SDGs)<sup>21</sup> that apply to all methodologies. The Puro SDG Assessment Requirements includes a list of project-level indicators, SDG Attributes, for demonstration of positive impacts on SDGs. Additional SDG Attributes can be proposed by external actors via a procedure described in those requirements. Certification of SDG Attributes requires collection of project-specific data and third-party verifications. Certification of SDG Attributes is optional and comes with additional certification fees.

<sup>19</sup> This is required to enable the determination of a unique and unambiguous Host Country for the removal activity.

<sup>&</sup>lt;sup>20</sup> Available in the Puro Standard document library.

<sup>&</sup>lt;sup>21</sup> Resolution adopted by the General Assembly on Work of the Statistical Commission pertaining to the 2030 Agenda for Sustainable Development, G.A. Res 78/206, U.N. Doc. A/RES/71/313 (Jul. 6, 2017). Note that this original SDG indicator framework is subject to regular updates and has since been revised several times.

In the context of Enhanced Rock Weathering, positive SDG impacts might be related to targets<sup>22</sup> such as improved agricultural productivity (SDG target 2.4), action to combat climate change and its impacts (SDG target 13), increase in the buffer capacity of the ocean (SDG target 14.3), or restoring degraded land (SDG target 15.3).

- 3.10.1 The CO<sub>2</sub> Removal Supplier shall provide in the Project Description a qualitative description of expected positive impacts on SDGs in accordance with the Puro Standard SDG Assessment Requirements.<sup>23</sup> This description shall be project-specific, based on the actual operations (e.g. type of feedstock used, measurements of crop productivity).
- 3.10.2 The CO<sub>2</sub> Removal Supplier may decide to pursue certification of SDG Attributes at any time throughout the crediting period. In that case, the CO<sub>2</sub> Removal Supplier shall provide the following documentation:
  - (a) For the Facility Audit, prepare an SDG Report based on the template provided, in which the selected SDG Attributes are described. The SDG Report must include a plan of how the requirements for each selected SDG Attribute will be demonstrated throughout the course of the crediting period. The plans described in the SDG Report must also be reflected in the Monitoring Plan (e.g. in an appendix specific for SDG Attributes).
  - (b) For the Facility Audit, provide in the Project Description a description of expected positive impacts on SDGs based on the selected SDG Attributes and their associated monitoring plan, and any outcome already available.
  - (c) For the Facility Audit or subsequent Output Audits, i.e. whenever available, provide the data required to demonstrate the achieved positive impact on SDGs. This information will be verified by the appointed auditor, and if successful, result in SDG Attributes associated for the applicable CORCs (see details in the SDG Assessment Requirements).

<sup>&</sup>lt;sup>22</sup> For a list of currently up to date SDG targets, see the current official SDG indicator list hosted at the United Nations Statistics Division website. Furthermore, the United Nations Department of Economic and Social Affairs website provides a browsable SDG indicator list.

<sup>&</sup>lt;sup>23</sup> Available in the Puro Standard documents library.

# 4 Reversal, environmental, and social risks

#### 4.1 Overview

The primary objective of identifying risks is to detect early and ongoing events and ambiguities that could affect the predetermined objectives of the ERW activity. Several risks concerning climate, ecosystems, and human health need to be identified, accounted for and mitigated. These risks can be categorised into **reversal** risks, **environmental** risks and **social** risks.

In the context of this methodology, *risk* refers to events and situations, whose outcomes are (reasonably well) known in advance and needs to be distinguished from *uncertainty*, which refers to aspects of decision-making which are not easily quantified (Park & Shapira, 2017). The overall risk of an event or situation is often defined as the combination of two parameters: the probability (likelihood) for the event to be realized, and the severity of the event, if realized. Effectively, risk management is composed of four main steps: identification, evaluation, mitigation and control of hazards that could occur within the activity boundary. Therefore, an effective risk assessment takes into account the nature and magnitude of risks in relation to the outcome.

For the purposes of this methodology, the term **reversal** refers to an event which cancels, entirely or in part, the effects of an issued CORC (for further details, see the Puro Standard General Rules<sup>24</sup>). Reversals are therefore considered as unaccounted-for events resulting in a situation where at least a part of the removed, quantified and certified carbon represented as a CORC is either released back into the atmosphere (re-emission) or can no longer be considered safely and durably stored for a long term. It is separated from carbon losses (see section 6.3), which include re-emission pathways identified prior to the CORC issuance, and therefore accounted for in the CORC quantification (see rule 5.3.1).

An eligible ERW activity must also take into consideration multiple **environmental and social risks**, which may negatively impact ecosystems, human health or the local communities. This section outlines the overall criteria to assess, evaluate and mitigate such risks, including certain predetermined risks which all projects seeking for CORC issuance must account for. In addition to the requirements set in the Puro Standard General Rules and in this section of the methodology, further requirements and guidelines are also found in the Puro Stakeholder Engagement Requirements, the Puro Stakeholder Engagement Report Template and the Puro Environmental and Social Safeguards Questionnaire<sup>25</sup>.

This methodology, together with applicable local legislation and regulations, sets guidelines and rules to mitigate the possible risks. Appropriate and transparent collection of data as well as regularly updated monitoring plans are key factors in managing and mitigating risks, but effective

<sup>&</sup>lt;sup>24</sup> Available in the Puro Standard documents library.

<sup>&</sup>lt;sup>25</sup> Ibid.

risk mitigation also requires efficient and transparent communication and collaboration between the CO<sub>2</sub> Removal Supplier and the local authorities and stakeholders.

# 4.2 General requirements for risk assessment and management

This section focuses on general risk management criteria applicable for reversal risks as well as environmental and social risks. Further assessment criteria specific to each risk type is defined in the following sections:

- Reversal risks (see section 4.3)
- Environmental and social risks (see sections 4.4 and section 4.5).

For all types of risk associated with the ERW activity, identifying the key risks is the first step towards a design of an effective monitoring, mitigation and response measures to minimize their likelihood and impact. By proactively managing these risks, the CO<sub>2</sub> Removal Supplier ensures the integrity and safety of the operations.

Risks can be proactively managed by utilizing a **mitigation hierarchy framework**, which aims to efficiently limit the negative impacts or outcomes of a given risk. Such a hierarchy is based on a sequence of five iterative actions (figure 4.1): anticipating the potential risk, avoiding the risk, minimizing and/or mitigating any negative impacts of the risk, and finally, compensating for any residual impacts. The steps are further characterised as:

- Anticipation: The first step comprises identifying potential risks relevant for a specific ERW
  project activity before they materialize and designing strategies to either avoid, mitigate or
  minimize their impact.
- **Avoidance**: Includes measures taken to avoid any negative impacts identified for a given risk. Avoidance measures may include, but are not limited to a careful selection of feedstock sources (see sections 3.6 and 3.8) or the application site (see section 3.9). Effective avoidance measures must be considered during the early stages of the project (see rule 4.2.1).
- **Minimization**: Includes measures to either reduce the duration, intensity or extent of a given risk, in case it cannot be fully avoided. Effective minimization measures may eliminate some negative impacts, if such measures are planned and executed accordingly.
- Mitigation: Includes measures to mitigate the impacts of a given risk, in case the impacts
  cannot be fully avoided or minimized. Collectively, avoidance, minimisation and mitigation
  measures serve to reduce, as much as possible, any negative residual impacts of a given risk.
- Compensation: As the last step, compensation measures are the last resort in case avoidance, minimisation and/or mitigation measures are not capable of fully preventing the negative

impacts of a given risk. In the context of this methodology, this applies in the case of a reversal event.<sup>26</sup>



Figure 4.1. Mitigation hierarchy framework for risk assessment in the context of an ERW project.

Note that the Puro Standard General Rules contain requirements on risk assessment and management, particularly in the context of permanence and reversal.

- 4.2.1 The CO<sub>2</sub> Removal Supplier shall comprehensively identify and assess all risks related to the ERW activity, including risks of reversal (section 4.3) and environmental and social risks (sections 4.4 and 4.5)
  - (a) The assessment of risks shall be systematic and based on robust, science-based risk assessment criteria, against which the significance of a specific risk/impact is evaluated and measured.
  - (b) The assessment of risks shall be specific to the ERW activity and Production Facility.
  - (c) Risk assessments shall be utilized to inform and improve project design and the monitoring plan (see rule 4.4.3 e)
  - (d) Risk assessments shall be reviewed and updated periodically (rule 9.2.4) together with the Monitoring Plan (see section 9.2).
- 4.2.2 The assessment of risks shall cover at least the following components:

<sup>&</sup>lt;sup>26</sup> Requirements for reversal events, including potential compensation, are further detailed in the Puro Standard General Rules, available in the Puro documents library

- (a) Identification and description of the anticipated risks and its impact.
  - The CO<sub>2</sub> Removal Supplier shall provide a detailed description of each identified risk as well as any adverse impacts associated with that risk.<sup>27</sup>
- (b) Assessment of each identified risk.
  - (i) The assessment shall at least include the characterization of likelihood and severity as well as an evaluation of the significance of the risk to the CO<sub>2</sub> Removal Project.
  - (ii) To analyse the likelihood and severity of each risk, the CO<sub>2</sub> Removal Supplier shall use either the risk matrix presented in table 4.1, or another quantitative and/or qualitative risk scoring system approved by the Issuing Body.
- (c) Description of the measures to avoid, minimize, mitigate or compensate the negative impacts of identified risks based on the mitigation hierarchy (figure 4.1), including where relevant a description of the parameters and methods utilized to monitor the potential impacts.
  - (i) Preventive and corrective measures shall be identified or planned as contingency measures to reduce risks.
  - (ii) The risk mitigation strategy may include, but is not limited to, data collected from both in-situ sampling and laboratory analyses conducted by the CO<sub>2</sub> Removal Supplier (see section 11).
  - (iii)When the severity or the likelihood of the risk is at an undesirable or intolerable level (table 4.1), the CO<sub>2</sub> Removal Supplier shall either eliminate or reduce the risk to a safe and acceptable level.
  - (iv) When the severity or the likelihood of the risk are at an inoperable level (table 4.1), the CO<sub>2</sub> Removal Supplier shall immediately cease all operations, prevent further negative impacts from occurring, and notify the Issuing Body.
- (d) Assessment of acceptable, alert and threshold values for each measurable parameter.

<sup>&</sup>lt;sup>27</sup> The impacts can result from direct, indirect or cumulative risks, and they can be either direct (i.e. isolated events with a clear trigger or cause), or progressive (i.e. gradual changes that accumulate over time).

- (i) The acceptable, alert and threshold values shall be derived from applicable local regulations or, if no such regulations exist, from other relevant sources, such as peer-reviewed scientific literature or industry best practices.
- (ii) In cases where values for acceptable, alert or threshold levels are prescribed in the applicable local regulations and these values are more stringent than values prescribed or recommended in this methodology, the local values shall be utilized.
- (iii) The CO<sub>2</sub> Removal Supplier shall design and implement operating procedures in case the alert or threshold value is reached.
- (iv) The acceptable, alert and threshold values shall be periodically reviewed to ensure the safety of the operations.
- (e) Description of public participation and consultation, as described in the Puro Standard General Rules and the Puro Stakeholder Engagement Requirements.<sup>28</sup>
- 4.2.3 The CO<sub>2</sub> Removal Supplier shall record and disclose to the Issuing Body any negative environmental or social impacts or reversal events (or claims thereof) occurred during the monitoring period, including but not limited to any legal actions and/or other written complaints filed by affected parties.

<sup>&</sup>lt;sup>28</sup> Available in the Puro Standard documents library.

**Table 4.1**. A 5x5 risk matrix and descriptions of the risk scores and required actions for the given risk levels.

Risk score	Risk level	Action				
1	Negligible	Insignificant risk with negligible consequences. No requirement for immediate action but requires planning to avoid future events.				
2–3	Acceptable	Minor risks with limited negative impacts. No requirement of immediate action, but effective monitoring and controls are necessary.				
4–9	Undesirable	Manageable risks, which require an active, planned approach for risk avoidance, minimization and mitigation to reduce the negative impacts.				
10–19	Intolerable	_	High likelihood or severe negative impacts. Requires immediate action to avoid, minimize or mitigate the impacts.			
20—25	Inoperable	Critical failure. Requires an immediate cessation of operations. Further avoidance, minimization or mitigation measures are required for the operations to continue.				
Likelihood → Severity ↓	Very Low (1)	Low (2)	Medium (3)	High (4)	Very High (5)	
Minor (1)	1	2	3	4	5	
Serious (2)	2	4	6	8	10	
Major (3)	3	6	9	12	15	
Severe (4)	4	8	12	16	20	
Extreme (5)	5	10	15	20	25	

# 4.3 Requirements for reversal risk assessment and management

The long-term effectiveness of any carbon removal activity depends on the ability to store carbon safely and durably. In this context, a reversal risk refers to any event or condition that may

compromise the integrity of carbon storage, leading to the unintended re-emission of previously sequestered carbon back into the atmosphere.

It is important to distinguish reversal risks from carbon losses (see section 6.3), which result from reemission pathways known or assumed a priori, and which therefore are accounted for at the time of CORC issuance. In contrast, reversals refer to previously unknown or unanticipated re-emissions that occur after the issuance of CORCs, and are addressed via the procedures described in the Puro Standard General Rules.<sup>29</sup> Reversal events may include physical disturbances or environmental changes, whether caused by natural phenomena or human activities, that temporarily or permanently affect the behaviour of stored carbon.

The primary objective of identifying reversal risks is to proactively detect potential events or conditions that could compromise the permanence of the carbon storage, enabling the CO<sub>2</sub> Removal Supplier to define measures to address those risks and compensate for any reversals. When all of the eligibility requirements (section 3) and risk assessment criteria (section 4.2) set in this methodology are met, the risk of reversal is considered low.

Note that this section is limited to specific assessment criteria for reversal risks. For reversal risk monitoring requirements, see section 9.6.

- 4.3.1 Prior to the start of the operations, the CO<sub>2</sub> Removal Supplier shall assess any potential sources of a reversal risk, based on the eligibility requirements (see section 3) and general risk assessment criteria detailed in section 4.2. The assessment shall include reversal risks arising from:
  - (a) Natural processes leading to the reacidification of soils or waters that could reverse carbonate or bicarbonate formation, such as acid rain or other acid accumulation
  - (b) Anthropogenic interference, including but not limited to:
    - (i) Land use changes that would lead to sequestered carbon reversals such as repeated applications of ammonium-based fertilizers
    - (ii) Acidic mine drainage or industrial spills that lead to soil acidification
  - (c) Any other potential reversal pathway identified by the CO<sub>2</sub> Removal Supplier.

# 4.4 Requirements for environmental and social risk assessment and management

The Puro Standard General Rules<sup>30</sup> contain the general requirements on environmental and social safeguards that apply to all methodologies, while this section contains further requirements on

<sup>&</sup>lt;sup>29</sup> Available in the Puro Standard documents library.

<sup>&</sup>lt;sup>30</sup> Available in the Puro Standard documents library.

assessing environmental and social risks and their impacts relevant to ERW activities in particular (see also section 4.2 for general risk assessment requirements).

EIA REGULATION FOR ERW PRODUCTION FACILITIES: In some jurisdictions ERW Production Facilities may be subject to Environmental Impact Assessment (EIA) regulation to evaluate and address their potential social and environmental effects. The need for an EIA is typically determined by local regulations based on project size, environmental risks, and location. If an EIA is required by law, compliance is mandatory for certification under this methodology. If regulation does not require an EIA, conducting an EIA is encouraged by Puro.earth as a best practice but is not a strict prerequisite.

- 4.4.1 The CO<sub>2</sub> Removal Supplier shall have in place, maintain, and abide by environmental and social safeguards to the extent required by this methodology, the Puro Standard General Rules<sup>31</sup>, and any applicable local statutory requirements, in order to ensure that the ERW activities do no "net-harm" to the surrounding natural environment or local communities.
- 4.4.2 The CO<sub>2</sub> Removal Supplier shall provide all documents related to the analysis and management of environmental and social impacts of the ERW activities required by the applicable local laws and regulations, including but not limited to environmental permits, assessments, licenses, or an Environmental and Social Impact Assessment (EIA).
- 4.4.3 The CO<sub>2</sub> Removal Supplier shall prepare a project-specific Environmental and Social Risk Assessment in accordance with the general risk assessment criteria detailed in section 4.2 and as further detailed in subrules a-d and rule 4.4.4.
  - (a) The Environmental and Social Risk Assessment shall comply with the requirements of this methodology, the Puro Standard General Rules<sup>32</sup>, other Puro Standard Requirements<sup>33</sup>, as well as any applicable local laws, regulations, and other binding obligations in scope and content.
  - (b) The scope of the assessment shall cover all stages (feedstock sourcing, processing, transportation, deployment and monitoring) within the activity boundary (see rule 7.2.2).

<sup>&</sup>lt;sup>31</sup> Available in the Puro Standard documents library.

<sup>32</sup> Ibid.

<sup>33</sup> Ibid.

- (c) To address the components of the Environmental and Social Risk Assessment partly or in full, the CO<sub>2</sub> Removal Supplier may utilize and refer to other documents (e.g. project description documents, stakeholder engagement reports, or legally mandated EIA or other environmental and social impact assessment documents) containing the required information, provided that such additional documents are also included (see rule 4.4.2).
- (d) In order to minimize environmental and social risks associated with the ERW activity, the CO<sub>2</sub> Removal Supplier shall utilize the findings, insights, and information resulting from the Environmental and Social Risk Assessment and other documents related to the analysis and management of environmental and social impacts<sup>34</sup> to inform and improve project design and the monitoring plan (section 9.2).

#### 4.4.4 The Environmental and Social Risk Assessment shall include:

- (a) A list and description of the applicable legal and regulatory framework and requirements pertaining to the assessment and management of the environmental and social impacts of the ERW project.
- (b) Description of the existing local environmental and socio-economic conditions (i.e. background information on the current environmental and socio-economic context in which potential impacts are assessed).
- (c) Description of the ERW activity in detail, including construction, operation, and decommissioning of infrastructure, and other aspects affecting the assessment of environmental and social impacts.
- (d) Identification and description of the anticipated environmental and social impacts, including but not limited to the predetermined risks set in this methodology (see section 4.5, and in particular table 4.2). For example, such impacts might include any potential negative effects to:
  - (i) Soil, air, and water quality (e.g., hydrological cycles, physical and biogeochemical properties).
  - (ii) Flora and fauna (e.g., biodiversity, habitats).
  - (iii) Human health and safety.
  - (iv) Socio-economic factors (e.g., related to land use or water resources).

<sup>&</sup>lt;sup>34</sup> Such documents might include a potential EIA or other legally mandated documents (see rule 4.4.2), and the Puro Standard Environmental and Social Safeguards Questionnaire (available in the Puro Standard document library)

- (v) Local communities (e.g., due to noise, pollution, limiting access to recreationally significant areas).
- (vi) Sites of cultural or archaeological significance (e.g., ancient burial sites).
- (e) A disaster management plan, in case of any abrupt situations such as spillages or natural hazards (see also rule 4.4.5 relating to management of physical harms and exposure to harmful chemicals in particular).
- (f) A plan for managing environmental hazards that may result from the ERW activity, including elevated levels of PTEs in soils. The plan for responding to elevated levels of PTEs in soil shall include an immediate ceasing of feedstock deployment and plan for soil remediation.
- (g) Documentation that robustly addresses all material environmental and social impacts, following criteria determined in the Puro Standard General Rules<sup>35</sup> and this methodology.
- 4.4.5 The CO<sub>2</sub> Removal Supplier shall prepare and abide by an **environment**, **health and safety (EHS) plan** to assess and mitigate exposure to harmful chemicals and physical harms. The plan shall contain at least the following elements related to environmental risks and human health risks:
  - (a) Identification and listing of any potentially harmful chemical compounds and potentially dangerous objects and procedures employed at any stage within the activity boundary.
  - (b) Risk assessment and mitigation measures for chemical or physical injuries (for example, due to inhalation, ingestion, or skin contact with harmful substances, or accidents with machines) considering all relevant exposure pathways.
  - (c) Based on the local statutory requirements, a determination of threshold exposure values and/or other limit values to prevent chemically induced diseases (whether through direct exposure, or indirect exposure such as through environmental contamination where relevant), and a description of the measures to limit and monitor the exposure to harmful chemicals.
  - (d) Identification of any potential pathways for chemical spills or leakages, and a description of the measures to prevent leakages and mitigate any harm to the environment or human health.
  - (e) Emergency preparedness plan, including appropriate response procedures in case a chemical spill has occurred. The plan shall at least address:

<sup>&</sup>lt;sup>35</sup> Available in the Puro Standard documents library.

- (i) How to prevent any further damage.
- (ii) Equipment and methods for cleanup.
- (iii) Evacuation zones and procedures.
- (iv) First-aid procedures.
- 4.4.6 The CO<sub>2</sub> Removal Supplier shall provide information to all involved stakeholders (e.g., local community, landowner, local municipality, investors, credit buyers) about the environmental and social risks associated with the ERW activity at the specific site of application and in the receiving catchment, in accordance with the Puro Standard Stakeholder Engagement Requirements.<sup>36</sup>
- 4.4.7 The CO<sub>2</sub> Removal Supplier shall comply with all applicable local laws and regulations relating to access and consumption of water resources. The CO<sub>2</sub> Removal Supplier shall furthermore recognize, respect and promote the human rights to safe drinking water and sanitation<sup>37</sup> as well as the right to water as laid out in the General Comment No. 15 of the United Nations Committee on Economic, Social and Cultural Rights.<sup>38</sup> In particular, the CO<sub>2</sub> Removal Supplier shall not endanger the availability, quality, or accessibility of the local water supply, as defined in article 12 of General Comment No. 15.<sup>39</sup>

# 4.5 Key environmental and social risks

During the weathering reactions, elements are released into the soil. Depending on the material composition, elements released can also include potentially toxic elements (PTEs) which above certain levels may have detrimental effects to the environment and be harmful to living organisms, including plants, animals, and humans. PTEs relevant to this methodology include heavy metals (e.g., nickel, chromium VI, cadmium, uranium), radionuclides (e.g. <sup>40</sup>K, <sup>226</sup>Ra, or <sup>232</sup>Th), and other contaminants such as asbestos. These may have negative effects on ecosystems (toxic for fauna and flora, contamination of water resources) and humans (health effects via dust inhalation, direct exposure to contaminated soil, ingestion through the food chain or contaminated water).

Beyond PTEs, environmental risks associated with ERW may include undesirable changes to soil biogeochemistry. While ERW can improve soil pH, increase nutrient availability (e.g., Ca, Mg), and boost crop yields, overapplication or unsuitable rock types may disrupt soil chemistry, lower organic carbon levels, or introduce harmful trace metals, potentially affecting plant health and productivity.

<sup>36</sup> Ibid.

<sup>&</sup>lt;sup>37</sup> The human rights to safe drinking water and sanitation, G.A. Res 78/206, U.N. Doc. A/RES/78/206 (Dec. 22, 2023).

<sup>&</sup>lt;sup>38</sup> General Comment No. 15 (2002), The right to water (arts. 11 and 12 of the International Covenant on Economic, Social and Cultural Rights), U.N. Doc. E/C.12/2002/11 (Jan. 20, 2003).

<sup>&</sup>lt;sup>39</sup> Ibid., p. 5.

This section outlines the key risks predetermined in the context of this methodology (table 4.2) and specific requirements for their assessment, avoidance and mitigation, when applicable.

**Table 4.2.** Predetermined environmental risks in the context of this methodology. Note that the list is not exhaustive.

Risk	Description	Risk assessment	Risk minimization or mitigation
Soil organic carbon (SOC)	Soil organic carbon may decrease as a consequence of ERW activity	Medium; monitor SOC concentrations and stocks before feedstock application and at the end of monitoring periods	Use SOC analysis values to ensure that SOC stocks in soils do not decrease drastically. Field sites with high SOC concentrations (>5% wt SOC) are not eligible for ERW (rule 3.9.1).
Heavy metals	Heavy metal concentrations in feedstocks and soils may lead to bioaccumulation, toxicity, and groundwater contamination	Low to medium; Evaluate metal concentrations in feedstocks and post- deployment soils	Use feedstock analysis values to ensure that metal concentrations in feedstocks and soils are within regulatory requirements and beneath established safe thresholds
Asbestos	Naturally occurring fibrous minerals in some (ultra)mafic rocks can become airborne during grinding or application	High health hazard if present; inhalation may cause cancer; risk depends on feedstock geology and particle handling	Avoid asbestos-prone rocks; conduct mineralogical testing; control dust; enforce PPE and safe material handling protocols
Radionuclides	Naturally occurring radioactive elements (e.g. uranium, thorium) may be present in trace amounts in some rock types	Generally low; potential exposure via dust inhalation or leaching depends on rock source and application scale	Screen feedstocks for radioactivity; avoid high-U/Th rocks; conduct leach tests; monitor radon in enclosed facilities
Respiratory Risks	Inhalation of fine rock dust (e.g., PM10, respirable silica) during crushing, handling, or spreading can impair lung function	Medium to high; prolonged exposure may cause silicosis, bronchitis, or other chronic respiratory conditions	Use dust suppression; apply in low-wind conditions; provide PPE; ensure enclosed or ventilated equipment for workers; increase moisture content of rock dust
Agricultural Disruption	ERW can alter soil pH, nutrient balance, or texture, potentially affecting crop growth and yields	Low to medium; impacts depend on crop type, soil conditions, and application rate	Conduct field trials; tailor application rates; monitor soil chemistry; engage farmers in planning and feedback

#### **Effect of Enhanced Rock Weathering on Soil Organic Carbon**

In addition to its impact on soil inorganic carbon, ERW may also influence soil organic carbon (SOC), a major pool of terrestrial carbon. The magnitude and direction of this influence remain subject of ongoing research and are likely to vary depending on local soil conditions and other factors. Whereas some studies suggest stabilization of SOC stocks, others have documented SOC decreases as a result of ERW activity (Buss et al., 2024; Lei et al., 2025; Sokol et al., 2024). Several mechanisms

may mediate ERW's effect on SOC, including changes in soil pH, microbial respiration rates, plant productivity, and physical soil properties such as compaction. SOC concentrations often vary greatly within and between years, compared to the variability of SIC. Because of the potential volatility of SOC and the resulting different storage permanence compared to SIC, carbon crediting based on changes in SOC stocks resulting from ERW is currently not a viable option (Mills et al., 2024). Soils with very high SOC concentrations (e.g., >5 wt% SOC, (Mills et al., 2024)) should be avoided for ERW project development in favor of less organic-rich soils to decrease the risk of SOC loss offsetting CDR.

- 4.5.1 The CO<sub>2</sub> removal supplier shall monitor soil organic carbon (SOC) concentrations and stocks (to NFZ depth, see rule 11.2.9) of the field site throughout the crediting period (see also rule 9.3.5 and table 9.2).
  - (a) Samples to monitor bulk SOC stocks shall be collected from a representative subset of the application and control sites included within the Production Facility.
    - (i) The CO<sub>2</sub> Removal Supplier shall determine the appropriate sampling area and density in accordance with rule 9.3.5 d and the targeted statistical significance and power of the required analysis (see subrule b).<sup>40</sup>
    - (ii) Samples shall be collected at least before or at the start ( $t_0$ ) and end ( $t_1$ ) of each monitoring period. Starting from the second monitoring period within each crediting period, the  $t_1$  measurements from the preceding monitoring period may be used instead of  $t_0$  measurements.
  - (b) The CO<sub>2</sub> Removal Supplier shall quantify the change in mean SOC stocks at the application sites relative to control sites within each homogeneous stratum at the end of each monitoring period.
    - (i) The difference in mean SOC stocks shall be determined at the 95% confidence level ( $\alpha = 0.05$ ) utilizing an appropriate statistical analysis method (e.g. the two-sample t-test).
    - (ii) The statistical power of the analysis shall be sufficient such that for a 5% reduction of SOC stock, the probability of a type II error (i.e. a false negative or failing to reject a false null hypothesis) is at most 20% ( $\beta \le 0.2$ ).

<sup>&</sup>lt;sup>40</sup> For approximate formulas to estimate necessary sample sizes, see e.g., van Belle (2008).

(c) If a statistically significant and sustained (i.e., persisting over >1 year) SOC stock reduction in application sites compared to control sites is observed, countermeasures (e.g., reduction of feedstock application) shall be considered to avoid long-term, significant SOC loss in future deployments. SOC reduction also falls under embodied emission treatment, see rule 7.4.4.

#### **Heavy metals**

Heavy metals in ERW feedstocks—such as nickel, chromium, or cobalt—have the potential to pose ecological and human health risks if mobilized into soil or water. In plants, elevated concentrations can inhibit growth and nutrient uptake. In soils, they may harm microbial communities and reduce fertility. If leached into groundwater or absorbed by crops, they can enter food chains, posing risks to animals and humans through bioaccumulation. Some, like hexavalent chromium, are toxic and carcinogenic even at low concentrations. The severity depends on metal concentration, rock weathering rate, soil properties, and local hydrology. In order to mitigate these risks, feedstocks and their applications will be subject to limitations and regulations laid out in this section.

#### Heavy metal concentrations in the weathering material

Heavy metal concentration in applied weathering materials shall be evaluated and reported to ensure they are consistent with local regulations and do not pose environmental or health risks.

- 4.5.2 The CO<sub>2</sub> Removal Supplier shall test their feedstocks and report on the concentrations of the PTEs listed in table 4.3.
- 4.5.3 CO<sub>2</sub> Removal Suppliers using slags, fly ash, kiln residues, or similar industrial-waste material feedstocks shall test those feedstocks for the presence of hexavalent chromium (Cr(VI)) using appropriate analytical tests. Evaluated feedstocks shall contain < 2 mg Cr(VI) /kg dry matter.<sup>41</sup>
- 4.5.4 The CO<sub>2</sub> Removal Supplier shall ensure that the concentrations of heavy metals and other PTEs in weathering material, including all the elements listed in table 4.3, complies with all local and jurisdictional regulations.

#### Maximum heavy metal concentrations in the soil

Evaluating heavy-metal risks in ERW projects using threshold values from maximum concentrations in soils requires measurement of background (pre-project) concentration levels as well as the post-application thresholds within the soil (rule 9.3.5, table 9.2).

4.5.5 The CO<sub>2</sub> Removal Supplier shall test the soils within their project prior to feedstock application and report on the concentrations of the PTEs listed in table 4.3.

<sup>&</sup>lt;sup>41</sup> European Commission, Regulation (EU) 2019/1009 of the European Parliament and of the Council — <u>Annex I: Requirements for fertilising products</u>

- 4.5.6 Limit values for heavy metals in soil (listed in table 4.3) should not be exceeded at the field site before or after feedstock application. Elements in table 4.3 without an identified limit shall also be evaluated and reported.
- 4.5.7 The CO<sub>2</sub> Removal Supplier shall demonstrate with ≥95% confidence using appropriate statistical tests that the full field site average concentration of each relevant PTE is below the applicable (see rules 4.5.8 to 4.5.11) limit value.

**Table 4.3**. Limit values for metal contents in soils derived from Council Directive 86/278/EEC of 12 June 1986 on the protection of the environment, and in particular of the soil, when sewage sludge is used in agriculture and Regeling Bodemkwaliteit 2022.

Metal	Limit (mg/kg dry matter) <sup>a</sup>
Antimony (Sb)	2
Arsenic (As)	5
Barium (Ba)	-
Beryllium (Be)	-
Cadmium (Cd)	1
Chromium (Cr)	100
Cobalt (Co)	20
Copper (Cu)	100
Lead (Pb)	60
Manganese (Mn)	-
Mercury (Hg)	0.5
Nickel (Ni)	150
Selenium (Se)	-
Thallium (Tl)	-
Uranium (U)	-
Vanadium (V)	100
Zinc (Zn)	200

- 4.5.8 CO<sub>2</sub> Removal Suppliers shall ensure that soil heavy-metal concentrations (as determined by mass balance based on feedstock concentrations, see rule 3.6.2 e) remain below limits specified by laws and regulations relevant to their jurisdiction of operation.
- 4.5.9 CO<sub>2</sub> Removal Suppliers who are operating in the United States or another area with less stringent limits for heavy metals in soil should operate within the limits prescribed in table 4.3.

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- 4.5.10 In cases where CO<sub>2</sub> Removal Suppliers are compliant with the regulatory limits of their region, but remaining below the limits proscribed in table 4.3 is not feasible, a contextual justification may be provided to indicate why soil concentrations exceed the limits and the risk mitigation efforts being undertaken.
- 4.5.11 Projects that exceed the prescribed PTE limits in soils after the application of soil amendments, but incorporate mitigation strategies, may be permissible. These projects should demonstrate compliance with the limits listed in table 4.3 by the end of the monitoring period.

#### **Asbestos**

Asbestos is the general name given to naturally fibrous silicate minerals occurring in 'asbestiform' crystals that can cause serious human health risks via exposure through inhalation. The most common type of asbestos minerals belongs to the serpentine group, namely chrysotile (white asbestos), but asbestos can also occur in rocks which contain minerals from the amphibole group including amosite, crocidolite, and tremolite.

In ERW projects, exposure to asbestos or asbestiform minerals may happen during handling or spreading of the weathering material, as well as after application through wind erosion. In ERW projects, grinding and comminution of the weathering material may be necessary, and it can thereby be conservatively concluded that weathering material should not contain asbestos or asbestiform minerals above trace levels.

- 4.5.12 CO<sub>2</sub> Removal Suppliers using ultramafic rocks such as serpentinite and peridotite, or rock containing amphibole minerals shall screen their feedstocks for the presence of asbestos.
- 4.5.13 Asbestos screening shall use Polarized Light Microscopy (PLM) or Transmission Electron Microscopy (TEM) or Scanning Electron Microscopy (SEM) to detect asbestos fibers. This may be aided by XRD and Thermogravimetric Analysis (TGA) or Differential Thermal Analysis (DTA). The acceptable limit shall be ≤ 0.25% by weight.<sup>42</sup>

#### **Radionuclides**

Radionuclides are naturally present in the environment, in soil, and in some weathering material. Excessive exposure to radionuclides affects human health. Application of weathering material with high levels of radionuclides might lead to increased concentrations in soils.

4.5.14 CO<sub>2</sub> Removal Suppliers using feedstocks that originate from phosphate rocks, granite, pegmatites, tectonically altered or volcanic rocks, mine tailings or industrial byproducts shall screen for the presence of radionuclides.

<sup>&</sup>lt;sup>42</sup> California EPA: Air Resources Board Test Method 435 Determination of Asbestos Content of Serpentine Aggregate

- 4.5.15 Radionuclides screening shall be performed via gamma spectroscopy or ICP-MS to measure:
  - (a) Uranium (U-238 series)
  - (b) Thorium (Th-232 series)
  - (c) Potassium-40 (K-40)
- 4.5.16 For radionuclides in the feedstock material, the acceptable limit of activity concentration shall be <1 kBq/kg.<sup>43</sup>

#### **Other PTEs**

4.5.17 CO<sub>2</sub> Removal Suppliers using feedstocks that may have been exposed to chemicals or other treatments which may pose risk to biological organisms or ecosystems shall conduct appropriate chemical analyses of the possible contaminants in the feedstock and comply with local regulations to minimize the risk.

#### Respiratory risk from dust inhalation

ERW involves grinding and spreading rocks, which can generate fine particulate dust (e.g.,  $PM_{10}$  and  $PM_{2.5}$ ). Inhalation of this dust—especially if it contains crystalline silica (quartz)—can pose significant respiratory risks. Chronic exposure may lead to silicosis, bronchitis, or other lung diseases, particularly for workers involved in crushing, handling, and field application.

The general public's risk is low if dust is well-contained, but improper application—especially under dry or windy conditions—can create localized air quality concerns. Risk is elevated in fine particle size ranges (under  $100 \, \mu m$ ), which are common in ERW to speed weathering.

Mitigation measures include using low-dust formulations, applying under damp conditions, enforcing PPE for workers, and selecting feedstocks with verified low hazard profiles. Dust control is critical for both worker safety and community acceptance of ERW projects.

4.5.18 CO<sub>2</sub> Removal Suppliers shall comply with mitigation measures prescribed in ISO 45001<sup>44</sup> pertaining to dust and inhalation hazards including the applicable hazard identification, risk assessment, risk mitigation, worker participation, monitoring and evaluation protocols (see also table 4.2).

<sup>&</sup>lt;sup>43</sup> Commission Delegated Regulation (EU) 2022/973 -Article 2.2 - laying down criteria on agronomic efficiency and safety for the use of by-products in EU fertilising products

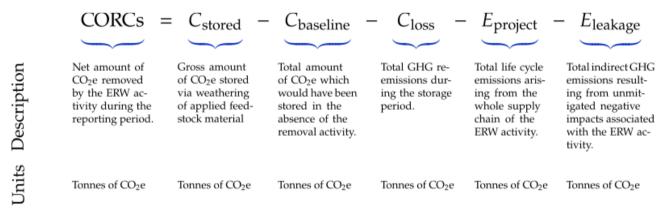
<sup>&</sup>lt;sup>44</sup> ISO. (2018). ISO 45001:2018 Occupational health and safety management systems Hazard identification for dust inhalation: Clause 6.1.2.1. Risk assessment of airborne dust exposures: Clause 6.1.2.2. Controls for dust hazards: Clause 8.1.2. Monitoring of workplace dust exposure: Clause 9.1

# 5 Quantification of CO<sub>2</sub> Removal Certificates (CORCs)

## 5.1 General principles

In general, a CORC represents net 1 tonne CO<sub>2</sub>e removed from the atmosphere. In the specific case of Enhanced Rock Weathering, the CO<sub>2</sub> removal results from the chemical reactions occurring during the weathering process, which remove CO<sub>2</sub> from the atmosphere and sequester it as long-lasting solid or dissolved mineral substances (mainly bicarbonates and carbonates).

The overall principle of the CORC calculation (see figure 5.1) is that the CO<sub>2</sub> Removal Supplier first determines the gross amount (in metric tonnes) of CO<sub>2</sub> sequestered as a result of the weathering reactions over a given monitoring period. Various deductions are then made, such as supply chain *emissions*, any potential *losses*, and the effect of any potential economic *leakage*. The resulting net amount of carbon sequestered is converted to CO<sub>2</sub> equivalents and credited as CORCs. More details on the method of calculation are given in this section.



**Figure 5.1.** CORC calculation equation (excluding uncertainty correction, see equation 5.1).

# 5.2 Requirements for robust quantification of net carbon removal

- 5.2.1 Continued in-field measurements are required from the CO<sub>2</sub> Removal Supplier in order to quantify the amount of CO<sub>2</sub> sequestered (section 6, section 11.2).
- 5.2.2 The CO<sub>2</sub> Removal Supplier shall meter, quantify, and keep records of the parameters needed to quantify the CO<sub>2</sub> removal. This includes, but is not limited to, the quantity of weathering material extracted and applied, the direct use of energy and fuels, and other greenhouse gas emissions from the process. These data must in particular be available to the Auditor, for the Production Facility Audit and Output Audits.

- 5.2.3 The CO<sub>2</sub> Removal Supplier shall assure the quality of measurements by applying appropriate quality control systems and procedures (section 10.3). This includes but is not limited to proper instrument calibration and data recording in reliable data systems.
- 5.2.4 The CO<sub>2</sub> Removal Supplier shall provide a written description of the approach used to quantify the weathering process and the expected carbon removal, in accordance with the requirements defined in this methodology. The description shall encompass both empirical quantification as well as any site-specific modeling (if applicable) of the weathering process (section 9).
- 5.2.5 Based on the results of an LCA analysis (section 7) and a scientifically justified estimation of the expected carbon removal over time, the CO<sub>2</sub> Removal Supplier must be able to present a net-negative overall carbon footprint for the cradle-to-grave activity, for eligibility of the ERW activity.
- 5.2.6 The CO<sub>2</sub> Removal Supplier shall quantify the overall uncertainty of the net CO<sub>2</sub> removal activity based on the combined uncertainty of the components included in equation 5.1 (see section 10.5).
- 5.2.7 The CO<sub>2</sub> Removal Supplier shall calculate the amount of sequestered carbon in the form of CO<sub>2</sub> Removal Certificates (CORCs) for each monitoring period, as per the requirements detailed in this Methodology.
- 5.2.8 The CO<sub>2</sub> Removal Supplier shall have in place, maintain, and utilize an information system to keep records of any events affecting the amount of CORCs resulting from the Enhanced Rock Weathering activity.<sup>45</sup> These records shall include time stamped, quantitative information such that their effect on the Output volume of the monitoring period can be quantified. These records shall be available to the Auditor, for the Production Facility Audit and Output Audits.

# 5.3 Overall equation

5.3.1 The overall number of CORCs (i.e., the total net amount of CO<sub>2</sub> removed) during a monitoring period shall be calculated as follows (see figure 5.1 for an illustration):

$$CORCs = F_c \times (C_{stored} - C_{baseline} - C_{loss} - E_{project} - E_{leakage})$$
 (5.1)

<sup>&</sup>lt;sup>45</sup> Examples of such events include any deployment or loss events, as well as the construction or replacement of any facilities, machinery or equipment (which would affect overall supply chain emissions).

Variable	Description	Unit
CORCs	Net amount of CO2 equivalents removed by the enhanced	tCO2e
	weathering activity.	
Fc	Factor of conservativeness calculated based on the total uncertainty	unitless
	in the net CO2 removal activity in accordance with the requirements	
	in section 10.5 (see in particular rule 10.5.3)	
$C_{stored}$	Gross amount of CO2 stored via weathering of the applied rock in	tCO2e
	the application sites. Further requirements on the calculation of this	
	term are given in section 6.1.	
$C_{baseline}$	Gross amount of CO2 stored via natural weathering in the control	tCO2e
	sites and via natural weathering of the untreated weathering	
	material. Further requirements on the calculation of this term are	
	given in section 6.2.	
$C_{loss}$	Total re-emissions or losses of the sequestered CO <sub>2</sub> as a result of	tCO2e
	subsequent biological uptake or chemical reactions in the	
	environment following the initial weathering. Further details and	
	requirements on the calculation of this term are given in section 6.3.	
$E_{project}$	Total amount of CO <sub>2</sub> -eq that is emitted along the supply chain of the	tCO <sub>2</sub> e
	removal activity. Further requirements on the calculation of this	
	term are given in section 7.	
$E_{leakage}$	The amount of CO <sub>2</sub> -eq emitted indirectly due to unmitigated	tCO2e
	negative ecological, market, and activity-shifting leakage resulting	
	from the Enhanced Rock Weathering activity. Further requirements	
	on the calculation of this term are given in section 8.	

The subsequent sections of this Methodology will follow eq. 5.1 by describing how C<sub>stored</sub>, C<sub>baseline</sub>, and C<sub>loss</sub> (section 6), project emissions (E<sub>project</sub>, section 7), and indirect emissions (E<sub>leakage</sub>, section 8) are determined. This is followed by section 9, which describes the monitoring program necessary for this, and section 10, which describes the sampling, measurements, and uncertainty quantification underlying this monitoring program.

# 6 Determination of stored carbon, baseline carbon removal, and carbon loss

# 6.1 Carbon stored ( $C_{stored}$ )

The term  $C_{stored}$  describes the gross amount of carbon dioxide sequestered into carbonate and bicarbonate ions through weathering of the applied material and exported from the NFZ to the FFZ. It also includes any precipitation of solid carbonate minerals (pedogenic carbonates) within the NFZ (section 1.5, section 11.2).

The CO<sub>2</sub> Removal Supplier needs to use two different measurement approaches (one quantification approach and one validation approach) to assess and quantify the amount of carbon sequestered within the field site (see rule 11.3.1). The primary quantification approach will be used to calculate  $C_{stored}$  as part of the CORC calculation, whereas the secondary *validation* approach is required for the purpose of confirming the accuracy of the primary approach. Thus, the results from the validation approach are not used as part of the CORC calculation but to validate the primary quantification approach and any associated carbon removal claims.

- 6.1.1 The quantification of  $C_{stored}$  shall be based on measurement of weathering signals at the application site(s).
  - (a) Measurements shall be conducted utilizing eligible quantification and validation approaches as further described in section 11.3 (see in particular rule 11.3.1) and summarized in table 6.1.
  - (b) The weathering signals shall be measured at least at the beginning ( $t_0$ ) and end ( $t_1$ ) of a monitoring period.
  - (c) To quantify  $C_{stored}$ , weathering signals shall be converted into removed carbon dioxide based on the stoichiometry of the underlying chemistry<sup>46</sup> in accordance with the chosen quantification method, as further described in section 11.3 (see in particular eqs. 11.14-11.50).

<sup>&</sup>lt;sup>46</sup> For example, if cations leached from the NFZ are used as the weathering signal, 1 mol of CO<sub>2</sub> is sequestered for each mole-equivalent cation charge lost from the NFZ (eq. 1.1). For carbonate mineral formation following silicate weathering (i.e., not accounting for any carbonates in the feedstock), 1 mol of CO<sub>2</sub> is sequestered for each mole of CaCO<sub>3</sub> that is formed within the NFZ as a consequence of the Enhanced Rock Weathering activity (eq. 1.4).

**Table 6.1.** Overview of eligible quantification and validation approaches for C<sub>stored</sub> measurements and applicable loss terms (section 6.3) associated with each.

Туре	Approach	Description	Applicable losses	Scientific reference	Quantification or validation
Soil	A1 - CATwm	Tracking weathering material	LOSSplant, LOSSacid, LOSSrivers, LOSSocean, (LOSSadsorb*, LOSScarbonate*)	Reershemius et al., 2023	Quantification/ validation
JUII	A2 - CATti	Tracking weathering material and immobile trace elements	LOSSplant, LOSSacid, LOSSrivers, LOSSocean, (LOSSadsorb*, LOSScarbonate*)	Reershemius et al., 2023	Quantification/ validation
	A3 - CATporewater	Tracking cations dissolved in soil pore water	Lossacid, Lossrivers, Lossocean	Amann et al. 2020	Quantification/ validation
Water	A4 - BICporewater	Tracking of bicarbonate + carbonate ions in soil pore water as alkalinity (4a) or DIC (4b)	LOSSrivers, LOSSocean	Amann et al., 2022; McDermott et al., 2024	Quantification/ validation
	A5 - CATresin	Tracking cations sorbed into a resin (from pore water)	LOSSacid, LOSSrivers, LOSSocean	-	Validation
	A6 - CAT <sub>sat</sub>	Tracking cations from soil water extracted after water saturation and centrifugation	Lossplant, Lossacid, Lossrivers, Lossacean	Skov et al. (submitted)	Quantification/ validation
Soil carbonate	A7 - SICsoil	Tracking cations reprecipitated as calcium carbonate	-	Haque et al., 2020; Haque, Santos, et al., 2019; Jariwala et al., 2022; Khalidy et al., 2021	Quantification (of soil carbonate**)

<sup>\*</sup> Loss term applicable if soil sample pre-treated with mild extractant (e.g., ammonium acetate) prior to C<sub>stored</sub> analysis.

# 6.2 Baseline ( $C_{baseline}$ )

C<sub>baseline</sub> represents an estimate of the carbon dioxide sequestration that would have occurred without the ERW activity. It has two components:

- Cbaseline-[feedstock], the counterfactual weathering of feedstock had it not been spread out on fields by the CO<sub>2</sub> removal supplier; and
- Cbaseline-[field], the carbonic-acid weathering in application site soil that would have naturally occurred without the ERW activity.

<sup>\*\*</sup> Soil carbonate quantification via SIC<sub>soil</sub> is independent from and parallel to the other quantification and validation approaches, see rules 11.3.1, 11.3.9.

As such, C<sub>baseline</sub> is equivalent to the "counterfactual" or the "business-as-usual" scenario (see also section 11.1).

6.2.1 The amount of baseline CO<sub>2</sub> sequestration in the absence of the ERW activity (C<sub>baseline</sub>) shall be calculated as follows:

$$C_{baseline} = C_{baseline-[field]} + C_{baseline-[feedstock]}$$
 (6.1)

Variable	Description	Unit
$C_{baseline-[field]}$	Field-component of baseline CO2 sequestration	tCO <sub>2</sub> e
	associated with the ERW activity. It is measured as	
	the weathering signal at control sites.	
$C_{baseline-[feedstock]}$	Feedstock-component of baseline CO2 sequestration	tCO2e
	associated with the ERW activity. It represents the	
	CO2 that would have been sequestered by weathering	
	of the feedstock material without the ERW activity.	

#### Counterfactual in-field weathering Cbaseline-[field]

- 6.2.2 Control sites (see section 11.1) shall be used to determine C<sub>baseline-[field]</sub>, i.e., the in-field component of C<sub>baseline</sub>, which also includes counterfactuals such as agricultural liming (rule 11.1.5, rule 11.1.6).
- 6.2.3 The quantification of C<sub>baseline-[field]</sub>, shall be based on measurement of weathering signals at the control site using quantification approaches as described in section 11.2 and summarized in table 6.1.
- 6.2.4 The weathering signal at the control sites shall be measured at least at the beginning ( $t_0$ ) and end ( $t_1$ ) of a monitoring period in order to calculate C<sub>baseline-[field]</sub> as appropriate for the applied quantification and validation approach (see eqs. 11.14-11.50, section 11.3). The same quantification and validation approaches shall be used on control sites as on the corresponding application sites.
- 6.2.5 If the estimation of  $C_{baseline-[field]}$  yields a negative value (i.e., suggesting that control sites are a  $CO_2$  source to the atmosphere), the value  $C_{baseline-[field]} = 0$  t  $CO_2$ e shall be used instead in the CORC equation.

#### Counterfactual feedstock weathering C<sub>baseline-[feedstock]</sub>

In addition to baseline weathering occurring on the field site, C<sub>baseline</sub> includes counterfactual weathering of rock material that would have occurred had the rock material not been treated (e.g., ground) and spread out on the application sites as feedstock, C<sub>baseline-[feedstock]</sub>.

- 6.2.6 The CO<sub>2</sub> removal supplier must present an estimate of counterfactual feedstock weathering (C<sub>baseline-[feedstock]</sub>), defined as the amount of CO<sub>2</sub> (in tonnes) that the weathering material utilized in the project would have naturally sequestered over the course of 50 years following the start of the ERW activity, had the activity not occurred. The estimate must be conservative and be based on information gathered from either the CO<sub>2</sub> Removal Supplier's own scientific research or peer-reviewed scientific publications.
- 6.2.7 The counterfactual feedstock weathering estimate shall consider at least the effect of three (3) factors to the sequestration rate represented by Cbaseline-[feedstock]: mineralogy, physical form (including particle size) and likely storage conditions (including ambient CO<sub>2</sub> concentrations). The sequestration amount shall be estimated based on the physical form of the material (e.g., solid mineral, ground particles, or fine dust) it would have been in without the project's activities.
- 6.2.8 To perform the counterfactual feedstock weathering estimate, the CO<sub>2</sub> removal supplier may utilize e.g. average sequestration rates from scientific literature that are applicable to the external conditions under consideration. A full chemical kinetics simulation is not required.
- 6.2.9 The CO<sub>2</sub> Removal Supplier must utilize reasonable, conservative assumptions for variable factors such as likely storage conditions during the counterfactual feedstock weathering estimation period.
- 6.2.10 The counterfactual feedstock weathering estimate shall include a discussion of the level and sources of uncertainty in the amount of CO<sub>2</sub> sequestered.
- 6.2.11 The counterfactual feedstock weathering estimate shall only consider the effect of natural CO<sub>2</sub> sequestration of the feedstock material. Specifically, no deductions due to e.g. avoided emissions or any other project activities may be included. The baseline sequestration amount can therefore never be negative.
- 6.2.12 For inert feedstock materials, the counterfactual feedstock weathering estimate and its effects on the amount of CORCs can be ignored in cases where it is scientifically reasonable to assume that the amount of CO<sub>2</sub> sequestered naturally by the material would be 1% or less of the total amount sequestered by the project. However, it shall be the responsibility of the CO<sub>2</sub> Removal Supplier to present scientific evidence to support such an assumption.
- 6.2.13 The CO<sub>2</sub> Removal Supplier must present its counterfactual feedstock weathering estimate and the underlying assumptions and sources thereof to Puro experts for review. The reliability of the estimate shall be at the discretion of Puro experts.
- 6.2.14 Projects, where the baseline carbon sequestration from counterfactual feedstock weathering is estimated to be 50 % of C<sub>stored</sub> or more are not eligible to be credited under the Enhanced Rock Weathering methodology.

#### Eligibility threshold with respect to C<sub>baseline</sub>

6.2.15 For CORCs to be issued for a given monitoring period and homogeneous stratum,  $C_{stored}$  must exceed  $C_{baseline-[field]}$  to a statistically significant degree. The CO<sub>2</sub> Removal Supplier shall demonstrate statistical significance at the 95% confidence level using appropriate inferential statistical tests (e.g. t-test) to test the null-hypothesis that no weathering occurred.

# 6.3 Carbon losses ( $C_{loss}$ )

The parameter C<sub>loss</sub> represents feedstock loss to non-carbonic weathering processes (see section 1.5) and biogeochemical processes that reverse initial carbon dioxide sequestration caused by the added weathering material. Note that as further explained in section 4.1, carbon losses refer to re-emission pathways identified and accounted for prior to the CORC issuance, and are separate from reversals which refer to events that cancel, entirely or in part, the effects of an already issued CORC.

- 6.3.1 The CO<sub>2</sub> Removal Supplier shall identify, quantify and account for all relevant loss (reemission) pathways. The set of relevant loss pathways (see section 1.5) shall at least include the loss terms defined in subrules a and b, as applicable to the chosen quantification and validation approaches (see table 6.1):
  - (a) Near Field Zone (NFZ) loss pathways:
    - (i) Lossacid: Weathering of rock feedstock by acids other than carbonic acid (a.k.a. *non-carbonic acid weathering*, or *strong-acid weathering*)
    - (ii) Lossplant: Plant uptake of major cations (Ca<sup>2+</sup>, Mg<sup>2+</sup>, Na<sup>+</sup>, K<sup>+</sup>)
    - (iii) Lossadsorb: Cation adsorption onto soil particles
    - (iv)Losscarbonate: Secondary carbonate mineral formation
    - (v) Losssilicate: Secondary silicate mineral formation
  - (b) Far Field Zone (FFZ) loss pathways:
    - (i) Lossrivers: Losses from surface freshwater systems (e.g. rivers, lakes)
    - (ii) Lossocean: Losses from marine systems (e.g. seas, oceans)
- 6.3.2 The total greenhouse gas emissions due to loss pathways ( $C_{loss}$ ) shall be calculated for each applicable loss pathway as described in rules 6.3.3-6.3.11. First, applicable loss terms based in the NFZ shall be summed up as follows to derive  $C_{loss-NFZ}$ :

$$C_{loss-NFZ} = \sum_{i \in S} mCO_2 e_i \tag{6.4}$$

Next, the FFZ-based loss terms shall be applied to the NFZ-loss corrected sequestration sequentially as follows to derive  $C_{loss-FFZ}$ :

$$C_{loss-FFZ} = (C_{stored} - C_{baseline-[field]} - C_{loss-NFZ}) \times (1 - \prod_{i \in R} [1 - F_i])$$
 (6.5)

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Finally, the calculated losses from NFZ and FFZ shall be summed up as follows:

$$C_{loss} = C_{loss-NFZ} + C_{loss-FFZ} \tag{6.6}$$

Variable	Description	Unit
$C_{loss}$	Total losses of the sequestered CO <sub>2</sub> as a result of subsequent chemical	tCO2e
	reactions in the environment following the initial weathering.	
$C_{loss-NFZ}$	Losses of sequestered CO2 as a result of subsequent chemical reactions in	tCO2e
	the NFZ following the initial weathering. Includes loss from the pathways	
	Lossacid, Lossplant, Lossadsorb, Losscarbonate, and Losssilicate as applicable.	
$C_{loss-FFZ}$	Total losses of the sequestered CO <sub>2</sub> as a result of subsequent chemical	tCO2e
	reactions in the FFZ following the initial weathering. Includes loss from the	
	pathways Lossrivers and Lossocean.	
$mCO_2e_i$	Total mass of GHGs emitted from NFZ loss pathway i	tCO2e
$F_i$	Percentage loss factor associated with the FFZ loss pathway i (either	%
	riverine or ocean losses), calculated as a percentage of the sequestered	
	carbon entering the FFZ (i.e. [Cstored - Cbaseline-[field] - Closs-NFZ])	
i	Summation index (an element in the set of loss pathways $S$ or $R$ )	unitless
S	The set of relevant loss pathways from the NFZ (Lossacid, Lossplant, Lossadsorb,	unitless
	LOSScarbonate, LOSSsilicate)	
R	The set of relevant loss pathways from the FFZ (Lossrivers, Lossocean).	unitless

- 6.3.3 The CO<sub>2</sub> Removal Supplier shall quantify the total amount of CO<sub>2</sub> released from each applicable loss pathway ( $mCO_2e_i$  for NFZ-losses, or  $F_i$  for FFZ-losses, see rule 6.3.2) through measurement, modeling, or conservative estimation as further detailed in rules 6.3.4-6.3.11. Applicable loss pathways for each C<sub>stored</sub> quantification approach are listed in table 6.1. For loss pathways that are inapplicable to the utilized quantification approach, no measurements or estimations are necessary and the value  $mCO_2e_i = 0$   $tCO_2e$  shall be utilized.
- 6.3.4 For the loss pathway **non-carbonic acid weathering (Loss**<sub>acid</sub>), the CO<sub>2</sub> Removal Supplier shall quantify the value of  $mCO_2e_i$  through one of the following means:<sup>47</sup>
  - (a) Direct measurement of the concentrations of major anions in soil porewater (e.g., via ion chromatography, ISO 10304-1:2007) from the NFZ combined with an estimate of the total volume of water infiltrated into the soil (soil water flux,  $F_{sw}$ ).

<sup>&</sup>lt;sup>47</sup> Note that, as further explained in section 1.6, while non-carbonic acid weathering might contribute to avoided outgassing of biogenic CO<sub>2</sub> in the FFZ, such potential removals are not accounted for in this methodology, and the non-carbonic acid weathering is conservatively always treated as a loss term due to the infeasibility of accurately quantifying this effect.

- (i) The monitored major anions shall include nitrate ( $NO_{3}^{-}$ ), phosphate ( $PO_{4}^{3-}$ ), chloride ( $Cl^{-}$ ), sulfate ( $SO_{4}^{2-}$ ), as well as any other anions that are or can reasonably be considered as relevant to local soil chemistry, land management practices, and the weathering material utilized.
- (ii) Anion concentration estimates shall be based on samples taken at least every three months during the monitoring period, including at the beginning ( $t_0$ ) and end ( $t_1$ ) of the monitoring period at the base of the NFZ (see rule 11.2.8-11.2.10) using appropriate sampling methodology (section 11.1). If  $t_0$  samples are taken prior to feedstock application, the sulfur content of the feedstock (measured as per table 3.1) shall be added to this soil anion concentration estimate in proportion to the feedstock application rate.
- (iii) If initial screening at a given site indicates undetectable concentrations of any anion, future measurements may exclude those anions from analysis provided an absence of relevant environmental and agronomic changes, especially sulfur deposition and fertilizer application.
- (iv)Soil water flux ( $F_{sw}$ ) shall be estimated following the requirements in rule 11.3.6 d (see also eqs. 11.28 and 11.33).
- (v) Concentrations of a given anion (i) measured across a monitoring period on a given application or control site shall be averaged ( $C_i$ ) and multiplied with the charge (n) of the given anion and the soil water flux estimate ( $F_{sw}$ ) to estimate the non-carbonic acid loss represented by the vertical anion export flux ( $F_{acid-loss}$ ) out of the NFZ of the set of anions (S, including nitrate, phosphate, chloride, sulfate) in the following way, separately for control (contr) and application (appl) sites:

$$F_{acid-loss,contr} = \sum_{i \in S} \left( \frac{C_{i,contr} \times n_{i,contr} \times F_{sw} \times MW_{CO2}}{MW_{AN_i} \times 10^6} \right)$$
(6.7)

$$F_{acid-loss,appl} = \sum_{i \in S} \left( \frac{C_{i,appl} \times n_{i,appl} \times F_{sw} \times MW_{CO2}}{MW_{AN} \times 10^6} \right)$$
(6.8)

(vi) Next, the conservative assumption shall be made that each negative anion charge exported was balanced by the positive charge of a cation after weathering, representing non-carbonic acid weathering. Based on this, the net carbonic-acid weathering rate in the control sites ( $C_{baseline-[field]}$ ) may be reduced by the estimated non-carbonic acid weathering rate on control sites but only to the point where  $C_{baseline-[field]}$  still remains  $\geq 0$  following this correction. This control-site estimate may then be subtracted from the parallel estimate of non-carbonic acid weathering on corresponding application sites. The resulting, control-site corrected non-carbonic acid weathering estimate shall then be used as the value for  $mCO_2e_i$  representing **Loss**<sub>acid</sub>:

$$mCO_2e_{Loss-acid} = (F_{acid-loss,appl} - F_{acid-loss,contr}) \times t \times A)$$
 (6.9)

If the calculation in eq. 6.9 results in a negative value,  $mCO_2e_{Loss-acid}$  shall equal zero.

Variable	Description	Unit
$C_i$	Measured concentration (average across monitoring period) of a given anion <i>i</i> at application ( <i>appl</i> ) or control ( <i>contr</i> ) site	mol L-1
$n_i$	Charge of a given anion $i$ (e.g., $i = 2$ for $SO_{4^2}$ , $i = 1$ for $NO_{3^2}$ )	-
S	The set of anions measured and taken into account for non- carbonic acid accounting, normally including nitrate, sulfate, phosphate, and chloride.	-
$F_{sw}$	Soil water flux estimate at application (appl) or control (contr) site	L m <sup>-2</sup> yr <sup>-1</sup>
$MW_{CO2}$	The molecular weight of CO <sub>2</sub>	g/mol
$MW_{AN_i}$	The molecular weight of a given anion <i>i</i>	g/mol
F <sub>acid</sub> -loss,j	Non-carbonic acid loss represented by the vertical anion export flux from the NFZ, where $j$ = application site ( $appl$ ) or control site ( $contr$ ).	tCO <sub>2</sub> e m <sup>-2</sup> yr <sup>-1</sup>
t	Duration of the monitoring period	yr
A	Application site area represented by this calculation	m <sup>2</sup>
$mCO_2e_{Loss-acid}$	Total mass of GHGs emitted from NFZ loss pathway Lossacid	tCO2e

(b) Indirect measurement of the concentrations of major anions in soil porewater combined with an estimate of the total volume water infiltrated into the soil. Such indirect estimates may be derived by subtracting [bicarbonate+carbonate] concentrations from cation concentrations after measuring each in porewater. The result of this subtraction may be assumed to represent major anions representing non-carbonic acidity, provided that the same requirements set above for direct anion concentration measurements are met, specifically sampling time points and comparison between control and application site.

- (c) A conservative estimation following the approach outlined by Dietzen & Rosing (2023) for determining the proportion of weathering by sources of acidity other than carbonic acid via a calculation of the carbonate system speciation based on any two parameters from the carbonate system measured in the soil. A conservative estimate of pCO<sub>2</sub> =  $1000 \mu$ atm (Dietzen & Rosing, 2023) may be used instead of measuring this parameter.
- 6.3.5 For the loss pathway **plant uptake of major cations (Loss**<sub>plant</sub>), the CO<sub>2</sub> Removal Supplier shall quantify the value of  $mCO_2e_i$  through direct measurement of the total base cation content of above-ground plant biomass (after digestion and appropriate cation concentration measurement: EPA Method 3050B, AOAC Official Method 975.03) coupled with an estimate of the total plant biomass yield of the field.
  - (a) This quantification of the loss shall be done separately for control sites and application sites and the value for  $\mathbf{Loss_{plant}}$  determined on control sites shall be subtracted from the value for  $\mathbf{Loss_{plant}}$  determined on application sites in order to quantify  $mCO_2e_i$ . If  $\mathbf{Loss_{plant}}$  on control sites is greater than on application sites, the value for  $mCO_2e_i$  shall be zero.
  - (b) For annual crops, plant samples shall cover the entire portion of the plant (typically the entire above-ground portion, but also the below-ground portion if actively removed from soil samples for C<sub>stored</sub> quantification) that contains cations that have escaped sampling for C<sub>stored</sub> quantification by incorporation into plant biomass. For perennial crops, the plant samples shall cover new growth that occurred during the monitoring period combined with an estimate of the net new biomass (Battles et al., 2014).
- 6.3.6 The loss pathway of **adsorbed cations within the NFZ (Loss**<sub>adsorb</sub>) describes cations adsorbed to surface sites of soil particles, preventing their export from the NFZ. Of the C<sub>stored</sub> quantification approaches described in section 11.3, none will create a false positive signal caused by cations adsorbed within the NFZ if sampling covers the entire NFZ. Therefore, the value  $mCO_2e_i = 0 \ tCO_2e$  may be utilized except under circumstances that require a **Loss**<sub>adsorb</sub> correction, which include:
  - Situations where, as part CAT<sub>WM</sub> or CAT<sub>Ti</sub> analysis, exchangeable cations are flushed from samples for C<sub>stored</sub> quantification using mild extractants such as ammonium acetate, Loss<sub>adsorb</sub> needs to be accounted for separately.

If a **Loss**<sub>adsorb</sub> correction is necessary, the value of  $mCO_2e_{Loss-adsorb}$  shall be determined by the quantification of exchangeable cations after soil extractions with mild extractants (e.g., ammonium nitrate, ammonium acetate) and following peer-reviewed or standard protocols, including ISO 23470:2018, ISO 11260:2018, Dietzen et al. (2018), and Kelland et al. (2020). The value for  $mCO_2e_{Loss-adsorb}$  shall derive from subtracting the increase in exchangeable cation charges during the monitoring period (from  $t_0$  to  $t_1$ )

in control site samples from the increase in parallel application site samples. If this subtraction results in a negative value,  $mCO_2e_{Loss-adsorb}$  shall equal zero. It should be noted that cation adsorption can significantly delay the cation export from the NFZ and, therefore, monitoring it may be recommendable even if it does not interfere with carbon accounting (Kanzaki et al., 2025).

- 6.3.7 The loss pathway **secondary carbonate mineral formation (Loss**<sub>carbonate</sub>) describes the loss of 1 mol CO<sub>2</sub> per mol CaCO<sub>3</sub> (or equivalent carbonate mineral) formed inside the NFZ (see eq. 1.5). Of the C<sub>stored</sub> quantification approaches described in section 11.3, none will create a false positive signal caused by secondary carbonate precipitation if sampling covers the entire NFZ. Therefore, the value  $mCO_2e_i = 0 \ tCO_2e$  may be utilized except under circumstances that require a **Loss**<sub>carbonate</sub> correction, which include:
  - Situations where, as part CAT<sub>WM</sub> or CAT<sub>Ti</sub> analysis, exchangeable cations are flushed from samples for C<sub>stored</sub> quantification using mild extractants such as ammonium acetate. This practice may partially dissolve calcite and so its employment warrants quantification of SIC decrease (falsely indicating additional cation loss from NFZ) in the soil sample as a result of this practice.

If a **Loss**<sub>carbonate</sub> correction is necessary, the value of  $mCO_2e_{Loss-carbonate}$  shall be determined by the quantification of soil inorganic carbon (SIC) from bulk soil samples taken just after feedstock application ( $t_0$ ) and at the end of the monitoring period ( $t_1$ ) using appropriate methods, including thermogravimetric analysis (TGA), calcimetry (ISO 10693:1995), or dry combustion (ISO 10694:1995). The value for  $mCO_2e_{Loss-carbonate}$  shall derive from subtracting the increase in SIC during the monitoring period ( $t_0$  to  $t_1$ ) in control site samples from the SIC increase in parallel application site samples. If this subtraction results in a negative value,  $mCO_2e_{Loss-carbonate}$  shall equal zero.

For the loss pathway **secondary silicate mineral formation (Loss**<sub>silicate</sub>), the value  $mCO_2e_i = 0 \ tCO_2e$  may be utilized as all eligible quantification approaches inherently correct for this loss term within the NFZ provided that samples cover the entire NFZ depth (rule 11.2.10). Despite this, there is a chance of losses from silicate mineral formation occurring below the NFZ but as of the writing of this document (October 2025), no operationally viable method is available to quantify this loss term (Mills et al., 2024). Thus, in order to minimize the risk of unaccounted losses from secondary silicate mineral formation, the CO<sub>2</sub> removal supplier should avoid field sites with high propensity for secondary silicate mineral precipitation, especially slow-draining soils (Wilson, 1999).

- 6.3.9 To assess the impact of the loss pathway **losses from surface freshwater systems** to their production facility (**Loss**<sub>rivers</sub>), the CO<sub>2</sub> Removal Supplier shall assess its two components, *i) carbonate mineral formation*, and *ii) CO<sub>2</sub> degassing due to carbonate system equilibration* in rivers downstream from the field site and account for it as follows:
  - (a) SI<sub>calcite</sub> (eq. 1.7), pH, and the share of CO<sub>2</sub> in DIC shall be quantified based on empirical data (see subrules b-c) that include at least temperature, pH, Ca<sup>2+</sup> concentrations, and either DIC concentration or alkalinity based on samples taken at the following sites:
    - (i) Representative samples from tile drainages at sites with tile drainage systems.
    - (ii) River water immediately (or as close as possible<sup>48</sup>) downstream of the field site. If different parts of a field site drain into different streams or rivers, samples shall be taken at least at the nearest point downstream where all these rivers meet but ideally additional samples should be taken also at the upstream branches closer to the field site outflows.
    - (iii)In water from the catchment's highest-order river. If groundwater from a given field site drains directly into the ocean, the supplier shall measure SI<sub>calcite</sub> and the share of CO<sub>2</sub> in DIC in the coastal ocean water near the groundwater discharge site.
  - (b) For the assessments defined in subrule a, any available river water quality datasets of sufficient scientific quality (e.g., public monitoring program by the United States Geological Survey) containing data from samples taken ≤10 years before the start of the crediting period shall be analyzed. Alternatively, or if such datasets do not exist for relevant sites, the CO₂ Removal Supplier shall take the necessary measurements using appropriate river water sampling and measurement approaches.
  - (c) These datasets or measurements shall include at least two annual measurement points for each relevant parameter at the two river sites (subrule a) and at least two annual measurement points shall be from contrasting seasons defined by the local climatic zone: e.g., wet vs dry season in tropical climate, summer vs winter in temperate climate.

<sup>&</sup>lt;sup>48</sup> In exceptional cases where legal (e.g., private property access) or physical (e.g., natural barriers like rapids or canyons) prohibit sampling immediately downstream of the field site, an accessible sampling site further downstream as close to the field site as possible shall be identified on a case-by-case basis and requires approval by the Issuing Body.

- (d) Based on these data, the values representing the carbonate mineral formation and CO<sub>2</sub> degassing components of the **Loss**<sub>rivers</sub> loss term shall be determined as follows:
  - (i) If SI<sub>calcite</sub> <1.0 consistently at all downstream measurement points and seasons, the supplier may either use a 5% conservative estimate for the value of Loss<sub>rivers</sub> (Zhang et al., 2025) or apply an appropriate model to estimate CO<sub>2</sub> evasion due to carbonate system equilibration in downstream river systems (e.g., Zhang et al. 2025) and use the resulting estimate to determine the value of Loss<sub>rivers</sub>.
  - (ii) If pH >6.5 and SI<sub>calcite</sub> <1.0 consistently at all downstream measurement points and seasons, the supplier may either use a 2.5% estimate for the value of Loss<sub>rivers</sub> (Zhang et al., 2025) or apply an appropriate model to estimate CO<sub>2</sub> evasion due to carbonate system equilibration in downstream river systems (e.g., Zhang et al. 2025) and use this estimate to determine the value of Loss<sub>rivers</sub>.
  - (iii) If SI<sub>calcite</sub> >1.0 consistently at one or more downstream measurement points and seasons, the supplier shall use the river dataset to estimate CO₂ loss from carbonate mineral formation in the river segment(s) represented by this measurement point, assuming that carbonate precipitation stops at SI<sub>calcite</sub> ≤1.0. This estimate shall be added to a 2.5% estimate for the carbonate-system equilibration component to determine the value of **Loss**<sub>rivers</sub> in this case.
  - (iv) If pH ≤6.5 consistently at one or more downstream measurement points and seasons, the supplier shall use appropriate models (e.g., Zhang et al., 2025) to estimate CO<sub>2</sub> evasion due to carbonate system equilibration in downstream river systems. This estimate shall be used as the value of Loss<sub>rivers</sub> in this case.

Note: for the above assessments of SI<sub>calcite</sub> and pH in river water, "consistently" shall allow for the exclusion of individual measurements that can be deemed random outliers either based on a measurement inaccuracy or based on statistical analysis compared to the available time series of measurements at a given location.

6.3.10 For the pathway **losses from marine systems** the value of  $F_i = \mathbf{Loss_{ocean}}$  shall equal the percentage loss due the decrease in carbon uptake efficiency ( $\frac{\Delta C}{\Delta A'}$  eq. 1.8) of the ocean given local seawater chemistry, and is defined as follows:

$$Loss_{ocean} = 1 - \frac{\Delta C}{\Delta A} \tag{6.12}$$

Note that as per eq. 6.5, **Loss**<sub>ocean</sub> is applied subsequently to accounting for applicable NFZ losses and **Loss**<sub>rivers</sub>.

To determine this efficiency, the CO<sub>2</sub> removal supplier shall use appropriate oceanographic data (e.g., from public databases or scientific publications) to solve for  $\frac{\Delta C}{\Delta A}$  based on eq. 1.8. For these calculations:

- equilibrium conditions shall be assumed;
- ocean near-surface water data that best represents the seawater receiving the river water from the catchment containing the field site shall be the basis;
- appropriate tools shall be used, such as CO2SYS (E. Lewis & Wallace, 1998).

Alternatively, if the CO<sub>2</sub> removal supplier cannot assess the carbon uptake efficiency based on local oceanographic data, a conservative estimate of 20% shall be used to represent **losses from marine systems** (Kanzaki et al., 2023; Renforth & Henderson, 2017). In mathematical terms, this shall be implemented by solving eq. 6.12 after substituting the term  $\frac{\Delta C}{\Delta A}$  in eq. 6.12 with the value 0.8.

6.3.11 For any other potential loss pathways identified, besides those within the purview of rules 6.3.4-6.3.10, the CO<sub>2</sub> Removal Supplier shall provide a detailed description of the identified pathway and the method of quantification.

# 7 Determination of project emissions

### 7.1 Life cycle approach for the quantification of project emissions

- 7.1.1 The CO<sub>2</sub> Removal Supplier shall calculate the life cycle emissions resulting from the development and operations of the carbon removal activity using a cradle-to-grave modelling approach (i.e. upstream and downstream activities), and based on both:
  - (a) A life cycle assessment model (LCA model) of operational emissions (section 7.3), and
  - (b) A life cycle inventory (LCI) of embodied emissions (section 7.4).

The life cycle emissions shall cover the scope defined in the system boundaries (rule 7.2.2), adhere to the Monitoring Plan requirements (rule 9.2.2), and follow the general principles defined in ISO-14040/44 and the ISO-14064 series.

7.1.2 The CO<sub>2</sub> Removal Supplier shall calculate and report project emissions using eq. 7.1 as follows:

$$E_{project,MP} = E_{ops,MP} + E_{emb,MP} \tag{7.1}$$

Variable	Description	Unit
$E_{project,MP}$	Lifecycle emissions associated with the operation of the project during the	tCO2e
	monitoring period (MP) and the amortized portion of the lifecycle's	
	embodied emissions.	
$E_{ops,MP}$	Lifecycle operational emissions from materials and energy used by the	tCO2e
	project during the monitoring period.	
$E_{emb,MP}$	Amortized lifecycle embodied emissions associated with the production,	tCO2e
	use, and disposal of infrastructure and equipment assets and direct land	
	use changes.	

- 7.1.3 The LCA model shall be developed in a digital tool that enables complete and transparent verification of the calculations, from input activity data to selection of emission factors. The digital tool can either be:
  - (a) A spreadsheet LCA model using the template provided by Puro.earth or a similar spreadsheet as long as formulae and cell referencing are transparent.
  - (b) A non-spreadsheet tool (e.g., dMRV platforms) provided that at least the same level of transparency and verifiability is achieved by the tool as enabled by the Puro.earth LCA spreadsheet model, and that data and model structure can be inspected and extracted by a third party.

- 7.1.4 The CO<sub>2</sub> Removal Supplier shall include with the Project Description (PD) a description of the LCA model, including the operational life cycle inventory, outlining each emission source, detailing what it represents as required by the data collection requirements (see section 10.4), and including:
  - (a) Relevant activity data (AD) included in the monitoring plan (section 9.2), and how it will be monitored and measured, along with explanation of the application of a cut-off criteria from the monitoring process, if applicable (see rule 7.1.6).
  - (b) Emission factors (EF) chosen (see rule 7.1.8).

### Use of data estimates in LCA models

- 7.1.5 The CO<sub>2</sub> Removal Supplier may leave out from the monitoring plan individual activities or emission sources that contribute less than 1% of total LCI emissions quantification and assign a conservative value in its place, in order to simplify the development of the LCA model and the data collection process and use data estimates in its place (see section 9.2), considering the following:
  - (a) Identify which individual activities or emission sources do not require monitoring and measurement of activity data from the operational life cycle inventory (LCI) model, which includes the following steps that the CO<sub>2</sub> Removal Supplier shall take:
    - (i) develop an inventory that lists all possible individual activities or emission sources for each unit process (see rule 7.2.2) and type of emissions sources (e.g. energy use, material use, waste treatment, direct emissions);
    - (ii) determine with the support of preliminary calculations which individual activities or emission sources are expected to represent less than 1% of the overall inventory emissions and will not change significantly during project operations;
    - (iii) select from the activities determined in the previous step those that would cover up to 5% of overall inventory emissions and assign fixed conservative activity values to those activities in order to exclude them from the monitoring process but still account for them in the inventory calculation.

- (b) The selection of any activity or emission sources from the LCI that will be excluded from the monitoring process shall be documented in the LCA Model Description and can be challenged by the third-party auditors during Facility Audit or Output Audits alike. For example, the auditor may compare the LCI data with similar processes or available emissions databases to determine the plausibility of completeness of the proposed inventory.
- (c) The following elements are considered out-of-scope for the purposes of LCA modeling and therefore do not need to be included in the LCA Model:
  - (i) site selection and feasibility studies, non-recurring R&D activities;
  - (ii) staff transport (e.g., business travel and employee commuting);
  - (iii)non-production related products, which include office furniture and supplies, IT support, and janitorial and cleaning services.

#### Modeling of secondary resources and cut-off criteria

7.1.6 If waste, recycled or post-consumer secondary resources are used as input to the activity (e.g. industrial waste materials such as slags or mine tailings), it is permissible and recommended to apply the cut-off system model approach<sup>49</sup> for waste, recycled and post-consumer secondary products in the LCA. Specifically, the environmental burdens from disposal of such resources shall be excluded from the system boundary, but the supply, transformation and handling of the secondary resources must be included from the start of the end-of-waste point.<sup>50</sup>

### Changes to the LCA model during the crediting period

7.1.7 The LCA Model and its Description may be updated by the CO<sub>2</sub> Removal Supplier during the course of the crediting period to reflect changes that have occurred within the operations of the Production Facility. Any such change must be declared and reported at the next Output Audit, during which the updated LCA Model and its Description shall be re-validated by the third-party auditor.

### Type of emission factors

7.1.8 The emission factors used in the LCA shall comply with the following elements:

<sup>&</sup>lt;sup>49</sup> Description of the cut-off system model is available on the website of the ecoinvent life cycle database. This approach can also be described as a "polluter-pay" approach, as the emissions from waste treatment are attributed to the previous life cycle.

<sup>&</sup>lt;sup>50</sup> This aligns with the European Commission 2023 targeted revision of the Waste Framework Directive and the proposal to include end-of-waste criteria. Accessed on 15 May 2025: https://environment.ec.europa.eu/topics/waste-and-recycling/waste-framework-directive\_en#end-of-waste-criteria

- (a) include at least the contribution of major greenhouse gases (fossil CO<sub>2</sub>, biogenic non-renewable CO<sub>2</sub>, CH<sub>4</sub>, N<sub>2</sub>O).
- (b) include a full-scope of emissions (i.e., including upstream and downstream emissions, or so-called supply chain emissions, as opposed to emission factors used for greenhouse gas inventory purposes). Note that it is common to use multiple emission factors to represent the full-scope of an activity, e.g. one factor for direct emissions and one or several factors for upstream and downstream emissions.
- (c) do not include any recycling or substitutions terms (i.e. diminishing the impact of the activity)
- (d) be geographically appropriate to the location of the activity.

Further, the CO<sub>2</sub> Removal Supplier may use emission factors from publicly available or commercial databases or developed by peer-reviewed studies complying with the above elements.

**REMARK:** Many public LCA data sources for emission factors, as well as literature data, have not yet been updated to reflect the changes of GWP<sub>100</sub> from the latest IPCC Assessment Report. Those changes are however deemed minor, and CO<sub>2</sub> Removal Suppliers should strive to use the most up-to-date emission factors available.

#### Cooperation between operators for LCA

7.1.9 The CO<sub>2</sub> Removal Supplier shall coordinate data collection and LCA modeling with any external operators<sup>51</sup> to the level necessary and extent possible to ensure compliance with this methodology and the Puro Standard requirements. In case when primary data cannot be collected from external operators, the CO<sub>2</sub> Removal Supplier may use conservative estimates including uncertainty values provided that their source and assumptions are clearly referenced in the corresponding LCI and monitoring plan following the format described in table 9.1.

# 7.2 Scope of Project Emissions

7.2.1 The CO<sub>2</sub> Removal Supplier shall define the functional unit of the ERW activity by determining all process flows and emissions associated with the application to soil and weathering of one (1) metric tonne of weathering material, with specific material granulometry, and soil incorporation process and depth, for the purpose of removing CO<sub>2</sub> from the atmosphere.

<sup>&</sup>lt;sup>51</sup> Data required for performing the LCA of an ERW activity originates from multiple parties operating in the feedstock production (i.e., quarry), transportation, and on-site application.

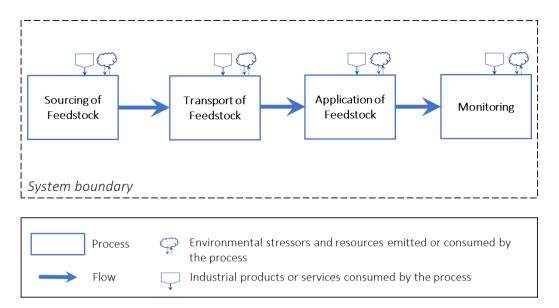


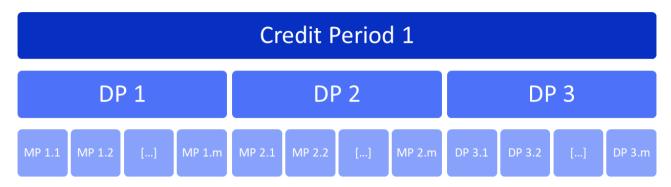
Figure 7.1. Generic process boundaries for ERW in soils.<sup>52</sup>

- 7.2.2 The **system boundaries** of the LCA model of the ERW activity shall include the four main unit processes represented in figure 7.1, and defined as follows:
  - (a) **Sourcing of Feedstock:** This process includes, e.g., the mining of rock (in case of natural weathering material use) and its processing for deployment on agricultural soils. It may consist of all operations required for extracting and processing the material to its final size and granulometry (crushing, grinding, milling), including infrastructure requirements, material and energy consumption, as well as waste treatment. This process terminates with crushed material ready for application at the processing location.
  - (b) Transport of Feedstock: This process includes all operations required for supplying the ground material to its site of application, including loading, transportation, and unloading, as well as infrastructure requirements (road, truck, fuel supply-chain), when applicable and in alignment with the GLECv3.1 framework. Calculation of transport-related emissions shall include, whenever applicable, emissions from unladen backhaul transport (empty return trips). This terminates with processed material ready for application at the site.
  - (c) **Application of Feedstock:** This process refers to all operations required for spreading and/or incorporation of the processed material to the site. This includes machinery and fuel use. This terminates with processed material applied and incorporated to the soil at the application location.

<sup>&</sup>lt;sup>52</sup> Note that *i*) each process can be detailed in sub-processes, *ii*) additional transportation may be included in each process, *iii*) additional processes can be added as fit to the specific project.

- (d) **Monitoring:** This process refers to all operations required for monitoring the weathering process, including consumable sampling equipment, site visits, transportation of samples, but excluding laboratory analyses.
- 7.2.3 The **spatial dimension** of the ERW activity system shall be provided in a map or a geospatial vector data (shapefile) with the Project Description for the Production Facility Audit, and shall be defined in the LCA Model Description for the selection of spatially-relevant emission factors and activity data (see section 10.4). This includes the areas covered by the four unit processes, from feedstock sourcing, transport, application and monitoring. These may include the following:
  - (a) Mine location: the origin of the rock or waste must be specified.
  - (b) **Processing facility**: the site(s) of processing of the material must be specified.
  - (c) **Application sites**: the area and the geolocation of the field site as well as the associated catchment in which the stored carbon is likely to be transported and stored (soil, groundwater, aquifer, watershed, rivers, ocean entry point), shall be specified
- 7.2.4 The **temporal dimension** of the ERW activity system shall be defined in the LCA Model and LCA Model Description considering the GHG emissions accounting considerations of a crediting period and the fact that operational emissions (section 7.3) and embodied emissions (section 7.4) have taken place before the weathering of the weathering material and shall be accounted as follows:
  - (a) operational emissions are associated with the deployment period (DP) following a weathering material application event, and shall be amortized across the "m" number of monitoring periods (MP) within its corresponding deployment period;
  - (b) embodied emissions are associated with the whole ERW activity and shall be amortized as required in rule 7.4.5.

**Note**: During a crediting period, feedstock may be applied several times. Each application of weathering material marks the start of a new deployment period that lasts until a new weathering material application event or the end of the crediting period. Moreover, a deployment period may be subdivided into multiple monitoring periods for the purpose of carbon removal accounting and CORC issuance. Figure 7.2 provides an illustration of the relationship between crediting period, deployment period, and monitoring period.



**Figure 7.2.** Example of the temporal dimensions of an ERW activity. DP: deployment period. MP: monitoring period.

7.2.5 The project emissions ( $E_{project,DP}$ ) shall be updated in each deployment period with actual measured and recorded activity data (such as transport distances as well as fuel, energy, and material consumption).

### 7.3 Quantification of operational emissions

- 7.3.1 The CO<sub>2</sub> Removal Supplier shall develop an operational LCI, accounting for the **operational emissions** of the three main unit processes described in rule 7.2.1, and calculate the **operational emissions** associated with the energy used to operate facilities, machinery, or other types of equipment as well as the material inputs (e.g., water, chemicals, packaging), waste treatment, and transportation (e.g., weathering material transportation) necessary for the carbon removal activity.
- 7.3.2 The emissions from the activities covered in the operational LCI shall be measured and reported during the monitoring period following eq. 7.2 and be possible to link to the amounts of feedstock used and weathered during the monitoring period.

$$E_{ops,DP} = E_{sourcing} + E_{transport} + E_{application} + E_{monitoring}$$
 (7.2)

Variable	Description	Unit	
$E_{ops,DP}$	Lifecycle operational emissions from materials and energy used	tCO2e	
	for the application of a weathering material event and associated		
	with a deployment period "DP".		
$E_{sourcing}$	Operational lifecycle emissions associated with sourcing of	tCO2e	
	weathering material and its processing for its application.		
$E_{transport}$	Operational lifecycle emissions associated with transport of		
	weathering material from the sourcing site to the application site.		
$E_{application}$	Operational lifecycle emissions associated with the application of	tCO2e	
	weathering material to the application site.		
$E_{monitoring}$	Operational lifecycle emissions associated with monitoring of	tCO2e	
	weathering material, including sample collection and transport to		
	laboratory for analysis.		

- (a) In cases where the counterfactual baseline scenario includes agricultural liming (see also rule 6.2.2), the operational emissions (i.e., the sourcing, transport and application of agricultural lime) associated with such liming during the monitoring period shall be quantified and deducted from E<sub>ops,DP</sub>.
- 7.3.3 Operational emissions shall be reported evenly over a period of time in line with its corresponding monitoring period (see rule 7.2.4), or the lifetime assumption of the Production Facility, whichever is shorter. To calculate the amount of operational emissions to amortize per monitoring period use eq. 7.3 as follows:

$$E_{ops,MP} = \frac{E_{ops,DP}}{m} \tag{7.3}$$

- (a) Alternatively, the CO<sub>2</sub> Removal Supplier may decide to amortize all operational emissions earlier, for example, during the first monitoring period, if requested by a third party (e.g., investor or buyer).
- (b) If the project is terminated prior to complete amortization of its attributable operational emissions, the remaining unamortized operational emissions are considered a liability and the CO<sub>2</sub> Removal Supplier shall settle the outstanding operational emissions by retiring CO<sub>2</sub> Removal Certificates (CORC) of similar permanence in equal amount to the outstanding amount of emissions on one (1) tCO<sub>2</sub>e to one (1) credit unit equivalence.

Variable	Description	Unit
$E_{ops,MP}$	Lifecycle operational emissions from materials and energy	tCO <sub>2</sub> e
	used by the project during the monitoring period.	
$E_{ops,DP}$	Lifecycle operational emissions from materials and energy	tCO <sub>2</sub> e
	used for the application of a feedstock event and associated	
	with a deployment period "DP".	
m	Number of monitoring periods between application of	Unitless
	feedstock on the site. "m" shall be equal or less than the	
	number of monitoring periods defined under the monitoring	
	period following an application event but preceding a	
	subsequent application event or the end of the crediting	
	period.	

### 7.4 Quantification of embodied emissions

7.4.1 The CO<sub>2</sub> Removal Supplier shall calculate the **embodied emissions (E<sub>emb</sub>)** of the project for project validation, and submit for audit:

- (a) A life cycle inventory of embodied emissions, accounting for the emissions of the foreground infrastructure and equipment, that includes the carbon emitted in the fabrication, construction, and demolition of infrastructure and/or equipment assets (E<sub>infra</sub>), and in direct land-use conversion (E<sub>dLUC</sub>) associated with the production facility and supporting infrastructure, when applicable (rules 7.4.2 to 7.4.4).
- (b) Schedule of amortization of embodied emissions (E<sub>emb,MP</sub>) to be included with the project emissions calculation (eq. 7.1) during the corresponding monitoring period based on the amortization rule 7.4.5.
- 7.4.2 The life cycle inventory of embodied emissions shall be estimated using eq. 7.4:

$$E_{emb} = E_{infra} + E_{dLIIC} \tag{7.4}$$

Variable	Description	Unit	
$E_{emb}$	Sum of lifecycle emissions associated with infrastructure and		
	equipment assets and direct land use changes.		
$E_{infra}$	Lifecycle emissions associated with infrastructure and equipment		
	assets.		
$E_{dLUC}$	Lifecycle emissions associated with direct land use changes.	tCO2e	

- 7.4.3 Embodied emissions shall account for the life cycle emissions of infrastructure and/or equipment (E<sub>infra</sub>) as follows:
  - (a) The calculation of embodied emissions shall be cradle-to-grave, including all steps from material extraction to waste disposal, and may follow as general guidance: EN 15804+A2,<sup>53</sup> EN 15978,<sup>54</sup> or ISO 21930:2017.<sup>55</sup>

<sup>&</sup>lt;sup>53</sup> EN 15804:2012+A2:2020 Sustainability of construction works - Environmental product declarations - Core rules for the product category of construction products.

<sup>&</sup>lt;sup>54</sup> EN 15978:2012 Sustainability of construction works - Assessment of environmental performance of buildings - Calculation method.

<sup>&</sup>lt;sup>55</sup> ISO 21930:2017 Sustainability in buildings and civil engineering works - Core rules for environmental product declarations of construction products and services.

- (b) Alternatively, recent monetary emission factors (e.g., kg CO₂e per USD spent) may be used as a proxy for estimating embodied emissions based on capital expenditure (CAPEX), provided that such factors are available in the countries where the facilities are built, or from other countries as proxy, if deemed sufficiently conservative. This approach may be based on an economic input-output life-cycle assessment (EIO-LCA).
- (c) The embodied emissions of operational pre-existing facilities shall not be accounted for in the project's embodied emissions. However, additional embodied emissions associated with the retrofit of the facility shall be accounted for.
- (d) In the event of an ownership change of an asset (e.g., trucks or agricultural machinery), the embodied emissions from the initial manufacturing shall be accounted to the pro-rata of its remaining lifetime. However, additional embodied emissions associated with the transportation, installation, or upgrading of the asset shall be accounted for in full.
- 7.4.4 Embodied emissions shall account for direct land-use (dLUC) conversion if land use has been changed for the construction of the Production Facility or any supporting infrastructure necessary for the operation of the carbon removal activity. To this end, the following rules shall apply:
  - (a) dLUC emissions shall be considered and included in the embodied LCI when the construction of the Production Facility and its supporting infrastructure entails land conversion.
  - (b) dLUC shall be assessed relative to the land area remaining in its historical state prior to the carbon removal project (new built or retrofit).
  - (c) dLUC shall include any loss of aboveground and belowground biogenic carbon stocks, relative to the historical state of the land. dLUC shall also include any greenhouse emissions arising during the land conversion such as emissions associated with land clearing by fire as these may include significant amounts of methane (CH<sub>4</sub>) and dinitrogen monoxide (N<sub>2</sub>O).
  - (d) These emissions shall be quantified using either the default values for land conversion available in the IPCC Guidelines for National Greenhouse Gas Inventories<sup>56</sup> (Tier 1), or country-specific values (Tier 2), or data specific to the project (Tier 3).

<sup>&</sup>lt;sup>56</sup> 2006 IPCC Guidelines for National Greenhouse Gas Inventories, Prepared by the National Greenhouse Gas Inventories Programme, Eggleston H.S., Buendia L., Miwa K., Ngara T. and Tanabe K. (eds).

(e) The calculation shall be performed using the eqs. 7.5 and 7.6 below:

$$E_{dLUC} = \frac{44}{12} \times (CS_B - CS_P) \times A + E_{conversion}$$
 (7.5)

where the carbon stock per unit area is defined as:

$$CS_X = C_{VEG_X} + C_{DOM_X} + SOC_X (7.6)$$

Variable	Description	Unit
$E_{dLUC}$	Absolute direct land use change associated with the construction of infrastructure.	
$CS_B$	Carbon stock per unit area associated with the baseline land use.	tC ha-1
$CS_P$	Carbon stock per unit area associated with the project land use.	
A	Area of land converted.	ha
$E_{conversion}$	Greenhouse gas emissions associated with the land use conversion activities, e.g. fuel usage for clearing the land, direct emissions from fire.	
$CS_X$	Carbon stock per unit area with the project or baseline land use, where subscript <i>X</i> indicates the type of land use.	
$C_{VEG_X}$	Above and below ground living biomass carbon stock.	tC ha-1
$C_{DOM_X}$	Dead organic matter or litter biomass carbon stock.	tC ha <sup>-1</sup>
$SOC_X$	Soil organic carbon stock.	tC ha-1

The variables  $C_{VEG_X}$ ,  $C_{DOM_X}$ , and  $SOC_X$  should be determined using the equations presented in volume 4 of the IPCC Guidelines for National Greenhouse Gas Inventories<sup>57</sup> and the EU Commission decision on guidelines for the calculation of land carbon stocks for the purpose of Annex V to Directive 2009/28/EC<sup>58</sup> (see also subrule d).

<sup>&</sup>lt;sup>57</sup> 2019 Refinement to the 2006 IPCC Guidelines for National Greenhouse Gas Inventories, Calvo Buendia, E., Tanabe, K., Kranjc, A., Baasansuren, J., Fukuda, M., Ngarize, S., Osako, A., Pyrozhenko, Y., Shermanau, P. and Federici, S. (eds).

 $<sup>^{58}</sup>$  2010/335/: Commission Decision of 10 June 2010 on guidelines for the calculation of land carbon stocks for the purpose of Annex V to Directive 2009/28/EC (notified under document C(2010) 3751).

7.4.5 Embodied emissions shall be amortized<sup>59</sup> evenly over a period of time in line with its first crediting period (10 years, see rule 2.2.6), or the lifetime assumption of the Production Facility, whichever is shorter. To calculate the amount of embodied emissions to amortize per monitoring period use eq. 7.7 as follows:

$$E_{emb,MP} = \frac{E_{emb}}{n} \tag{7.7}$$

Variable	Description	Unit
$E_{emb,MP}$	Amortized lifecycle embodied emissions associated with the production, use, and disposal of infrastructure and equipment assets and direct land use changes.	
$E_{emb}$	Sum of lifecycle emissions associated with infrastructure and equipment assets and direct land use changes.	
n	Number of monitoring periods under which the embodied emissions inventory will be amortized. "n" shall be equal or less than the number of monitoring periods defined under the crediting period.	

- (a) Alternatively, the CO<sub>2</sub> Removal Supplier may decide to amortize all embodied emissions earlier, for example, during the first monitoring period, if requested by a third party (e.g., investor or buyer).
- (b) If the project is terminated prior to complete amortization of its attributable embodied emissions, the remaining unamortized embodied emissions are considered a liability and the CO<sub>2</sub> Removal Supplier shall settle the outstanding embodied emissions by retiring CO<sub>2</sub> Removal Certificates (CORC) of similar permanence in equal amount to the outstanding amount of emissions on one (1) tCO<sub>2</sub>e to one (1) credit unit equivalence.

**REMARK ON BACKGROUND INFRASTRUCTURE EMISSIONS:** The rules in section 7.4 apply specifically to *foreground* infrastructure emissions, not *background* infrastructure emissions. Foreground infrastructure includes facilities built by the operator, such as feedstock deployment equipment and storage buildings. In contrast, background infrastructure refers to elements like the infrastructure required for electricity generation used in the process. Since background infrastructure emissions are already accounted for in the LCA emission factors—along with their own assumptions e.g. on lifetime and maintenance requirements— $CO_2$  Removal Suppliers do not need to modify or verify these assumptions. Background emission factors can be applied as provided.

<sup>&</sup>lt;sup>59</sup> In this document, amortization is an equivalent concept to the "linear discounting approach" presented in the GHG Protocol (2011) Product Life Cycle Standard (Appendix B) and GHGP (2022) Land Sector and Removals Guidance, Part 1: Accounting and Reporting Requirements and Guidance. (Draft for pilot testing and review).

## 7.5 Reporting of project emissions

- 7.5.1 The CO<sub>2</sub> Removal Supplier shall report project emissions every monitoring period by updating the LCA model with the corresponding operational and embodied emissions assigned to that period for accounting purposes.
- 7.5.2 The CO<sub>2</sub> Removal Supplier shall submit for Production Facility Validation the LCA model and a CORC summary calculation using expected values for a monitoring period, clearly defining the assumptions that will govern the project during the crediting period. The LCA results and the calculation of other contributing elements to the CORC calculation are ex-ante values that shall not be used to issue CORCs, but may be used to check that the project is performing within expected limits in future Output Audits.

### Disaggregated results for auditing

7.5.3 The CO<sub>2</sub> Removal Supplier shall submit LCA results in the LCA model and CORC calculation summary in a disaggregated manner as presented in table 7.1. For each level 1 unit process (see figure 7.1 and table 7.1), the LCA results shall clearly exhibit the contributions of the corresponding substages (level 2) and their contributions (level 3). <sup>60</sup>

### Aggregated results for public disclosure

- 7.5.4 The CO<sub>2</sub> Removal Supplier shall publicly disclose the results of the LCA calculations (i.e. the verified LCA results after each Output Audit) in the Puro Registry, to the extent described in subrules a-b.
  - (a) The CO<sub>2</sub> Removal Supplier shall publicly disclose all level 1 and level 2 contributions, as well as certain level 3 contributions (i.e. direct land use change emissions). The contributions required to be publicly disclosed are marked with and asterisk (\*) in table 7.1.
  - (b) Contributions other than those within the purview of subrule a may be aggregated to a level sufficient to protect sensitive information or licensed LCA data, as agreed with the Issuing Body.

<sup>&</sup>lt;sup>60</sup> Disaggregated reporting is required to ensure the transparency and interpretability of the results and to facilitate the auditing process (i.e., verification of claims).

**Table 7.1**. Levels of contribution to the LCA calculations of the unit processes, and identification of which contributions must be made public in the Puro Registry as part of Output Audit data (marked with an asterisk, \*).

Main stages Level 1 unit process	Sub-stages Level 2 contributions	Further sub-stages Level 3 contributions	Comment
$^*E_{sourcing}$	*Operational emissions of feedstock production, supply, processing, (if applicable) and transport to the production site	Production Processing Supply	Third-level contributions may be split in sub-stages as relevant for each supply-chain.
	*Embodied emissions of assets for feedstock extraction and processing	Construction and disposal of infrastructure and equipment Note: Direct land use change (dLUC) associated with sourcing (i.e., mining) is covered under leakage emissions.	Those emissions are verified at the Facility Audit and then amortized evenly over the first crediting period.
$*E_{transport}$	*Operational emissions of transporting feedstock.	Energy use (heat, electricity, fuel) Material use Transport	Third-level contributions may be split in sub-stages as relevant for each supply-chain.
$^*E_{application}$	*Operational emissions for spreading the feedstock on site, excluding transportation from sourcing to site of use.	Energy use (heat, electricity, fuel) Material use Waste treatment.	Third-level contributions may be split in sub-stages as relevant for each supply-chain.
	* Embodied emissions of assets for operational application of feedstock.	*Direct land use change (dLUC)	
$^*E_{monitoring}$	*Operational emissions of monitoring weathering process.	Sample collection and transport from site to laboratory for analysis	

# 8 Determination of Leakage (Eleakage)

The concept of leakage in the Puro Standard General Rules refers to the increase or decrease of greenhouse gas (GHG) emissions generated by the carbon removal activity outside of its system boundary and the activity's baseline scenario. For the purpose of CORC quantification, only the increase in GHG emissions or decreases in carbon stocks are quantified and subtracted to arrive at the activity's net carbon removal if not avoided or mitigated. Net positive effects are not included in the quantification of CORCs.

As defined in the Puro Standard General Rules, the scoping for sources of leakage is performed at the methodology level and shall result in a list of such sources. Further, Puro categorizes sources of indirect effects in two groups, whose definition is reminded here:

- Ecological leakage: a project can change the greenhouse gas fluxes mediated by ecosystemlevel changes in surrounding areas outside of the project boundaries, especially with hydrologically connected land areas. This is also referred to as potential negative effects to nearby land and ecosystem.
- Market and activity shifting leakage: a project can generate competition for resources and services, altering the supply-demand equilibrium, leading to changes in price and availability of goods or services, causing an increase/decrease in emitting activities elsewhere (market effects) and a project can displace an activity or change the likelihood of an activity outside the project's boundaries (activity shifting). These two notions are grouped together as they are often interrelated and sometimes necessary to assess jointly.

This section defines the relevant sources of leakage emissions that could be associated with the ERW carbon removal activity, following the three-step approach defined in the Puro Standard General Rules:

- 1. Determine potential leakage source (see section 8.1).
- 2. Avoid or mitigate leakage sources (see section 8.2).
- 3. Quantify unmitigated leakage (see section 8.3).

# 8.1 Identification and characterization of leakage emissions

The availability of basalt and other rocks suitable for ERW may be limited due to geological factors. Moreover, there is strong commercial demand in well-established markets for construction aggregate, metal extraction, glass/ceramics manufacturing, and decorative stone. As a consequence, this methodology anticipates that an ERW activity may lead to a competing use of natural rocks for carbon sequestration and could include as a potential source of leakage the indirect land use change impact associated with mining operations to meet the demand for the product.

When the ERW feedstock is demonstrably a waste material (e.g., slags, ashes, fines, mine tailings, or other alkaline industrial waste materials, see rule 3.8.2 c) with no viable competing use, leakage associated with market displacement shall be considered negligible.

8.1.1 The CO<sub>2</sub> Removal Supplier shall disclose the location from which the rock is sourced from (rule 3.8.1) and provide third-party market reports of current market supply and expected demand growth to determine whether the ERW activity will increase the demand for rock.

**Note**: If the CO<sub>2</sub> Removal Supplier cannot determine or provide evidence of feedstock sourcing for quarried or mined rock as required under rule 3.8.1, it is conservatively assumed that there is a competing market demand for the material and leakage shall be quantified according to rule 8.3.1.

## 8.2 Avoidance and mitigation of leakage emissions

- 8.2.1 To avoid leakage emissions from quarried or mined feedstock, the CO<sub>2</sub> Removal Supplier shall demonstrate for each deployment period (see rule 7.2.4) that the demand for feedstock rock by the ERW activity does not exceed the current national market available supply. However, when feedstock is imported from outside the country where the ERW activity is taking place, it is conservatively assumed that leakage is taking place and so it shall be quantified using rule 8.3.1.
- 8.2.2 To mitigate leakage emissions from quarried or mined feedstock, the CO<sub>2</sub> Removal supplier shall demonstrate that the feedstock sourcing site is in a jurisdiction that requires mine post-closure land reclamation and includes a reclamation surety bond or similar financial instrument to ensure the implementation of the reclamation plan.

# 8.3 Quantification of non-mitigated leakage emissions

- 8.3.1 To quantify non-mitigated leakage emissions, the CO<sub>2</sub> Removal Supplier shall estimate the impact on carbon stocks associated with forest areas being converted into barren lands as a proxy for the expansion of mining operations. This is estimated based on the share of the total demand of rock used by the project during the crediting period (see rule 7.2.4) relative to the total extractable/permitted rock and the effective land mine area, and taking into account the IPCC guidelines for land use change as follows:
  - (a) Determine the share of land use change impact (F<sub>s</sub>) based on the fraction of the total demand of rock (Q<sub>rock</sub>) used by the project during the monitoring period to the total extractable/permitted rock of the mine (Q<sub>permitted</sub>) using eq. 8.1;
  - (b) Estimate the impact of land use change using eqs. 8.2, 8.3, and 8.4.

(c) Land use change emissions shall be quantified using the available values for land conversion following the IPCC Guidelines for National Greenhouse Gas Inventories<sup>61</sup>, giving preference to data specific to the project (Tier 3), followed by country-specific values (Tier 2), or finally, average values (Tier 1). The choice shall be justified with the appropriate reference to the data source.

$$F_s = \frac{Q_{rock}}{Q_{permitted}} \tag{8.1}$$

$$A_{converted} = F_s \times A_{mine} \tag{8.2}$$

(d) The calculation shall be performed using eqs. 8.3 and 8.4:

$$E_{leakage} = \frac{44}{12} \times (CS_B - CS_P) \times A_{converted} + E_{conversion}$$
 (8.3)

where the carbon stock per unit area is defined as:

$$CS_X = C_{VEG_X} + C_{DOM_X} + SOC_X (8.4)$$

(i) The variables  $C_{VEG_X}$ ,  $C_{DOM_X}$ , and  $SOC_X$  should be determined using the equations presented in volume 4 of the IPCC Guidelines for National Greenhouse Gas Inventories<sup>62</sup> and the EU Commission decision on guidelines for the calculation of land carbon stocks for the purpose of Annex V to Directive 2009/28/EC<sup>63</sup> (see also rule 7.4.4 d).

Variable	Description	Unit
$F_s$	Attributable share of impact.	
$Q_{rock}$	Total amount of rock applied to site during the monitoring period.	tonne
$Q_{permitted}$	Total amount of extractable rock permitted at the mining site.	tonne
$A_{converted}$	Area of land converted attributable to project.	
$A_{mine}$	Effective mining land area defined in the land permit or lease.	ha
$E_{leakage}$	Absolute direct land use change associated with the new mining operations during the monitoring period.	tCO <sub>2</sub> e
$CS_B$	Carbon stock per unit area associated with the baseline land use.	tC ha <sup>-1</sup>
$CS_P$	Carbon stock per unit area associated with the project land use.	tC ha <sup>-1</sup>

<sup>&</sup>lt;sup>61</sup> 2006 IPCC Guidelines for National Greenhouse Gas Inventories, Prepared by the National Greenhouse Gas Inventories Programme, Eggleston H.S., Buendia L., Miwa K., Ngara T. and Tanabe K. (eds).

<sup>&</sup>lt;sup>62</sup> 2019 Refinement to the 2006 IPCC Guidelines for National Greenhouse Gas Inventories, Calvo Buendia, E., Tanabe, K., Kranjc, A., Baasansuren, J., Fukuda, M., Ngarize, S., Osako, A., Pyrozhenko, Y., Shermanau, P. and Federici, S. (eds).

<sup>&</sup>lt;sup>63</sup> 2010/335/: Commission Decision of 10 June 2010 on guidelines for the calculation of land carbon stocks for the purpose of Annex V to Directive 2009/28/EC (notified under document C(2010) 3751).

Variable	Description	Unit
$A_{converted}$	Area of land converted.	ha
$E_{conversion}$	Greenhouse gas emissions associated with the land use conversion activities, e.g. fuel usage for clearing the land, direct emissions from fire.	tCO2e
$CS_X$	Carbon stock per unit area with the project or baseline land use, where subscript $X$ indicates the type of land use.	tC ha <sup>-1</sup>
$C_{VEG_X}$	Above and below ground living biomass carbon stock.	tC ha-1
$C_{DOM_X}$	Dead organic matter or litter biomass carbon stock.	tC ha-1
$SOC_X$	Soil organic carbon stock.	tC ha-1

# 9 Monitoring Requirements

### 9.1 General principles

Monitoring, measuring, and reporting the performance of the carbon removal activity is essential to ensure that the requirements prescribed in this methodology have been fulfilled. Due to the complexity of the underlying system and the lack of consensus on quantification approaches (see section 11.3), it is paramount that the monitoring plan is designed in a robust manner, based on upto-date scientific knowledge and substantial baseline measurements in the local system.

In practice, the monitoring, measuring, and reporting procedures followed in this methodology are the responsibility of the CO<sub>2</sub> Removal Supplier. The verification of the information submitted by the CO<sub>2</sub> Removal Supplier is conducted by a recognized third-party auditor. Finally, the issuance of CO<sub>2</sub> Removal Certificates (CORCs) as a result of the project's performance is the responsibility of the Issuing Body.

A key step in verifying the monitoring data consists of inspection of relevant evidence and corroborating calculations by the auditor. Depending on the requirement, the pieces of evidence themselves can take various forms, such as data records, permits, official documents, or other relevant information which demonstrate compliance with the requirements, and enable claims to be verified. If the auditor concludes, based on the evidence presented, that the carbon removal activity is compliant with the requirements of this methodology, the validated amount of CORCs can then be issued to the CO<sub>2</sub> Removal Supplier.

Note that while this section contains several overarching requirements on the data collection, monitoring, and reporting requirements concerning the Enhanced Rock Weathering activity, additional requirements on these topics are included in other sections of this methodology as well.

While the resolutions or accuracies of individual tools in the monitoring suite may vary, it is the cumulative data from the monitoring approach as a whole that yields the necessary level of detail to determine with a very high degree of certainty that CO<sub>2</sub> is sequestered and effectively stored long-term, that soil, groundwater, and the environment more generally are being protected, and that any irregularities can be detected and addressed before they escalate.

### 9.2 Monitoring plan

- 9.2.1 The CO<sub>2</sub> Removal Supplier shall prepare and abide by a **Monitoring Plan** to assess the performance of the carbon removal activity.
  - (a) The Monitoring Plan shall be developed in conjunction with the Quality Control Procedures (section 10.3) and describe the procedures by which the CO<sub>2</sub> Removal Supplier will collect data and evidence in accordance with ISO 14064-2:2019<sup>64</sup> and Puro Standard requirements.<sup>65</sup>
  - (b) The scope of the Monitoring Plan shall cover all aspects related to:
    - (i) ensuring the conformity of the project with the eligibility requirements (section 3);
    - (ii) monitoring environmental and social impacts in support of SDGs (section 3.10) and safeguarding against identified environmental and social risks (section 4);
    - (iii) measuring the project's carbon sequestration (C<sub>stored</sub>, C<sub>baseline</sub>, C<sub>loss</sub>) and GHG emissions (section 5, section 6, section 7, and section 8); and
    - (iv)monitoring the risk of reversals (section 9.5).
  - (c) The suite of monitoring technologies described in the Monitoring Plan shall be:
    - (i) chosen such as to enable the verification of the changes in carbon stock based on the different quantification approaches included in this methodology (section 11.3), in support of the sampling approach (section 11.1), and following the QC procedures (section 10.3); and
    - (ii) adapted to the site-specific needs of the Removal Activity.
- 9.2.2 The Monitoring Plan shall include the following components:
  - (a) description of the monitoring practices based on their purpose;
  - (b) project boundaries and monitoring system diagram;
  - (c) roles and responsibilities of the project personnel involved in the monitoring and data collection processes;
  - (d) data collection plan for feedstock characterization, CORC quantification, and pre-application soil characterization, including at least:

<sup>&</sup>lt;sup>64</sup> ISO 14064-2:2019 Greenhouse gases, Part 2: Specification with guidance at the project level for quantification, monitoring and reporting of greenhouse gas emissions reductions or removal enhancements.

<sup>&</sup>lt;sup>65</sup> Available in the Puro Standard document library.

- (i) a list of all utilized parameters and their associated attributes in accordance with table 9.1; and
- (ii) sampling strategy (including criteria for definition of homogeneous strata (rule 11.1.1), use of evaluation area, assignment of control sites (rule 11.1.4).
- (e) LCA model and description, including:
  - (i) separate LCI for operational and embodied GHG emissions; and
  - (ii) clearly stating which activity data (AD) to collect and which uses average or fixed values;
- (f) uncertainty assessment and quantification procedures;
- (g) description of data quality control (QC) procedures (see section 10.3);
- (h) description of the information management system for record keeping and data management;
- (i) definition of expected or normal values or value ranges, or threshold values;
- (j) procedures to define and respond to significant irregularities in the project performance (i.e., contingency monitoring), including the case of reversal events, and violation of environmental and social safeguards; and
- (k) information about any internal or external laboratories, and outsourced procedures utilized (names and addresses), and their relevant accreditation, if applicable (see also rule 10.3.4).
- 9.2.3 The CO<sub>2</sub> Removal Supplier shall submit the Monitoring Plan with the Project Description for its validation during the Production Facility Audit, as described in the Puro Standard General Rules<sup>66</sup>, and is required to be made available in the Public Registry, either in full or in a redacted form for confidentiality, once the Facility Audit is successfully completed.
- 9.2.4 The Monitoring Plan shall be periodically evaluated and updated to ensure the monitoring practices remain appropriate and effective.
  - (a) The evaluation shall include a reassessment of the site-specific monitoring requirements and risks.
  - (b) Updates to the monitoring plan might be necessary due to:

<sup>&</sup>lt;sup>66</sup> Available in the Puro Standard documents library.

- (i) changes to the Production Facility that affect the activities being monitored;
- (ii) changes to the Puro normative framework that require an update in the monitoring activities; and
- (iii) corrective actions requested from the auditor.
- (c) All changes to the Monitoring Plan are subject to re-validation by the third-party auditor during the next available Output Audit.
- 9.2.5 The CO<sub>2</sub> Removal Supplier shall utilize the parameters and monitoring procedures described in the Monitoring Plan to report and provide evidence of the Production Facility performance for each monitoring period in accordance with the reporting requirements described in section 13.
- 9.2.6 The terminology used in this methodology in relation to monitoring frequency shall be interpreted as detailed in subrules a-b:
  - (a) The following definitions apply to the description of monitoring frequency:
    - Monthly monitoring is defined as at least once per calendar month.
    - Quarterly monitoring is defined as at least four times per calendar year (once every three months).
    - Semi-annual monitoring is defined as at least twice per calendar year (once every six months).
    - Annual monitoring is defined as at least once per calendar year.
    - Periodical monitoring is defined as monitoring at predetermined, regular temporal intervals decided by the CO2 Removal Supplier based on sitespecific needs as well as any applicable regulations. The monitoring frequency and rationale thereof shall be explained in the monitoring plan.
  - (b) Monitoring activities with a predefined cadence (e.g. quarterly monitoring) shall be evenly distributed throughout the monitoring period (e.g. once every three months for quarterly monitoring). The CO<sub>2</sub> Removal Supplier may make reasonable adjustments to the monitoring schedule for reasons of necessity or practicality, but such adjustments shall not result in any undue or disproportionate delays to the monitoring activities.

**Table 9.1.** Information to be compiled in the monitoring plan for each relevant parameter involved in the LCA and CORC calculations, and environmental and social safeguards (see rule 9.2.2.d.i).

Field name	Description	
ID	A unique identifier of the parameter.	
Parameter	The name of the parameter.	
Unit	The measurement unit of the parameter.	
Value	The value of the parameter.	
Equation	Reference to the equation where this parameter contributes to.	
Description	A brief text describing what the parameter is about, and how it is used in calculations.	
Source of data	A brief text describing where the data is sourced from: measured (m), calculated (c), or estimated (e).	
Monitoring frequency	The frequency of monitoring of the parameter.	
Monitoring density	The density (in number of samples per area of field site) of monitoring of the parameter.	
QC procedures	A brief text describing how the data is obtained, via what measurements, and why the value selected is conservative in light of possible error or uncertainty.	
Measurement uncertainty (%)	An estimation of the <i>random error</i> component associated with the measurement, and estimated as percentage uncertainty in the parameter.	
Comments	Free text comments	

# 9.3 Monitoring eligibility compliance

- 9.3.1 The CO<sub>2</sub> Removal Supplier shall comply with the eligibility requirements described in this Methodology and Puro Standard General Rules.<sup>67</sup>
  - (a) In the case where any deviations or non-conformities with the eligibility requirements or validated Production Facility design are detected during a monitoring period, the CO<sub>2</sub> Removal Supplier shall without delay:
    - (i) notify the Issuing Body;
    - (ii) develop a plan to solve the situation at the earliest possible; and

<sup>&</sup>lt;sup>67</sup> Available in the Puro Standard documents library.

- (iii) demonstrate actions to meet the eligibility requirements.
- (b) The non-conformity with the eligibility requirements can:
  - (i) impact the verification of the Output of the Production Facility and the corresponding CORC issuance for that period; and/or
  - (ii) require the Issuing Body to suspend the Production Facility in accordance with the Puro Standard General Rules.<sup>68</sup>
- 9.3.2 The CO<sub>2</sub> Removal Supplier shall keep a record of the documentation that supports the chain of custody of the eligible sources of weathering feedstock in accordance with requirements for sustainability and traceability of origin (see section 3.8) and make that documentation available for third-party verification upon request.

### Characterization of the field site prior to feedstock application

- 9.3.3 The CO<sub>2</sub> Removal Supplier shall comprehensively characterize the field site by sampling prior to spreading weathering material in order to:
  - (a) Evaluate site eligibility (see section 3.9).
  - (b) Establish the environmental conditions of the storage site prior to weathering material deployment and assess environmental changes due to the ERW activity (rule 9.3.5).
  - (c) Determine homogeneous strata for sampling strategy (section 11.1)
- 9.3.4 **Subsequent monitoring periods**: From the second monitoring period at a given field site onwards, measurements taken at the end ( $t_1$ ) of the preceding monitoring period may be used as part of the pre-application soil characterization for the new monitoring period, unless the preceding monitoring period ended more than 1 year before the start of the new monitoring period.
- 9.3.5 The CO<sub>2</sub> Removal Supplier shall conduct soil analyses at the field site before spreading of the weathering material (i.e., before the start of a Deployment Period, see rule 7.2.4, figure 7.2) as well as at some point between spreading and end of the Deployment Period as further specified in subrules a-e and listed in table 9.2. This is for the purpose of monitoring the influence of the ERW activity on soil ecological health and to inform efficient ERW deployment, including the identification of homogeneous strata (see rule 11.1.1, rule 11.1.2).

<sup>68</sup> Ibid.

- (a) The soil analysis shall determine the soil type(s) and initial (pre-application) physical and chemical characteristics of the field site by applying the measurements listed in table 9.2. Some of these measurements shall be repeated after feedstock application on application and control sites as specified in table 9.2.
- (b) Sampling depth (if applicable) for soil characterization purposes shall equal the sampling depth applied for C<sub>stored</sub> on a given field site and follow the same rules (11.2.8-11.2.11).
- (c) In order to determine the information required in subrule a, the CO<sub>2</sub> Removal Supplier may, where available, utilize representative external sources of information, such as values from soil databases or previous measurements (e.g. measurements conducted as part of typical agronomic practices of the region). However, the CO<sub>2</sub> Removal Supplier *should prefer* direct measurements, and utilize external sources of information to complement, rather than to replace, experimental baseline sampling.
- (d) The CO<sub>2</sub> Removal Supplier shall ensure that the collected soil information is statistically representative of the entire field site by employing appropriate sampling strategies (e.g., split field, randomized control, grid sampling) as well as a sampling density appropriate to the site-specific characteristics of the field site (such as the types of soils within the Production Facility and the underlying spatial variability thereof, typical parameter ranges and variance). The minimum sampling density guidelines in table 11.1 may serve as initial guidance but more sampling is recommended where initial results suggest higher variability in relevant parameters (see table 9.2).
- (e) The sampling density of relevant parameters for soil condition monitoring after feedstock application (see table 9.2) can likely be lower than before feedstock application, because conditions are by that point understood better. Therefore, to assess changes in soil condition due to feedstock application, post-feedstock application samples shall be taken at least from each homogeneous stratum (rule 11.1.1).

**Table 9.2.** Overview of required and recommended measurements across the field site with recommended analytical methods for soil characterization, including agricultural parameters. Note that requirements and recommendations or lack thereof refer only to soil characterization and not to C<sub>stored</sub> or C<sub>loss</sub> quantification for which separate requirements apply.

Parameter	Analytical methods and reference	Before feedstock application	After feedstock application
Soil type/texture	See rule 11.1.2	Required	Not required
SOC	Dry combustion (ISO 10694:1995)	Required (rule 4.5.1)	Required (rule 4.5.1)
SIC	Thermogravimetric analysis (TGA), calcimetry (ISO 10693:1995), dry combustion (ISO 10694:1995)	Required	Required
Bulk soil major cations, including Mg, Ca, K, Na.	ICP-MS or ICP-OES (e.g., ISO 22036:2024) after soil digestion (e.g., ISO 14869-3:2017, Mehlich-3 (Mehlich, 1984))	Required	Not required
Bulk soil immobile trace cations (e.g., Ni, Ti,)	ICP-MS or ICP-OES (e.g., ISO 22036:2024) after soil digestion (e.g., ISO 14869-3:2017)	Recommended for informing sampling strategy if Approach A2 is considered.	Not required (unless Approach A2 is used)
Soil bulk density	ISO 11272:2017	Required	Recommended <sup>69</sup>
Soil pH	ISO 10390:2021	Required	Required
CEC (at soil pH)	ISO 11260:2018, ISO 23470:2018	Required	Required
Heavy metals (listed in table 4.3, see also section 4.5.	ICP-MS (ISO 17294-1:2024) or ICP- OES (ISO 11885:2007) after acid digestion (EPA 3050B)	Required (see rule 4.5.2 and rule 3.9.3)	Required (rule 4.5.2)
Crop type	Agricultural documentation	Required	Required
Agricultural yield or year-over-year yield difference	Agricultural documentation	Required (if farmer consents to sharing yield data <sup>70</sup> )	Required (if farmer consents to sharing yield data)
Plant cation composition	EPA Method 3050B, AOAC Official Method 975.03, ICP-MS (ISO 17294- 1:2024), ICP-OES (ISO 11885:2007)	Recommended	Recommended
Organic and inorganic fertilizer application	Agricultural documentation	Recommended	Recommended

<sup>&</sup>lt;sup>69</sup> Soil density is needed to calculate SOC stocks (rule 4.5.1). Therefore, density measurements are recommended to use for more accurate SOC stock calculations than could be done using the density measured prior to feedstock application, which is, however, a permissible alternative.

<sup>&</sup>lt;sup>70</sup> Note that stakeholders have the option of using feedback and grievance mechanisms outlined in the Puro Stakeholder Engagement Requirements, section 2.5.

# 9.4 Monitoring for C<sub>stored</sub> quantification

### Evidence requirements for C<sub>stored</sub>

- 9.4.1 The CO<sub>2</sub> Removal Supplier shall quantify the gross amount of carbon stored during the monitoring period (C<sub>stored</sub>) utilizing site-specific empirical measurements in accordance with the quantification approaches described in section 11.3. For this, the CO<sub>2</sub> Removal Supplier shall use a quantification approach and a validation approach as described in rule 11.3.1. Additionally, models may be used to extrapolate from measurements as per rules 12.2.1-12.2.12.
- 9.4.2 The CO<sub>2</sub> Removal Supplier shall quantify the maximum CO<sub>2</sub> removal capacity (CDR<sub>max</sub>) for the utilized feedstock and the corresponding maximum gross CO<sub>2</sub> removal for the Production Facility (C<sub>stored, max</sub>) as further detailed in subrules a-c.
  - (a) The value for CDR<sub>max</sub> (in tonnes of CO<sub>2</sub> equivalents per tonne of feedstock) shall be calculated in accordance with eq. 1.6 based on the measured major element oxide composition and carbon content of the feedstock (see table 3.1).
  - (b) The value for C<sub>stored, max</sub> shall be calculated by multiplying CDR<sub>max</sub> by the total amount of feedstock applied in the Production Facility.
  - (c) The CO<sub>2</sub> Removal supplier shall compare the quantified value of C<sub>stored</sub> to the theoretical maximum value C<sub>stored</sub>, <sub>max</sub> to sense-check that no obvious overestimation of C<sub>stored</sub> has occurred.
    - (i) In cases where C<sub>stored</sub> > C<sub>stored</sub>, max, the value of C<sub>stored</sub> shall be considered invalid, and the CO<sub>2</sub> Removal Supplier shall trace the error that led to this evident overestimation of C<sub>stored</sub> and correct the value of C<sub>stored</sub> as appropriate before CORCs can be issued.

# 9.5 Monitoring for CO<sub>2</sub> release and reversal

9.5.1 The CO<sub>2</sub> Removal Supplier shall assess the reversal risk according to the general requirements for risk assessment set in section 4.2, requirements for reversal risk assessment in section 4.3 and the Puro Standard General Rules.<sup>71</sup> Note, that only previously unknown or unanticipated re-emissions *after issuance of CORCs* are termed reversals, and separated from carbon losses which are accounted for *at the time of CORC issuance* (see section 6.3).

<sup>&</sup>lt;sup>71</sup> Available in the Puro Standard documents library.

### 9.6 Monitoring for environmental and social impacts

- 9.6.1 For monitoring of social and environmental impacts, the CO<sub>2</sub> Removal Supplier shall conduct an inclusive stakeholder engagement process in accordance with the Puro Stakeholder Engagement Requirements.<sup>72</sup> The result of the process shall be reported and included with the Project Description for the validation of the Production Facility. Any potential risk identified through this process shall be incorporated in the Monitoring Plan.
- 9.6.2 The Monitoring Plan shall include the following monitoring procedures:
  - (a) Environmental risks including, but not limited to, the predetermined risks identified in section 4.5, in accordance with the general requirements for risk assessment (see section 4.2), requirements for environmental and social risk assessment (see section 4.4) and the environmental safeguards defined in the Puro Standard General Rules.<sup>73</sup>
  - (b) The social risks identified in the Puro Stakeholder Engagement Report<sup>74</sup>, in accordance with the general requirements for risk assessment (see section 4.2), requirements for environmental and social risk assessment (see section 4.4) and the social safeguards defined in the Puro Standard General Rules and the Puro Stakeholder Engagement Requirements.<sup>75</sup>
  - (c) The environmental and social impacts that may contribute to the Sustainable Development Goals (see section 3.10) pursued by the CO<sub>2</sub> Removal Supplier in accordance with the Puro Standard General Rules and Puro SDG Assessment Requirements.<sup>76</sup>
- 9.6.3 The CO<sub>2</sub> Removal Supplier shall monitor the environmental impacts (changes to the initial conditions) using measurement procedures described in section 4.

<sup>72</sup> Ibid.

<sup>&</sup>lt;sup>73</sup> Available in the Puro Standard documents library.

<sup>74</sup> Ibid.

<sup>75</sup> Ibid.

<sup>76</sup> Ibid.

- 9.6.4 The CO<sub>2</sub> Removal Supplier shall design and implement an "Ongoing feedback and grievance mechanism" as described under the Puro Stakeholder Engagement Requirements<sup>77</sup> to facilitate the continuous engagement between the project stakeholders for the identification and resolution of any issue or grievance associated with the carbon removal activity.
- 9.6.5 The CO<sub>2</sub> Removal Supplier shall maintain a record of the stakeholder feedback and follow-up actions, and report the status and actions associated with this process in the corresponding Output Report until its adequate resolution.
- 9.6.6 The CO<sub>2</sub> Removal Supplier shall address any grievances in accordance with the mitigation hierarchy described in section 4.2.

## 9.7 Monitoring for greenhouse gas accounting

9.7.1 The CO<sub>2</sub> Removal Supplier shall collect monitoring data from all project activities to measure and calculate GHG emissions and carbon removals in order to determine the net carbon removal in accordance with the CORC equation (figure 5.1). All collected data relevant to CORC issuance must be reported, specifically negative (i.e., lack of CDR) data shall not be excluded.

77 Ibid.

# 10 Uncertainty Quantification and Discounting

### 10.1 General principles

Puro Standard Methodologies strive to minimize, quantify, and manage the uncertainties associated with conceptualisation and modelling the carbon removal activity. In general, uncertainty in quantification results from *observational errors*, which refer to the difference between an observed or measured value of a quantity and its unknown 'true value'. In the context of uncertainty assessment, these differences are further characterized by the concepts of *accuracy* and *precision* (see figure 10.1):

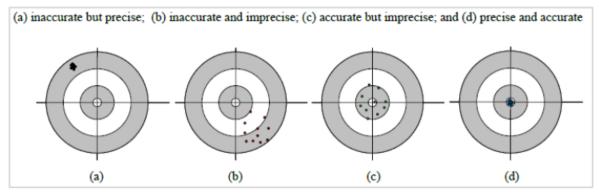
- Accuracy refers to how closely the average of repeated measurements or predictions
  corresponds to the true value of a variable. Accuracy implies the absence of systematic error,
  and translates for example into the need for proper calibration of measuring equipment and
  the use of representative data.
- Precision refers to the degree to which repeated measurements of the same variable produce
  consistent results. A higher precision indicates lower *random error*, obtained, for example,
  through the use of more precise measurement devices or the gathering of more data points.

For the purposes of this methodology, the uncertainties themselves can be also divided into two broad classes based on the source and nature of the uncertainties:

- Random errors refer to errors caused by unknown and unpredictable changes in the system or the experiment affecting the *precision* of quantification (see figure 10.1). These errors are not repeatable, and are uncorrelated between measurements. Random errors can arise from factors such as the inherent variability of environmental conditions (e.g. fine-scale soil heterogeneity), or incidental measurement errors (e.g., due to precision of the measurement device itself, or unpredictable variations in sample preparation). While random errors are unpredictable and always present, they can be estimated by statistical methods (see section 10.5).
- **Systematic errors** (or bias) refer to errors associated with repeatable processes inherent to the system affecting the *accuracy* of quantification (see figure 10.1). These errors often either remain constant or change in a predictable manner with changing conditions. Systematic errors can arise from innumerable sources, such as:
  - o a flawed characterization of the study variables or their sampling and measurement procedures (e.g. flawed experiment design, faulty or miscalibrated equipment); or
  - an incomplete understanding or other conceptual inaccuracies in the processes included in measurement and quantification (e.g. inaccurate or oversimplified assumptions underlying the quantification approach).

Systematic errors can, to a certain extent, be eliminated via reviewing, criticizing, and modifying the quantification approach and measurement procedures. However, deep

conceptual inaccuracies (so-called "unknown unknowns")—resulting, for example, from incomplete scientific understanding of the weathering process itself—can be difficult or impossible to completely eliminate.



**Figure 10.1**. Illustration of accuracy and precision (Buendia et al., 2019). Note that precision is independent of accuracy, meaning that measurements can be precise without necessarily being accurate.

For robust results, it is important to reduce quantification uncertainties as much as possible, and the  $CO_2$  Removal Supplier plays an important role in minimizing the uncertainty associated with the carbon removal activity performance (see also section 10.2 and 10.5). For example, the quantification of the gross amount of carbon removed (i.e. the  $C_{stored}$  component of the CORC equation, see section 6.1) can be affected by significant sources of uncertainty. For example, this component includes systematic errors linked to the understanding of the weathering processes, and challenges in monitoring and measuring chemical changes in the soil over time. The quantification is furthermore influenced by random errors due to both the inherent variability of soil conditions as well as factors such as measurement or sampling errors.

The estimation and management of errors, as well as uncertainty assessment in general have been extensively studied, and further relevant information on the treatment uncertainty can be found, for example, in the IPCC Guidelines for National Greenhouse Gas Inventories<sup>78</sup> (Buendia et al., 2019; Eggleston et al., 2006). In this methodology, the requirements for uncertainty estimation and management include, for example, the assessment of potential causes for uncertainties and mitigation strategies (see section 10.2), quality control procedures (section 10.3), and quantification and discounting of uncertainty (section 10.5).

<sup>&</sup>lt;sup>78</sup> See in particular IPCC Guidelines for National Greenhouse Gas Inventories, Volume 1: General Guidance and Reporting, Chapter 3: Uncertainties and Reporting, 2006 IPCC Guidelines for National Greenhouse Gas Inventories, and 2019 Refinement to the 2006 IPCC Guidelines for National Greenhouse Gas Inventories.

## 10.2 Uncertainty assessment

- 10.2.1 The CO<sub>2</sub> Removal Supplier shall undertake an uncertainty assessment of the implementation of the ERW activity, as further detailed in subrules a-c.
  - (a) The purpose of the uncertainty assessment is to:
    - (i) Identify and quantify the possible causes of uncertainty (see subrule b).
    - (ii) Establish actions that reduce uncertainty through the design of the ERW activity, and improve the accuracy and precision of the net carbon removal calculation (see subrule c).
  - (b) The uncertainty assessment shall address the potential causes of uncertainty summarised in table 10.1.<sup>79</sup>
  - (c) The uncertainty assessment shall at least encompass:
    - (i) Specification of the parameters that contribute to the quantification model described by the overall CORC equation (see figure 5.1).
    - (ii) Quantification of uncertainty estimates for the parameters used for the quantification of the net carbon removal process (see 10.5.2).
    - (iii) Calculating the overall uncertainty of the net CO<sub>2</sub> removal activity based on the mathematical combination of uncertainties (utilizing, e.g., frequentist or Bayesian methods, see section 10.5).
  - (d) The uncertainty assessment shall define the actions to be taken by the CO<sub>2</sub> Removal Supplier to reduce the causes of uncertainty in the implementation of the Enhanced Rock Weathering activity in accordance with the quality control procedures for each parameter included in data collection (section 10.3).

<sup>&</sup>lt;sup>79</sup> The CO<sub>2</sub> Removal Supplier should refer to the IPCC Guidelines for National Greenhouse Gas Inventories and General Guidance and Reporting for further information on treating uncertainty (Buendia et al., 2019; Eggleston et al., 2006). Note that the IPCC Guidelines include two additional causes of uncertainty excluded from table 10.1. These are the lack of completeness in the system definition and the model formulation. Both causes are addressed in this methodology through the selection of the quantification approaches.

Table 10.1. Causes of Uncertainty (after Buendia et al., 2019; Eggleston et al., 2006)

Cause of uncertainty	Туре	Potential mitigation actions
Lack of data	Bias	Quality Control:
		expert judgement
Lack of representativeness of data	Bias	Quality Control:
		Pedigree matrix approach80
	Random errors	Quality Control:
		Sampling
Statistical random sampling errors	Random errors	Quality Control:
		Sampling
Measurement error	Bias	Quality Control:
		Calibration
	Random errors	Quality Control:
		Sampling
Misreporting	Bias	Quality Control
Data gaps	Bias and random	Quality Control:
	errors	Statistics, experts

# 10.3 Quality control (QC) system and procedures

A quality control system and procedures are paramount to ensure the accuracy and reduce the uncertainty in the GHG emission calculations and other data required to assess the carbon removal activity's performance.

10.3.1 The CO<sub>2</sub> Removal Supplier shall ensure that all parameters required by this methodology—including but not limited to total net carbon removal, and environmental and social indicators (e.g. concentrations of potentially toxic elements)—are quantified *accurately* and *precisely* in accordance with this methodology as well as all applicable local laws, regulations, and other binding obligations.<sup>81</sup> This shall be evidenced by means of the quality control (QC) system (see rule 10.3.2) and data collection practices (see section 10.4 and table 10.2).

<sup>&</sup>lt;sup>80</sup> GHG Protocol Quantitative Uncertainty Guidance.

<sup>&</sup>lt;sup>81</sup> Note that accuracy and precision depend on the uncertainty associated with the processes and data inputs involved in quantification of the parameters (e.g. the GHG emissions, or the net carbon removal from the implementation of the ERW activity).

- 10.3.2 The CO<sub>2</sub> Removal Supplier shall have in place and abide by a quality control (QC) system as further detailed in subrules a-c.<sup>82</sup>
  - (a) The quality control system is comprised of:
    - (i) quality control procedures to measure and control the quality of the GHG inventory for the calculation of the net carbon removal (see rule 10.3.3); and
    - (ii) data necessary for other monitoring purposes (see rule 9.2.1 b).
  - (b) The purpose of the quality control system is to:
    - (i) ensure the data is presented in accordance with the principles of relevance, completeness, consistency, accuracy, transparency, and conservativeness as described in ISO 14064-2;83
    - (ii) identify and address errors and omissions; and
    - (iii)document and archive all inventory material and records in accordance with rule 13.1.5.
  - (c) The CO<sub>2</sub> Removal Supplier shall prepare a quality control plan providing a detailed description of the quality control system and any updates thereof (see also rules 10.3.3 and 10.3.5).
- 10.3.3 The quality control (QC) procedures shall include at least the following components:
  - (a) Roles and responsibilities:
    - (i) Identify the parties involved in coordinating the implementation of the quality control procedures.
    - (ii) Maintain a responsibility matrix to track ownership of data streams and quality tasks.
  - (b) Documentation and data traceability:
    - (i) Ensure complete documentation of all data sources, assumptions, and emission factors, and version control for all data management tools.
    - (ii) Maintain an audit trail for data collection, processing, storage, and reporting.

<sup>&</sup>lt;sup>82</sup> The CO<sub>2</sub> Removal Supplier should consult the IPCC Guidelines for National Greenhouse Gas Inventories (2006, 2019) for more detail in the development of a QC system.

<sup>&</sup>lt;sup>83</sup> ISO 14064-2:2019 Greenhouse gases, Part 2: Specification with guidance at the project level for quantification, monitoring and reporting of greenhouse gas emissions reductions or removal enhancements.

# (c) Activity data verification:

- (i) Perform independent checks of activity data (e.g., feedstock measurements, land-use data, energy/fuel inputs).
- (ii) Cross-verify field data with source documentation (e.g., invoices, satellite imagery, sensor logs).

## (d) Emission factor validation:

 (i) Confirm appropriateness and consistency of default or project-specific emission/removal factors, and reference their database sources or peerreviewed studies.

# (e) Data Entry and Transcription Checks:

- (i) Implement double data entry or automated error-checking procedures for manual entries.
- (ii) Review calculations and database queries for coding or logic errors, when applicable.

# (f) Uncertainty analysis:

- (i) Identify key data sources and quantify uncertainties as per rules in section 10.5.
- (ii) When possible, require laboratory analyses to be conducted by laboratories accredited under ISO 17025 and request laboratory results with their corresponding uncertainty estimation.

# (g) Internal audits and peer reviews:

- (i) Schedule regular internal QC reviews by qualified personnel not involved in data collection.
- (h) Data management and storage (record keeping):
  - (i) Ensure secure and redundant storage of all relevant data (field logs, photos, GIS files).
  - (ii) Apply access controls to protect data integrity while ensuring appropriate transparency.
  - (iii) Ensure confidentiality of the managed information, when required.
- (i) Calibration and maintenance of instruments:

- (i) Ensure all measurement instruments are installed, operated and regularly calibrated according to the device manufacturer's specifications or according to an appropriate industry consensus standard.
- (ii) Maintain logs of instrument maintenance, calibrations, and replacements.
- (j) Training and competency assurance:
  - (i) Provide training for field staff, data analysts, and QC reviewers on methods and quality procedures.
  - (ii) Document qualifications and continuous improvement activities.
- (k) Reporting and corrective actions:
  - (i) Establish a mechanism for reporting QC findings, inconsistencies, and corrective actions.
  - (ii) Track resolution of issues and integrate lessons learned into QC plan and procedures.
- 10.3.4 The CO<sub>2</sub> Removal Supplier shall ensure that laboratories used to carry out analysis for the quantification of carbon removal and environmental impacts meet the requirements equivalent to EN ISO/IEC 17025, including the following:
  - (a) Evidence of implementation of appropriate quality management procedures in the form of at least one of the following:
    - (i) accredited certification of the laboratory in conformity with EN ISO/IEC 9001 or other certified quality management systems;
    - (ii) other similar documentation and evidence of the utilized quality management procedures to the satisfaction of the Issuing Body.
  - (b) Evidence of technical competence covering all of the following elements:
    - management of the personnel's competence for the specific tasks assigned;
    - (ii) suitability of accommodation and environmental conditions;
    - (iii) selection of analytical methods and relevant standards;
    - (iv) where applicable, management of sampling and sample preparation, including control of sample integrity;
    - (v) Use of replicate analysis, standardized reference material (e.g., of known analyte concentration), and blanks analyzed in parallel to actual samples in order to determine the analytical precision, analytical accuracy, and analytical detection limit, respectively;

- where applicable, development and validation of new analytical methods or application of methods not covered by international or national standards;
- (vii) uncertainty estimation;
- (viii) management of equipment, including procedures for calibration, adjustment, maintenance and repair of equipment, and keeping records thereof;
- management and control of data, documents and software; (ix)
- management of calibration items and reference materials; (x)
- quality assurance for calibration and test results, including regular (xi) participation in proficiency testing schemes, applying analytical methods to certified reference materials, or inter-comparison with an accredited laboratory;
- (xii) management of outsourced processes; and
- (xiii) management of assignments, customer complaints, and ensuring timely corrective action.
- 10.3.5 The CO<sub>2</sub> Removal Supplier shall periodically review and update the QC procedures based on methodological advances or feedback and findings from the third-party validation of the QC plan and verification of the Output Report. Examples of such improvements include (but are not limited to) improving the estimates of emissions and/or removals, or reassessing data compilation processes and uncertainty estimates.84

#### 10.4 Data Collection

- 10.4.1 The CO<sub>2</sub> Removal Supplier shall collect the necessary data in accordance with the Monitoring Plan to fulfil the requirements of this methodology as well as all other Puro Standard requirements<sup>85</sup>, and requirements imposed by any applicable local laws, regulations, and other binding obligations.
- 10.4.2 The CO<sub>2</sub> Removal Supplier shall calculate the net carbon removal for each monitoring period. The calculation process and its result shall be included in the Output Report (see section 13) and made available to the Auditor for the Output Audit.

<sup>84</sup> In particular, the CO2 Removal Supplier should strive to reduce the parameter uncertainty and improve the quantification of the inventory of GHG emissions and carbon removal based on the data and information obtained from quantification of uncertainty (see section 10.5).

<sup>85</sup> Available in the Puro Standard documents library.

10.4.3 The CO<sub>2</sub> Removal Supplier shall define the attributes listed in table 10.2 for all parameters described in the Monitoring Plan.

**Table 10.2**. List of required parameter attributes.

Attribute	Description
ID	A unique identifier of the parameter.
Parameter	The name of the parameter.
Unit	The measurement unit of the parameter.
Value	The value of the parameter.
Equation	Reference to the equation where this parameter contributes to.
Description	A brief text describing what the parameter is about, and how it is used in calculations.
Type of data	Classify the type of data as measured (m), estimated (e), or calculated (c) based on the definitions described in rule 10.4.4.
Source of data	Reference of the data source: database, peer-reviewed study, etc.
Monitoring frequency	The frequency of monitoring of the parameter.
QC procedures	A brief text describing how the data is obtained, via what measurements, and why the value selected is conservative considering possible error or uncertainty.
Measurement uncertainty	An estimation of the <i>standard uncertainty</i> (see section 10.5) associated with the measurement, where applicable.
Data archive process	A brief text describing how the data is archived.
Time of data archive	For how long will the data be archived?
Comments	Free text comments

10.4.4 The CO<sub>2</sub> Removal Supplier shall classify the parameters described in the Monitoring Plan as either measured (m), estimated (e), or calculated (c) as further defined in subrules a-c. In cases of ambiguity, the CO<sub>2</sub> Removal Supplier may utilize best judgement to select the closest match.

- (a) **Measured**: parameters, whose values are obtained directly from an instrument or observation. The measurements may be conducted by the CO<sub>2</sub> Removal Supplier, or by external operators (such as external laboratories), provided that the CO<sub>2</sub> Removal Suppliers has access to the measurement data and relevant metadata for analysis of the results and associated uncertainty.<sup>86</sup>
- (b) **Estimated**: parameters, whose values are inferred using judgment, approximation, or indirect evidence (often when direct measurement is not possible), including parameters, whose values are obtained from scientific peer-reviewed literature, national or locally available survey maps or databases (e.g. databases for emission factors and average activity data), or other similar robust sources of information.
- (c) **Calculated**: parameters, whose values are obtained by applying a defined mathematical relationship or model to measured or estimated inputs.
- 10.4.5 The CO<sub>2</sub> Removal Supplier shall report parameter values in the units of measurement specified in this methodology or any reporting templates, guidance documents or other supplementary materials provided by the Issuing Body. For parameters where no specific unit is explicitly required, the International System of Units (SI) are the preferred units of measurement, but the CO<sub>2</sub> Removal Supplier may utilize other unit measurement systems (e.g. the British imperial system and the United States customary system).

# 10.5 Quantification of measurement uncertainty

Knowledge of measurement uncertainty implies increased confidence in a result's validity (Ellison, S L R & Williams, 2012). In the context of this methodology, the main object of estimating measurement uncertainty is the net carbon dioxide removal based on the elements that contribute to the CORC calculation. The CO<sub>2</sub> Removal Supplier should refer to the ISO/IEC Guide 98 series or the EURACHEM-CITAC Guide CG (Ellison, S L R & Williams, 2012) for further guidance on the estimation of measurement uncertainty.

- 10.5.1 For the purposes of this methodology, the following terms are utilized to describe uncertainty (JCGM 100:2008):
  - (a) Uncertainty (of measurement): parameter, associated with the result of a measurement, that characterizes the dispersion of the values that could reasonably be attributed to the measurand.

<sup>&</sup>lt;sup>86</sup> Measurement uncertainty depends on factors such as precision and calibration of measuring instruments, the sampling design, handling, etc.

- (b) **Absolute uncertainty**: uncertainty expressed in the same units as the measured quantity.
- (c) **Relative uncertainty**: uncertainty of the result of a measurement expressed as a ratio or percentage, calculated by dividing the absolute uncertainty by the measured value.
- (d) **Standard uncertainty**: uncertainty of the result of a measurement expressed as a standard deviation.
- (e) **Standard error**: standard deviation of the sampling distribution of a statistic (often the mean).<sup>87</sup>
- (f) **Combined uncertainty**: uncertainty of the result of a measurement when that result is obtained from the values of a number of other quantities.
- (g) Total uncertainty: combined standard uncertainty.
- (h) **Expanded uncertainty**: quantity defining an interval about the result of a measurement that may be expected to encompass a large fraction of the distribution of values that could reasonably be attributed to the measurand.<sup>88</sup> The expanded uncertainty is obtained by multiplying the total uncertainty by a numerical factor (i.e. the coverage factor) determined based on the level of confidence desired.
- (i) **Coverage factor**: numerical factor used as a multiplier of the combined standard uncertainty in order to obtain an expanded uncertainty (see also table 10.3).
- (j) **Type A evaluation (of uncertainty)**: method of evaluation of uncertainty by the statistical analysis of a series of observations.
- (k) **Type B evaluation (of uncertainty)**: method of evaluation of uncertainty by means other than the statistical analysis of a series of observations (e.g., by literature sources or expert judgement).

<sup>&</sup>lt;sup>87</sup> Note that while the standard error can be thought of as a type of standard uncertainty, there is a difference between the standard deviation (standard uncertainty) associated with a population or sample of observations, and the standard deviation (standard error) associated with a statistic (e.g. the mean) calculated from the sample. Importantly, note that the standard error falls as the sample size increases whereas the standard deviation will tend to remain the same.

<sup>&</sup>lt;sup>88</sup> The fraction may be viewed as the coverage probability or level of confidence of the interval. Note that to associate a specific level of confidence with the interval defined by the expanded uncertainty requires explicit or implicit assumptions regarding the probability distribution characterized by the measurement result and its combined standard uncertainty. The level of confidence that may be attributed to this interval can be known only to the extent to which such assumptions may be justified.

Table 10.3: Common coverage factors for the calculation of expanded uncertainty in the case of the normal distribution.

Level of confidence $p$ (%)	Coverage factor $oldsymbol{k}_p$ (unitless)
68.27	1.00
80.00	1.28
90.00	1.64
95.00	1.96
95.45	2.00
99.00	2.58
99.73	3.00

- 10.5.2 The CO<sub>2</sub> Removal Supplier shall determine the standard uncertainty of all parameters contributing to the overall uncertainty of the net CO2 removal activity as further defined in subrules a-c.
  - (a) The list of parameters for which standard uncertainty is determined shall include at least  $C_{stored}$ ,  $C_{baseline-[field]}$ ,  $E_{project}$ , (as defined in rule 5.3.1), as well as all their significant dependent parameters (see subrule c).
  - (b) The determination of standard uncertainty shall be based on appropriate and scientifically justifiable sources of information as further defined in rule 10.5.11.
  - (c) The CO<sub>2</sub> Removal Supplier may omit any or all of the following parameters from the quantification of uncertainty:
    - (i) The parameters  $C_{loss}$ ,  $C_{baseline-[feedstock]}$ , and  $E_{leakage}$ . For these parameters, the quantification requirements set in this methodology are deemed to result in sufficiently conservative values, such that further deductions due to uncertainty are not necessary.
    - (ii) Any mathematical or scientific constants (e.g. molecular weights), and default values included in this methodology.

For the purposes of calculating combined uncertainties, the CO<sub>2</sub> Removal Supplier may assume that the standard uncertainty of the omitted parameters is equal to zero.

10.5.3 The CO<sub>2</sub> Removal Supplier shall determine the parameters detailed in subrules a-d describing the overall uncertainty of the net CO<sub>2</sub> removal activity.

(a) The total uncertainty,  $u_c(CORC)$ , shall be calculated as follows (see rule 10.5.2 c for parameters that may be omitted).<sup>89</sup>

$$u_c(CORC) = \sqrt{u_c(C_{stored})^2 + u_c(C_{loss})^2 + u_c(C_{baseline})^2 + u_c(E_{project})^2 + u_c(E_{leakage})^2}$$
(10.1)

(b) The expanded uncertainty,  $U_c(CORC)$ , shall be calculated as follows:<sup>90</sup>

$$U_c(CORC) = 1.28 \times u_c(CORC) \tag{10.2}$$

(c) The relative expanded uncertainty,  $U_r(CORC)$ , shall be calculated as follows:

$$U_r(CORC) = \frac{U_c(CORC)}{C_{stored} - C_{loss} - C_{baseline} - E_{project} - E_{leakage}}$$
(10.3)

(d) The factor of conservativeness,  $F_c$ , shall be calculated as follows:

$$F_c = \max(0, 100\% - U_r(CORC)) \tag{10.4}$$

Variable	Description	Unit
$u_c(CORC)$	Combined standard uncertainty of the net amount of CO <sub>2</sub> equivalents removed by the enhanced weathering activity.	tCO2e
$u_c(C_{stored})$	(as defined in rule 5.3.1).	tCO2e
$u_c(C_{baseline})$	Combined standard uncertainty of the parameter $C_{baseline}$ (as defined in rule 5.3.1).	tCO2e
$u_c(\mathcal{C}_{loss})$	(as defined in rule 5.3.1).	tCO2e
$u_c(E_{project})$	Combined standard uncertainty of the parameter $E_{project}$ (as defined in rule 5.3.1).	
$u_c(E_{leakage})$	Combined standard uncertainty of the parameter $E_{leakage}$ (as defined in rule 5.3.1).	tCO2e
$U_c(CORC)$	The expanded uncertainty of the net amount of CO <sub>2</sub> equivalents removed by the enhanced weathering activity	tCO2e
$U_r(CORC)$	The relative expanded uncertainty of the net amount of CO <sub>2</sub> equivalents removed by the enhanced weathering activity	%
$F_c$	Factor of conservativeness used to discount the Output volume issued as CORCs, in accordance with rule 5.3.1.	%

<sup>&</sup>lt;sup>89</sup> Note that eq. 10.1 is an approximation of the true total uncertainty and lacks, e.g., terms describing correlations between the parameters. For further notes on the approximations made, see rules 10.5.10 a and 10.5.11 d and footnotes therein.

 $<sup>^{90}</sup>$  The coverage factor 1.28 in this equation corresponds to a confidence interval of 80% (subject to the assumption that the underlying distribution is normal).

- 10.5.4 The CO<sub>2</sub> Removal Supplier shall establish a parameter hierarchy listing all of the dependent parameters (uncertainty contributors) for the top-level parameters  $C_{stored}$ ,  $C_{loss}$ ,  $C_{baseline}$ ,  $E_{project}$ , and  $E_{leakage}$  in an organized fashion, as further detailed in subrules a and b.
  - (a) The parameter hierarchy shall clearly identify all dependent parameters contributing to the uncertainty of the top-level parameters in the  $CO_2$  Removal Supplier's specific implementation of the ERW activity (i.e. taking into account, for example, that the parameters contributing to  $C_{stored}$  depend on the chosen quantification method).
  - (b) The CO<sub>2</sub> Removal Supplier may choose a suitable representation for the parameter hierarchy, such as the example given in table 10.4, or a cause and effect diagram such as in EURACHEM-CITAC Guide CG 4, Appendix (Ellison, S L R & Williams, 2012).

**Table 10.4.** Example of a hierarchy of parameters contributing to uncertainty of the parameter  $E_{project}$ .

Level 0 component	Level 1 contributor	Level 2 contributor contributor		Level 4 or more
	Operation emissions	Esourcing Etransport Eapplication	Emission factor (EF <sub>i</sub> ) Activity data (AD <sub>i</sub> ) Allocation factor (AF <sub>i</sub> )	
$E_{project}$		Einfra	WBLCA <sup>a</sup>	Cveg
	Embodied emissions		CS	C <sub>DOM</sub> SOC
			A Econversion	

<sup>&</sup>lt;sup>a</sup> Note that a whole building life cycle assessment (WBLCA) for infrastructure emissions requires an extensive life cycle inventory. The CO<sub>2</sub> Removal Supplier should request or provide an estimated uncertainty for the whole infrastructure model.

- 10.5.5 The CO<sub>2</sub> Removal Supplier shall determine standard uncertainty utilizing appropriate and scientifically justifiable sources of information for each type of parameter (measured, estimated, or calculated; see rule 10.4.4), as further detailed in subrules a-c.
  - (a) For **measured** parameters, the CO<sub>2</sub> Removal Supplier shall utilize one or several of the following sources of data uncertainty:
    - (i) statistical analysis of repeated measurements;
    - (ii) previous measurement data;
    - (iii) measurement device manufacturer's specifications;

- (iv)data provided in calibration and other certificates; and
- (v) laboratory results from laboratories accredited under ISO 17025 or following equivalent evidenced practices (see rule 10.3.4).
- (b) For **estimated** parameters, the CO<sub>2</sub> Removal Supplier shall utilize one or several of the following sources of data uncertainty:
  - (i) uncertainties obtained from peer-reviewed publications or other similar credible sources (such as regulatory data, public databases, etc.);
  - (ii) uncertainties assigned based on quantitative procedures defined in peerreviewed publications or other similar credible sources (such as regulatory data, public databases, etc.);<sup>91</sup> and
  - (iii) expert knowledge or judgement.
- (c) For **calculated** parameters, the CO<sub>2</sub> Removal Supplier shall determine the uncertainty based on a combination of the uncertainty of its dependent parameters (see rule 10.5.9).
- 10.5.6 To determine the total uncertainty, the CO<sub>2</sub> Removal Supplier shall comprehensively account for the identified sources of uncertainty as further detailed in subrules a and b.
  - (a) The CO<sub>2</sub> Removal Supplier shall, to the extent feasible, account for all sources of uncertainty identified in the uncertainty assessment (see rule 10.2.1 and table 10.1).<sup>92</sup>
    - (i) The CO<sub>2</sub> Removal Supplier may omit identified sources of uncertainty for which quantification is not possible or feasible with the available data and information, and for which no other reasonable estimate of uncertainty can be made.<sup>93</sup>

<sup>&</sup>lt;sup>91</sup> For example, through utilizing the pedigree matrix approach defined in the GHG Protocol guidance for Quantitative Inventory Uncertainty. This involves using the pedigree matrix approach based on qualitative indicators to compute the parameter's geometric standard deviation and propagating its uncertainty using a Taylor series expansion.

<sup>&</sup>lt;sup>92</sup> For example, the total uncertainty for a measured parameter might include contributions due to random errors (e.g. resulting from variability of the soil or imprecision of the measurement device) as well as systematic errors (e.g. due to instrument drift or sample pretreatment). The former can be quantified through statistical analysis (Type A evaluation), while the latter e.g. from calibration records or other QA/QC documentation (Type B evaluation).

<sup>&</sup>lt;sup>93</sup> Such uncertainties might include e.g. uncertainties due to gaps in the scientific understanding of the weathering process itself or other "unknown unknowns", or similar inherent biases (see also discussion in section 10.1)

- (ii) Uncertainty components arising from different sources should not be "double counted". In particular, when conducting a Type A uncertainty evaluation, additional uncertainties arising from a Type B evaluation should be included as independent components of the combined standard uncertainty only to the extent that the additional component does not contribute to the observed variability of the observations.<sup>94</sup>
- (b) Evaluations of uncertainty shall be based on all available information, and utilize quantitative data to the maximum extent possible.
  - (i) The uncertainty contributions for measured parameters shall be quantified using statistical analysis of repeated measurements wherever feasible (Type A evaluation).
  - (ii) The uncertainty contributions for modeled parameters (e.g. parameters quantified utilizing an ERW simulation model, see section 12) shall include uncertainties arising from the simulation itself (e.g. as a result of inaccurate input values), as well as uncertainties associated with imperfect treatment of modeled phenomena.<sup>95</sup>
  - (iii)Where quantitative data for the determination of uncertainty is not available or sufficient, the CO<sub>2</sub> Removal Supplier shall transparently document and justify choice of values, sources of data, expert elicitation, and assumptions made.

<sup>&</sup>lt;sup>94</sup> For example, when the standard uncertainty of a parameter is obtained via statistical analysis of a sample of repeat measurements (Type A evaluation), the random errors arising from the measurement device (device precision) contribute to the overall variability in the observations and therefore need not be separately added as an independent component of uncertainty. However, potential systematic errors (e.g. instrument drift), determined e.g. through calibration records, would need to be added as an independent uncertainty contribution.

<sup>&</sup>lt;sup>95</sup> For example, in an ERW simulation model, uncertainties can stem from the use of inaccurate input values (e.g. weathering rates), which can be rather straightforwardly quantified e.g. through Monte Carlo simulations. However, additional uncertainty can result from the imperfect treatment of relevant biogeochemical processes in the model itself. Such uncertainties might not be adequately captured in a Monte Carlo simulation, and often additional quantification is necessary (e.g. validation through comparing modeled results to empirically measured results to estimate root mean square error).

- 10.5.7 Uncertainty estimates for a given parameter x obtained from an evaluation of the statistical dispersion of repeated measurements shall be quantified as the standard uncertainty u(x) of the parameter x. In particular, this standard uncertainty can, depending on the quantity of interest, refer to the observed (sample) standard deviation, or the standard deviation of the sampling distribution (i.e. the standard error) of a statistic (e.g. the mean or median) calculated from the data as further defined in subrules a and b.
  - (a) When expressing the uncertainty in single measurements, or the uncertainty associated with a particular sample (as opposed to the population from which the sample is drawn),<sup>97</sup> the sample standard deviation is used.
  - (b) When expressing the uncertainty of a statistic calculated from the sample, the standard error of the statistic is used. In particular, for expressing the uncertainty of average values obtained through the calculation of the arithmetic mean, the standard error of the mean is used.

<sup>&</sup>lt;sup>96</sup> Note that the standard uncertainty can be thus different for different parameters or statistics calculated from the same underlying data. For further information on the difference between standard deviation and standard error, see e.g. 2019 Refinement to the 2006 IPCC Guidelines for National Greenhouse Gas Inventories, Chapter 3: Uncertainties, Box 3.0A (pp. 3.13–3.14)

<sup>&</sup>lt;sup>97</sup> For example, when sampling a plot of land for a particular soil parameter (e.g. mean magnesium concentration), one is usually not ultimately interested in the mean of any particular sample of data points, but rather in the mean across the entire plot of land from which the sample is drawn (the underlying population). The mean will vary from sample to sample, but any given sample mean will be an *estimate* of the population mean.

**Example:** Consider a set of 100 measurements of soil cation concentration (e.g.  $[Mg^{2+}]$ ) measurements over a group of fields, with an observed mean of 2500 ppm and a standard deviation of 500 ppm. Now, on average, the result of a single measurement of  $[Mg^{2+}]$  is 2500 ppm  $\pm$  500 ppm (i.e. a relative uncertainty of 20%). However, one is often more interested in the uncertainty of the mean itself rather than that of a single measurement (for example, if using the mean Mg concentration to assess the total Mg stock in the fields). In this case, the quantity of interest is the standard error of the mean, which can be estimated as

$$u(\underline{[Mg^{2+}]}) \approx \frac{u([Mg^{2+}])}{\sqrt{n}} = \frac{500 \, ppm}{\sqrt{100}} = 50 \, ppm,$$

Where  $u(\underline{[Mg^{2+}]})$  is the standard uncertainty in the mean  $Mg^{2+}$  concentration,  $u(\underline{[Mg^{2+}]})$  is the observed standard uncertainty in the sample, and n is the number of samples. In other words, if one were to obtain *another* set of 100 measurements and calculate a new mean from *that* set of observations, and repeat the process many times, the standard uncertainty in the set of means thus obtained would be approximately 50 ppm, considerably lower than the observed sample standard deviation of the single data sample.

- 10.5.8 Uncertainty estimates obtained from external sources (i.e. based on expert judgement, previous measurement data or other sources defined in subrules 10.5.5 a and b, except cases falling under the purview of rule 10.5.6) shall, where necessary, be converted to standard uncertainty as further detailed in subrules a-c.
  - (a) Where an uncertainty estimate of a parameter x is reported as limits with a specified level of confidence p (that is, values reported in the form of  $x \pm a$  at p% confidence), the standard uncertainty u(x) of the parameter x is obtained by dividing the reported uncertainty range a by the coverage factor  $k_p$  (see table 10.3) corresponding to the reported level of confidence p, i.e. as  $u(x) = a/k_p$ . 98
  - (b) Where an uncertainty estimate of a parameter x is reported as limits without a specified level of confidence (that is, merely in the form of  $x \pm a$  without level of confidence), the standard uncertainty is obtained as follows.
    - (i) In cases where the underlying distribution is stated or otherwise known to such an extent that the omitted level of confidence can be determined, the uncertainty shall be determined as detailed in subrule a.

<sup>&</sup>lt;sup>98</sup> Note that the value of the coverage factor depends not only on the level of confidence, but also on the underlying distribution of values, and the values in table 10.3 refer to the normal distribution in particular. Where uncertainty is reported as a confidence interval without specifying the distribution, the normal distribution may be assumed.

- (ii) In cases where the underlying distribution is unknown or poorly characterized,<sup>99</sup> and there is limited or no reason to believe that any part of the specified range is more likely than another, CO<sub>2</sub> Removal Supplier may assume a rectangular distribution and use the value  $u(x) = a/\sqrt{3}$  as the standard uncertainty in the parameter x.
- (iii)In cases where the underlying distribution is unknown or poorly characterized, but there is justifiable reason to believe that extreme values (i.e. values near the ends of the reported range) are unlikely, the CO<sub>2</sub> Removal Supplier may assume a triangular distribution and use the value  $u(x) = a/\sqrt{6}$  as the standard uncertainty in the parameter x.
- (c) Where an estimate of the uncertainty of a parameter x is made based on expert judgement, and directly estimating the standard uncertainty (standard deviation) is not possible, then an estimate shall be made of the maximum deviation  $x \pm a$  which could reasonably occur in practice. The standard uncertainty u(x) of the parameter x shall then be obtained as detailed in subrule b.
- 10.5.9 In cases where the quantification of uncertainty of a parameter requires combination of uncertainties from other (dependent) parameters, the CO<sub>2</sub> Removal Supplier shall determine the combined uncertainty as further detailed in subrules a and b.
  - (a) The combination of uncertainties shall be based on the parameter hierarchy described in rule 10.5.4, and proceed by combining the uncertainty of parameters lower in the hierarchy to estimate the combined uncertainty of parameters higher in the hierarchy.
  - (b) To determine the combined uncertainty, the CO<sub>2</sub> removal supplier shall utilize one or several of the following principal methods for propagating measurement uncertainty:
    - (i) Propagation of uncertainty through local expansion, including in particular the law of propagation of uncertainty (see rules 10.5.10 and 10.5.11).
    - (ii) Propagation of uncertainty based on repeated random sampling of input data or distributions, including in particular Monte Carlo simulations and related methods such as bootstrapping (see rule 10.5.12).

<sup>&</sup>lt;sup>99</sup> In certain cases, it may be possible to estimate only the plausible upper and lower limits for a parameter, without knowledge about the possible values of the parameter inside the interval.

- (iii)Propagation of uncertainty based on calculation of a posterior probability distribution utilizing Bayesian inference (see rule 10.5.13).
- 10.5.10 For the purposes of obtaining a combined standard uncertainty utilizing local expansion methods, including in particular the law of propagation of error, the following rules apply.
  - (a) The combined uncertainty shall be quantified through utilization of local linear or higher-order approximations (e.g. a first-order Taylor series expansion) to propagate the uncertainties of the input parameters through the measurement function to obtain an explicit estimate of the variance of the measurand (see also rule 10.5.10 for formulae specifically related to the law of propagation of error).
    - (i) The estimated variance shall be expressed at least in terms of the standard uncertainties of the input parameters, and their associated sensitivity coefficients (partial derivatives of the measurand with respect to the input parameters).<sup>100</sup>
    - (ii) Where possible, the estimated variance should include the appropriate covariance terms for correlated input parameters.<sup>101</sup>
  - (b) The combined standard uncertainty shall be quantified as the positive square root of the estimated variance.
  - (c) The CO<sub>2</sub> Removal Supplier shall provide thorough documentation of the expansion method utilized, which shall at least include:
    - (i) A general description of the model including the functional relationship modeled and the method used for propagating uncertainties;
    - (ii) The explicit mathematical formulae used for propagation of uncertainty;
    - (iii) definition of all sensitivity coefficients (partial derivatives), standard uncertainties, and other input parameters; and
    - (iv) description of all modelling assumptions (e.g. local linearity or independence of inputs), along with their justification based on scientific literature, pre-existing data, measurement information, or other scientific rationale.

<sup>&</sup>lt;sup>100</sup> Note that besides the standard uncertainties and sensitivity coefficients, the expansion might additionally include other quantities, such as covariance terms for correlated inputs.

<sup>&</sup>lt;sup>101</sup> Covariance terms can be difficult or impossible to quantify if correlated parameters are not measured jointly (e.g. from the same soil sample). Practically speaking, covariance terms should be included in the computation only if they have been estimated from sufficient data (Ku, 1966).

- 10.5.11 For the purposes of obtaining the combined standard uncertainty utilizing the law of propagation of uncertainty, the following rules apply:
  - (a) All uncertainty contributions shall be expressed as standard uncertainties (i.e. as standard deviations) before combination, except in cases where relative uncertainties are combined in the special cases detailed in subrules c and d. This may involve conversion to standard uncertainty from some other measure of dispersion (see rule 10.5.8).
  - (b) To calculate the combined standard uncertainty, the CO<sub>2</sub> Removal Supplier may utilize the simplified variance formula, defined as follows in the EURACHEM-CITAC Guide CG 4, section 8.2. (Ellison, S L R & Williams, 2012):

$$u_c(y) = \sqrt{\sum_{i=1}^n \left(\frac{\partial y}{\partial x_i}\right)^2 u(x_i)^2}$$
(10.5)

Note that the simplified variance formula and equations derived from it (eqs. 10.5 - 10.9.) are based on a first order approximation which might not be justified in all cases (see subrule d).

- (c) As a direct consequence of the simplified variance formula in equation 10.5, the following formulas apply when variables are **combined through sum or difference**, i.e. if  $y = x_1 \pm x_2 \pm ... \pm x_n$ :
  - (i) The combined standard uncertainty is

$$u_c(y) = \sqrt{u(x_1)^2 + u(x_2)^2 + \dots + u(x_n)^2}$$
(10.6)

(ii) The combined relative uncertainty is

$$u_{c,r}(y) = \frac{\sqrt{(u_r(x_1) \cdot x_1)^2 + (u_r(x_2) \cdot x_2)^2 + \dots + (u_r(x_n) \cdot x_n)^2}}{|x_1 + x_2 + \dots + x_n|}$$
(10.7)

- (d) As a direct consequence of the simplified variance formula in equation 10.5, the following formulas apply when variables are **combined through product of quotient**, i.e. if  $y = x_1 x_2 ... x_n$  or  $y = x_1 x_2 ... x_k / (x_{k+1} ... x_n)$ :<sup>102</sup>
  - (i) The combined standard uncertainty is

$$u_c(y) = |y| \sqrt{\left(\frac{u(x_1)}{x_1}\right)^2 + \left(\frac{u(x_2)}{x_2}\right)^2 + \dots + \left(\frac{u(x_n)}{x_n}\right)^2} (10.8)$$

(ii) The combined *relative* uncertainty is

$$u_{c,r}(y) = \sqrt{u_r(x_1)^2 + u_r(x_2)^2 + \dots + u_r(x_n)^2}$$
(10.9)

<sup>&</sup>lt;sup>102</sup> Note that this does not apply to division in general (e.g. when the numerator or denominator is a sum of terms rather than a product of terms).

- (e) In cases where independence of the dependent parameters  $x_i$  cannot be assumed, or the nonlinearity of the parameter y is significant, the CO<sub>2</sub> Removal Supplier should, where possible, utilize alternate methods to determine uncertainty, or a more accurate version of the law of propagation of error.<sup>103</sup> Such methods could include e.g. jointly measuring correlated quantities (e.g. from the same soil core) and utilizing bootstrapping on the joint probability distribution, or a more advanced propagation formula (including covariances) to determine the combined uncertainty.<sup>104</sup> In particular, these alternate methods should be considered when either of the below conditions occur.
  - (i) Two or more dependent variables are or can be expected to be correlated (i.e. the variables  $x_i$  are not all independent); or
  - (ii) the relative uncertainty in one or several of the dependent parameters  $x_i$  is 30% or greater.<sup>105</sup>

Variable	Description	Unit
у	A parameter calculated from depending parameters $x_1, x_2,, x_n$ , calculated as $y = f(x_1, x_2,, x_n)$ for some given function $f$ .	Varies based on data
$x_i$	A dependent parameter utilized in the calculation of another parameter $y$ . The index $i = 1, 2,, n$ is used to distinguish different parameters.	Varies based on data
$u(x_i)$	Standard uncertainty of the parameter $x_i$ .	Varies based on data
$u_c(y)$	Combined standard uncertainty of the parameter <i>y</i> .	Varies based on data
$u_r(x_i)$	Relative uncertainty of the parameter $x_i$ , calculated as $u(x_i) = \frac{u(x_i)}{ x_i }$	%
$u_{c,r}(y)$	Combined relative uncertainty of the parameter $y$ , calculated as $u_{c,r}(y) = \frac{u_c(y)}{ y }$	%

 $<sup>^{103}</sup>$  The variance formula is a first order simplification which neglects any covariances between the dependent variables, as well as all higher order terms. In practice, neglecting covariances between input variables may not always be justified (e.g. soil bulk density can be correlated with soil inorganic carbon content). The importance of higher order terms (i.e. terms proportional to  $2^{nd}$  and higher order derivatives of the parameter y) depends on the magnitude of the uncertainties in the dependent parameters  $x_i$ . When the uncertainties in the dependent parameters are small enough, the higher order terms can be neglected with little impact to the result.

<sup>&</sup>lt;sup>104</sup> For more accurate versions of the variance formula (including higher order terms and covariances), see e.g. JCGM 100:2008, sections 5.1.2 and 5.2.2. Note, however, that fully determining all covariances between input parameters may not be possible or feasible in practice.

<sup>&</sup>lt;sup>105</sup> For further discussion, see e.g. 2019 Refinement to the 2006 IPCC Guidelines for National Greenhouse Gas Inventories, Chapter 3.2.3 Methods to combine uncertainties.

**Remark:** Note that the variance formula in equation 10.5 is defined in terms of standard uncertainties  $(u(x_i))$ . At times, it can be useful to combine relative uncertainties instead of standard uncertainties. To determine the correct formulas for combination of relative uncertainties, the variance formula can be utilized to calculate the combined relative uncertainty, i.e. the quantity  $u_{c,r}(y) = \frac{u_c(y)}{|y|}$ . In the special cases where the calculated parameter y can be expressed as a simple sum, difference, product, or quotient, the results of this calculation are given in rule 10.5.11.

**Example:** Soil bulk density

$$BD = \frac{M_{solids}}{V_{soil}}$$

can be determined based on measurements of the mass of solid soil particles ( $M_{solids}$ ) in a given volume of soil  $(V_{soil})$ . The combined standard uncertainty in the bulk density, $u_c(BD)$ , can be determined from the standard uncertainties in the measured variables ( $u(M_{solids})$ ) and  $u(V_{solids})$  based on the variance formula as follows. First, set

$$y = BD$$
,  $\frac{\partial y}{\partial M_{solids}} = \frac{1}{V_{soil}}$ ,  $\frac{\partial y}{\partial V_{soil}} = -\frac{M_{solids}}{V_{soil}^2}$ 

and calculate the uncertainty as 
$$u_c(BD) = \sqrt{u(M_{solids})^2 \left(\frac{1}{V_{soil}}\right)^2 + u(V_{solids}) \left(-\frac{M_{solids}}{V_{soil}^2}\right)^2}, \text{ or equivalently as}$$
 
$$u_c(BD) = BD \sqrt{\left(\frac{u(M_{solids})}{M_{solids}}\right)^2 + \left(\frac{u(V_{solids})}{V_{soil}}\right)^2}$$

- 10.5.12 For the purposes of obtaining a combined standard uncertainty utilizing repeated random sampling of input data or distributions (i.e., utilizing Monte Carlo simulations and related approaches), the following rules apply:
  - (a) The combined uncertainty shall be quantified through utilization of a probabilistic model where repeated random sampling (or resampling 106) of input data or distributions is employed to propagate measurement uncertainties, model uncertainties, and other input variability through the model to obtain an explicit empirical probability distribution of values reasonably attributable to the measurand. 107
  - (b) The combined standard uncertainty shall be quantified as the standard deviation of the resulting simulated or resampled distribution of the measurand.
  - (c) The CO<sub>2</sub> Removal Supplier shall provide thorough documentation of the probabilistic model employed, which shall at least include:
    - (i) a general description of the model including the simulation or resampling algorithm used and how uncertainty sources are propagated;
    - (ii) a step-by-step outline of the modelling process flow, including key modeling parameters (e.g. number of iterations/samples utilized) and relevant convergence diagnostics;
    - (iii) definition of all model parameters, input distributions, and other inputs, including references to the scientific literature, supporting data or other sources used for their selection;
    - (iv)description of all modelling assumptions (e.g. the choice of input distributions), along with their justification based on scientific literature, pre-existing data, measurement information, or other scientific rationale.

<sup>&</sup>lt;sup>106</sup> In statistics, resampling refers to the creation of new samples based on a previous observed sample. This is the basis of e.g. the bootstrapping approach, where resampling (with replacement) from the original sample is used to estimate the sampling distribution of a statistical estimator. It is important to note that a key principle of resampling is that variables that were measured jointly (e.g., from the same sample) need to be resampled together to account for covariances between the variables. For example, the concentrations of base cations and immobile tracer elements need to be resampled jointly rather than individually to implicitly capture the covariance between the two.

<sup>&</sup>lt;sup>107</sup> For general guidance on Monte Carlo simulations and related approaches, the CO<sub>2</sub> Removal Supplier should refer to applicable standards, particularly ISO/IEC Guide 98-3:2008/Suppl 1:2008, as well as relevant scientific literature and technical guidance (Davison & Hinkley, 1997; Efron & Tibshirani, 1994; Papadopoulos & Yeung, 2001; Shi et al., 2015; J. Zhang, 2021). Furthermore, there exist several online tools and software packages relevant for uncertainty estimation utilizing the Monte Carlo approach, such as the simple NIST uncertainty machine (Lafarge & Possolo, 2015), as well as the more extensive Monty package for simulating geochemical data in the context of ERW (Baum et al., 2024).

- 10.5.13 For the purposes of obtaining a combined standard uncertainty utilizing Bayesian inference, the following rules apply:
  - (a) The combined uncertainty shall be quantified through utilization of a probabilistic model where Bayes' theorem is used to combine information from measurements with prior information about the possible (or likely) distribution of values of the measurand to generate an explicit posterior probability distribution describing an updated probabilistic estimate of values reasonably attributable to the measurand.<sup>108</sup>
  - (b) The combined standard uncertainty shall be quantified as the standard deviation of the resulting Bayesian posterior probability distribution for the measurand.
  - (c) The CO<sub>2</sub> Removal Supplier shall provide a thorough documentation of the probabilistic model utilized, which shall at least include:
    - (i) a general description of the model including algorithms utilized and how uncertainty sources are propagated
    - (ii) a step-by-step outline of the modelling process flow, including key modeling parameters (e.g. metrics related to the sampling algorithms utilized) and relevant convergence diagnostics;
    - (iii) definitions of all model parameters, prior distributions, likelihood functions, and other inputs, including references to the scientific literature, supporting data or other sources used for their selection;
    - (iv) description of all modelling assumptions (e.g. the choice of prior distributions), along with their justification based on scientific literature, pre-existing data, measurement information, or other scientific rationale.

<sup>&</sup>lt;sup>108</sup> For general guidance on constructing Bayesian models, the CO<sub>2</sub> Removal Supplier should refer to applicable standards (e.g. ISO/TR 13587:2012, and applicable parts of ISO/IEC Guide 98-3:2008/Suppl 1:2008), as well as relevant scientific literature and technical guidance (Baum et al., 2024; Brus et al., 2022; Clark, 2005; Gelman et al., 2020; Kruschke, 2015; McElreath, 2020).

# 11 Sampling, Measuring, and Quantification Approaches

# 11.1 Homogeneous Strata, Application, Evaluation, and Control Sites

In a Production Facility the field site is composed of one or more homogeneous strata (see figure 3.2) which share similar agricultural, application, and soil characteristics defined in rule 11.1.1. Each stratum is further subdivided into application and control sites (see figure 3.2). The designated control site will be subject to the monitoring protocols, as will a subset of the application site selected as the evaluation area.

Stratification is used to ensure that comparisons between application and control sites are scientifically valid, and that observed differences in carbon removal or environmental impact can be attributed to the ERW activity rather than underlying variability in site conditions. In practice, the number of control sites per homogeneous stratum can be as low as 1 (although a larger number is recommended as a backup in case of unexpected land use change, contamination, or other confounders) as long as the following rules are adhered to:

- 11.1.1 The CO<sub>2</sub> removal supplier shall apply a stratified sampling strategy by identifying *homogeneous strata* made up of fields with similar agronomic and soil properties defined in subrules a-d.
  - (a) When assigning plots to homogeneous strata, the CO<sub>2</sub> removal supplier shall ensure that each stratum is consistent with respect to at least the following criteria:
    - (i) **Climatic conditions**: a single homogeneous stratum shall fall within a single Köppen-Geiger climate zone including precipitation and temperature subgroups (Beck et al., 2018).
    - (ii) Applied ERW **feedstock type**, application density, and timing of application shall be consistent across all fields within a stratum.
    - (iii) **Soil properties**: a single homogeneous stratum shall contain only a single soil type, as defined in rule 11.1.2.
    - (iv) **Agronomic practice**: tillage, irrigation, past and present fertilizer application or liming, as well as past ERW application shall be consistent within each homogeneous stratum. In case of unexpected changes in agricultural practice during a monitoring period, these changes shall be documented and their impact shall be evaluated in consultation with the Issuing Body.

- (b) Additionally, the strata should be similar with respect to crop type. Crops are subject to rotation during a given growing season but homogeneous strata should as much as possible be delineated in a way as to contain only one type of crop at any given time during a monitoring period.
- (c) Additionally, the strata should be similar with regards to the parameter measured in the chosen quantification approach for C<sub>stored</sub>.
- (d) Additional quantitative parameters should be chosen to maximize similarity within strata, which include but are not limited to soil pH, pH buffering capacity, base saturation, CEC, SOC, SIC, slope, and other soil properties with relevance to feedstock weathering.
- 11.1.2 The CO<sub>2</sub> Removal supplier shall ensure that plots assigned to the same homogeneous stratum possess similar soil properties as further defined in subrules a-c.
  - (a) The CO<sub>2</sub> Removal supplier shall determine similarity in soil properties according to an appropriate predefined categorical or numerical classification system (table 9.2).
    - (i) Plots with soils belonging to the same category (subrule b) or cluster (subrule c) shall be deemed as possessing similar soil properties.
  - (b) For categorical classification, the CO<sub>2</sub> Removal Supplier shall utilize a preexisting, commonly utilized soil classification framework, such as the USDA Soil Taxonomy system (ST),<sup>109</sup> the World Reference Base for Soil Resources (WRB),<sup>110</sup> or similar locally relevant soil classification systems.
    - (i) The CO<sub>2</sub> Removal Supplier shall select an appropriate hierarchy level for classification.
    - (ii) As a recommendation, the CO<sub>2</sub> Removal Supplier should utilize the Suborder level of the USDA ST, the Reference Soil Group level of the WRB, or a similar level of granularity in other classification systems.

<sup>&</sup>lt;sup>109</sup> USDA Natural Resources Conservation Service. Keys to Soil Taxonomy, 13th Edition. Washington, D.C.: United States Department of Agriculture, 2022.

<sup>&</sup>lt;sup>110</sup> IUSS Working Group WRB. 2022. World Reference Base for Soil Resources. International soil classification system for naming soils and creating legends for soil maps. 4th edition. International Union of Soil Sciences (IUSS), Vienna, Austria.

- (iii)Where the application of a more refined soil classification system is not possible or feasible, the CO<sub>2</sub> Removal Supplier may utilize the major soil texture classification defined by the USDA.<sup>111</sup>
- (c) For numerical classification, the CO<sub>2</sub> Removal Supplier shall utilize clustering (e.g. K-means clustering) or similar numerical classification based on a distance metric (e.g. the Euclidean or Mahalanobis distance) calculated from relevant soil parameters affecting weathering.<sup>112</sup>
  - (i) The utilized clustering method shall be based on peer-reviewed scientific literature relating to the numerical classification of soils. See e.g. Ng & McBratney, 2025; Zhu et al., 2025.
  - (ii) The parameter space utilized as the basis for clustering shall at least include the soil pH and CEC, as well as relevant texture parameters (percentage sand, silt, and clay).<sup>113</sup>
  - (iii) The CO<sub>2</sub> Removal Supplier shall utilize feature scaling (e.g. Z-score normalization) to normalize the range of the variables in the parameter space prior to calculation of pairwise distances.
  - (iv) The CO<sub>2</sub> Removal Supplier shall utilize a clustering metric (e.g., the silhouette coefficient) and/or a distance cutoff to determine appropriate clustering.
  - (v) Inside a given cluster, the standard deviations of all parameters shall be smaller than the standard deviation of the corresponding parameter across the whole Production Facility (e.g. for plots belonging to the same cluster, the standard deviation of the soil pH must be smaller than the standard deviation of soil pH for all plots in the Production Facility, and similarly for other variables).

<sup>&</sup>lt;sup>111</sup> In this classification, the major texture classes are sand, loamy sand, sandy loam, loam, silt loam, silt, sandy clay loam, clay loam, silty clay loam, sandy clay, silty clay, and clay. The textures are classified by the fractions of sand, silt, and clay present in a soil, and are often represented in the form of a triangle plot.

<sup>&</sup>lt;sup>112</sup> Although significant research has been conducted on numerical systems of soil classification since at least the 1960s (see e.g. Rayner, 1966), most of these methods are not often utilized outside case studies (Ng & McBratney, 2025; Zhu et al., 2025). However, while categorical classification systems like the USDA Soil Taxonomy or the World Reference Base are much more common, they are designed to be generic and broadly applicable, and cannot provide a quantitative taxonomic difference between soils (Dotto et al., 2020). On the other hand, numerical classification schemes, while less well-known, could offer a more purpose-focused classification based on key properties affecting weathering.

<sup>&</sup>lt;sup>113</sup> Note that utilizing all three texture parameters in numerical classification might not be useful as these parameters are not linearly independent (i.e., the percentages of sand, silt, and clay cannot all be varied independently as one of them is determined by the other two).

- (vi)The CO<sub>2</sub> Removal Supplier shall not utilize fuzzy clustering (i.e., a point shall not belong to more than one cluster).
- 11.1.3 Similarity in quantitative parameters between fields for the purpose of identifying homogeneous strata (see rule 11.1.1) shall be determined by pre-application measurements of the relevant parameters (see also rule 9.3.5).
- 11.1.4 Each homogeneous stratum shall be further stratified as defined in subrules a-d.
  - (a) Each homogeneous stratum shall be subdivided into an application site with a designated evaluation area, and a control site, as defined in rule 3.9.2.
  - (b) The homogeneous stratum shall be subdivided into application site, control site and evaluation area utilizing either the two plot approach or the three-plot approach defined as follows.
    - (i) Two-plot approach: the homogeneous stratum is subdivided into a control site and an application site.
    - (ii) Three-plot approach: the homogeneous stratum is subdivided into a control site, an application site, and an evaluation area.
  - (c) For each homogeneous stratum, the minimum percentage share of the total stratum area to be assigned as the control site area and evaluation area shall each be determined as follows (see also examples in table 11.1).

$$p_{min} = 0.055 = 5.5\%$$
  $A \le 10 \ ha$  (11.1)

$$p_{min} = \frac{1}{200} (14 - 3 \log_{10}(\frac{A}{ha})) \qquad 10 \ ha < A < 10 \ 000 \ ha$$
 (11.2)

$$p_{min} = 0.01 = 1\%$$
  $A \ge 10\ 000\ ha$  (11.3)

(d) The CO<sub>2</sub> Removal Supplier shall utilize appropriate sampling strategies (e.g. split field, randomized control, grid sampling) in assigning application, evaluation, and control site areas within a stratum in order to avoid systematic patterns or other bias between the areas.

Variable	Description	Unit
$p_{min}^{}$	Minimum percentage share of the total stratum area to be assigned as the control site and evaluation area (each separately).	0/
Α	Total stratum area in hectares.	ha
$log_{10}(x)$	The base 10 logarithm of the input number <i>x</i>	unitless

**Table 11.1.** Minimum requirements for the areal extent of control and evaluation per homogeneous stratum. Note that the evaluation area is the subset of the application site that is monitored for C<sub>stored</sub> quantification and validation.

Stratum Size (ha)	Control Site Area	Evaluation Area
≤10	5.5%	5.5%
100	4%	4%
1,000	2.5%	2.5%
5,000	1.5%	1.5%
≥10,000	1%	1%

#### **Control Sites**

Control sites are plots of land within the Production Facility to which Enhanced Rock Weathering is not applied but which are monitored to quantify the field-component of C<sub>baseline</sub> for the CORC equation (see figure 5.1) as described in section 6.2. Thus, the purpose of control sites is to enable quantification of the baseline scenario, which is equivalent to the counterfactual (or *business-as-usual*) scenario.

- 11.1.5 Control sites shall be treated in the same way as the agricultural plots that are part of the Production Facility used to be treated prior to and would have been treated in the absence of the Enhanced Rock Weathering activity, including in the following regards:
  - (a) **Liming**: limestone rock shall be applied at the same frequency and quantities to control sites as in the counterfactual scenario, i.e., the business-as-usual case at a given location before the ERW activity.
  - (b) **Fertilizer use**: Enhanced Rock Weathering can replace or reduce the use of traditional fertilizers. Fertilizers should be applied to control sites at the frequency and quantity of the counterfactual scenario.
  - (c) **Agronomic practices**: if the Enhanced Rock Weathering activity leads to any changes in agronomic practices (e.g., frequency of tillage), these practices shall be implemented on control sites as in the counterfactual scenario
- In cases where liming applies as a counterfactual (would have been part of business as usual) but a carbon dioxide removal supplier cannot correct for counterfactual liming practices by liming the control site, a conservative estimate of the counterfactual carbon dioxide removal must be made and added to C<sub>baseline</sub> (rule 5.3.1).

- (a) This conservative estimate shall take into account the amount of counterfactual liming based on documented records and assume complete carbonic-acid weathering of all limestone that would have been deployed in the counterfactual scenario as per the following equation, i.e., assuming 1 mol of CO<sub>2</sub> sequestered per 1 mol of CaCO<sub>3</sub> equivalents (see equation 1.4) in limestone applied under the counterfactual scenario.
- (b) This conservative estimate for CO<sub>2</sub> removed in the counterfactual liming scenario may be corrected for the loss terms in rules 6.3.3-6.3.11 prior to addition of the resulting value to C<sub>baseline</sub>.
- 11.1.7 Control sites shall be selected in a way that minimizes contamination risk from application sites; e.g., control sites downhill of application sites are at risk to receive weathering material via surface-runoff.

# 11.2 Sampling

A proper sampling protocol is crucial to ensure representative and accurate measurements resulting in detectable weathering signals. This section describes the requirements for sampling within the homogeneous strata, which are comprised of application and control sites (see section 11.1 and figure 3.2).

# **Sampling tools**

# Soil sampling tools

Typical soil sampling tools include augers, tubes or cores and simple shovels. Augers are one of the most commonly used tools, available in various designs such as bucket, spiral, and Edelman augers, each suited for different soil textures. Soil cores provide intact soil columns that preserve natural stratification and bulk density. Piston corers can be useful for deeper profiles, as they minimize soil compression and disturbance during extraction. Tube samplers and split-tube samplers are often employed for undisturbed soil sampling, providing high-quality cores for laboratory analysis. Shovels and trowels, while convenient for quick soil sampling, are not precise enough for ERW projects, which require accurate control over sampling depth. In the context of this document, soil samples are expected to be cores that are later homogenized to integrate the soil between the soil surface and the bottom of the soil core sample. Such soil core samples can be used for several C<sub>stored</sub> quantification approaches (section 11.2): CAT<sub>Ti</sub>, CAT<sub>WM</sub>, SIC<sub>soil</sub>.

## Soil water sampling tools

Soil water can exist in a myriad of tensions (tension-free or gravitational to hygroscopic water), and in a variety of locations within the soil matrix (micropore vs. macropore). Further, soil water flow paths differ as a function of soil moisture and may change from one precipitation event to the next. Thus, the chemical composition of soil water is naturally dynamic and spatially heterogeneous. However, several tools exist that can be employed to obtain an estimation of the processes operating

in the soil environment. It is important to note that for all tools, the volume of water collected is typically sporadic and inconsistent between replicates. Some studies show that vacuum tools show higher concentrations in comparison to tension-free samples (Barbee & Brown, 1986; Giesler et al., 1996; S. Buckingham et al., 2008) but divergence of vertical soil water flow around tension-free lysimeters can be a problem (Wöhling et al., 2009). Nevertheless, given that tension-free tools are generally better at estimating solute export from the soil profile (i.e., leaching fluxes), they seem also to be the most appropriate tool for C<sub>stored</sub> calculations, while vacuum-tools can be useful for understanding geochemical processes occurring at the micropore level.

The most widely used tools for soil pore water collection are vacuum soil water sampling tools such as rhizon samplers and porous ceramic cups (in some texts interchangeably called lysimeters). Both devices intend to imitate the suction of soil pore water by roots by applying a vacuum force to pull out soil pore water. Although effective and commonly utilized, care must be taken in interpreting data collected from these tools. The porosity of the samplers will dictate what parts of the soil pore water will be collected. Rhizons typically have sub-micrometer pore sizes, which, if working properly, has the advantage of avoiding a filtering step before measurements. On the other hand, the small permeable tips can lead to selective sampling due to adsorption forces in the soil. Ceramic cups are more complex and come in different sizes. They can collect higher pore water volumes (few hundreds of millimeters) in comparison to the rhizons that can only collect 20 to 40 mL of water pulled into syringes. As ceramic cup tips typically have higher porosity (on the micron scale) than rhizon samplers, samples need to be filtered before most measurements to eliminate microorganism and solid particles using at least ≤0.45 µm (better 0.2 µm) filters. Vacuum soil water sampling tools collect water that is in the soil pore space at the time of sample collection and therefore results from these sampling methods represent a discrete snapshot in time rather than an integrated measurement of longer-term conditions.

Passively collecting soil water sampling tools like vacuum-free lysimeters (e.g., pan lysimeters) have been applied in various agronomic and ERW studies to measure leachate soil water. These devices collect soil drainage/leachate water into a closed sampler (such as a cup). Most designs include a relatively large sample chamber (e.g., several liters in volume). This means that chemical re-equilibration will occur inside the sample chamber due to air contact in between each sampling event (which could be days or even months apart, depending e.g. on the rain conditions and potential irrigation systems). As a consequence of these subsequent reactions, some parameters (e.g. pH and DIC) might no longer be representative of the soil pore chemistry by the time of collection and measurement. On the other hand, compared to vacuum tools, lysimeter samples integrate the cumulatively leached ions over longer periods of time. Samples collected in lysimeters require filtering before measurements (0.45 µm filters are recommended to eliminate microorganisms and solid particles).

As a final subcategory, **cation exchange resins** (discussed in detail also in section 11.2, Approach 5 - CAT<sub>resin</sub>) do not in fact collect soil water but are installed within the soil, where they directly capture cations dissolved in soil water via negatively charged surface sites. These captured cations can then

be analysed after resin retrieval and elution with strong acids. Thus, cation exchange resins can also provide time-integrated measurements of leached cations over longer periods. Resin-based sensors now exist that can measure the amount of leached cations in-situ, enabling the creation of continuous time-series data on cation export.

11.2.1 For each quantification approach (section 11.3), appropriate and consistent sampling tools shall be used within a given monitoring period. Each sampling tool used (e.g. auger, lysimeter), shall be linked to (a) relevant monitored parameter(s) in the monitoring plan.

#### **Definition of a soil sample**

- 11.2.2 A soil sample shall consist of a number of subsamples that are combined to make up a representative, composite soil sample of the data point location where it is collected as further specified in subrules a-c:
  - (a) One soil sample shall consist of at least 5 subsamples but should ideally consist of 15 or more subsamples. If less than 15 subsamples are taken, the CO<sub>2</sub> Removal Supplier shall justify this choice by demonstrating that appropriate statistical evaluation is possible with the applied number of subsamples.
  - (b) Soil subsamples making up a single composite soil sample shall be collected within a radius of 5 to 15 m from a central point (which should be georeferenced).
  - (c) Subsamples should then be homogenized to form a single composite sample per site and time point ( $t_0$ ,  $t_1$ ) that is then sent to analysis.

#### Definition of a soil water sample

11.2.3 A soil water sample shall be defined as the water (or dissolved ions collected from soil water) collected by a soil water sampling device (see above: Soil water sampling tools) at a given point in time (discrete samples from vacuum-based tools) or over a longer continuous period of time (integrated samples from passive tools or resins).

#### Sampling frequency

- 11.2.4 For quantification of C<sub>stored</sub>, sampling and associated measurements shall be performed at least twice for each monitoring period at all designated control and application sites:

  1) shortly before or after (depending on quantification approach) feedstock application (t<sub>0</sub>); 2) at the end of the monitoring period (t<sub>1</sub>). Note that these two measurement points are in addition to pre-application soil characterization measurements (see section 9.3), which may, however, be re-used for t<sub>0</sub> measurements in cases where t<sub>0</sub> is measured before feedstock application (rule 9.3.4).
- 11.2.5 Additional samples (between  $t_0$  and  $t_1$ ) may be taken at various times during the monitoring period to improve and inform data evaluation and operational decisions.

11.2.6 CDR quantification approaches based on soil water sampling do not inherently integrate the weathering signal between time points  $t_0$  and  $t_1$ . In these cases, sampling frequency or duration shall be increased beyond  $t_0$  and  $t_1$  measurements in a way that ensures quantitative capturing of the weathering signal. This can be achieved by longer-term (weeks to months; Milliken et al., 2025) continuous sampling (for time-integrating sampling tools such as passive lysimeters) and/or higher sampling frequency (for non-time-integrating sampling tools such as vacuum-based soil water samplers). For more details, see the section on sampling tools.

# Sampling density for C<sub>stored</sub> quantification

- 11.2.7 For the quantification and validation of the gross amount of CO<sub>2</sub> sequestered (C<sub>stored</sub>), the number of samples taken from each homogeneous stratum (section 11.1) shall be determined in accordance with subrules a-c (see also tables 11.2-11.5).
  - (a) The number of samples shall be sufficiently large to enable the quantification of enhanced weathering signals at a statistically significant level (see rule 6.2.15) within each homogeneous stratum.
  - (b) The minimum number of samples taken from each homogeneous stratum shall be determined as follows.<sup>114</sup>

$$N_{min} = \max(9, \operatorname{ceil}(k \times \sqrt{A}, 3))$$
(11.4)

(i) For the quantification approach (see rule 11.3.1):

for soil samples: 
$$k = 3$$
 (11.5)

for soil porewater 
$$k = 1$$
 (11.6) samples:

(ii) For the validation approach (see rule 11.3.1):

for soil samples: 
$$k = \frac{3}{2}$$
 (11.7)

for soil porewater 
$$k = \frac{1}{2}$$
 (11.8) samples:

<sup>&</sup>lt;sup>114</sup> Note that the number and density of samples can have a significant effect on uncertainty and, by extension, the number of CORCs issued (see section 10.5, and esp. rule 10.5.3). Naturally, the CO<sub>2</sub> Removal Supplier may opt to take more samples than the prescribed minimum to limit the uncertainty in the gross amount of CO<sub>2</sub> sequestered (C<sub>stored</sub>). As the uncertainty is further affected by several project-specific factors (such as the quantification approach and the spatial and temporal heterogeneity), the potential further considerations for an optimum sample size should be informed by the uncertainty quantification and management process laid out in section 10.

- (c) The minimum number of samples taken from the evaluation area, the application site, and the control sites within a homogeneous stratum shall be determined as follows.
  - (i) For the two plot approach (see rule 11.1.4):

$$N_{min,control} = \frac{1}{3} N_{min} \tag{11.9}$$

$$N_{min,application} = \frac{2}{3} N_{min} \tag{11.10}$$

(ii) For the three-plot approach (see rule 11.1.4):

$$N_{min,control} = \frac{1}{3} N_{min} \tag{11.11}$$

$$N_{min,application} = \frac{1}{3} N_{min} \tag{11.12}$$

$$N_{min,evaluation} = \frac{1}{3} N_{min} \tag{11.13}$$

Variable	Description	Unit			
$N_{min}$	Minimum number of samples taken from a given homogeneous stratum.	unitless			
A		ha			
k	Scaling coefficient.				
ceil(x,3)	A function that rounds the input number $x$ upwards to the nearest multiple of three (e.g. $ceil(10,3) = 12$ ).				
$N_{min,control}$	Minimum number of samples taken from the control site.				
$N_{min,application}$	Minimum number of samples taken from the application site.				
$N_{min,evaluation}$	Minimum number of samples taken from the evaluation area.	unitless			

**Table 11.2.** Minimum soil sampling density for C<sub>stored</sub> quantification approaches: Sampling density required for quantification of C<sub>stored</sub> using a soil sampling quantification approach, expressed as the minimum number of samples required per homogeneous stratum taken on the stratum's control site, evaluation area, and non-evaluation area of the application site. The minimum number of samples is calculated in accordance with rule 11.2.7. This table provides examples for sample numbers required for various stratum sizes.

		3-Plot Soil Samples Min.			2-Plot Soil Min.	
Stratum Size (ha)	Min Total Samples	Control Site	Application Site	Evaluation Area	Control Site	Application Site
10	12	4	4	4	4	8
50	24	8	8	8	8	16
100	30	10	10	10	10	20
500	69	23	23	23	23	46
1000	96	32	32	32	32	64
5000	213	71	71	71	71	142

**Table 11.3.** Minimum porewater sampling density for C<sub>stored</sub> quantification approaches: Sampling density required for quantification of C<sub>stored</sub> using a soil water sampling quantification approach, expressed as the minimum number of samples required per homogeneous stratum taken on the stratum's control site, evaluation area, and non-evaluation area of the application site. The minimum number of samples is calculated in accordance with rule 11.2.7. This table provides examples for sample numbers required for various stratum sizes.

		3-Plot Water Samples Min.			2-Plot Water Min.	
Stratum Size (ha)	Min Total Samples	Control Site	Application Site	Evaluation Area	Control Site	Application Site
10	9	3	3	3	3	6
50	9	3	3	3	3	6
100	12	4	4	4	4	8
500	24	8	8	8	8	16
1000	33	11	11	11	11	22
5000	72	24	24	24	24	48

**Table 11.4.** Minimum soil sampling density for C<sub>stored</sub> validation approaches: Minimum sampling density required for validation of C<sub>stored</sub> using a soil sampling validation approach, expressed as the minimum number of samples required per homogeneous stratum taken on the stratum's control site, evaluation area, and non-evaluation area of the application site. The minimum number of samples is calculated in accordance with rule 11.2.7. This table provides examples for sample numbers required for various stratum sizes.

		3-Plot Soil Samples Min.			2-Plot Soil Min.	
Stratum Size (ha)	Min Total Samples	Control Site	Application Site	Evaluation Area	Control Site	Application Site
10	9	3	3	3	3	6
50	12	4	4	4	4	8
100	15	5	5	5	5	10
500	36	12	12	12	12	24
1000	48	16	16	16	16	32
5000	108	36	36	36	36	72

**Table 11.5.** Minimum porewater sampling density for C<sub>stored</sub> validation approaches: Minimum sampling density required for validation of C<sub>stored</sub> using a soil water sampling validation approach, expressed as the minimum number of samples required per homogeneous stratum taken on the stratum's control site, evaluation area, and non-evaluation area of the application site. The minimum number of samples is calculated in accordance with rule 11.2.7. This table provides examples for sample numbers required for various stratum sizes.

		3-Plot Water Samples Min.			2-Plot Water Min.	
Stratum Size (ha)	Min Total Samples	Control Site	Application Site	Evaluation Area	Control Site	Application Site
10	9	3	3	3	3	6
50	9	3	3	3	3	6
100	9	3	3	3	3	6
500	12	4	4	4	4	8
1000	18	6	6	6	6	12
5000	36	12	12	12	12	24

#### Sampling depth

- 11.2.8 The sampling depth for the quantification of ERW signals shall equal the depth of the near-field zone (NFZ, see rule 11.2.9). Furthermore, the sampling depth shall be consistent across sampling events (e.g.,  $t_0$ ,  $t_1$ ), at a given sampling site, and between control and application sites that are compared with each other (e.g., within a given homogeneous stratum).
- 11.2.9 The CO<sub>2</sub> Removal Supplier shall determine the depth of the near-field zone (NFZ) as further detailed in subrules a-c.
  - (a) The depth of the near-field zone shall be defined either as a fixed depth (see subrule b), or relative to soil horizons (subrule c).
    - (i) For consistency, the CO<sub>2</sub> Removal Supplier shall utilize the same definition (either fixed depth or along soil horizons) for all sites in the Production Facility.
  - (b) For the utilization of a fixed value, the depth of the NFZ shall be set to at least 20 cm, or 5 cm below the average tillage depth (whichever is larger).
    - (i) In cases where tillage is not practiced, the depth of the NZF shall be set to at least 20 cm.
    - (ii) In cases where the depth to the local groundwater table is less than the fixed value, the depth of the NZF shall be set to equal the depth to the local groundwater table.
  - (c) For the utilization of soil horizons, the depth of the NZF shall be determined as follows.
    - (i) The absolute depth (in cm) of the NFZ shall comply with the fixed depth requirements defined in subrule b, with the exception that up to 10% of samples may fall slightly (at most 5 cm) short of the sampling depth.
    - (ii) The relative depth (in relation to soil horizons) of the NFZ shall be selected by the CO<sub>2</sub> Removal Supplier in a consistent manner relative to the identified soil horizons.
    - (iii) The shallowest relative sampling depth shall be the middle of the A horizon.
- 11.2.10 The CO<sub>2</sub> Removal Supplier shall record the absolute sampling depth (in cm) of each sample.

Sampling along soil horizons: As an alternative to using an absolute NFZ depth, the NFZ depth may be defined relative to natural soil horizons (rule 11.2.9). For example, if the bottom of horizon A is used, samples must be taken to this depth regardless of the absolute depth (in cm) at various sampling sites across the field site. Sampling along soil horizons reduces the risk of mixing chemically and physically distinct soil layers and is expected to lead to better comparability of application and control site samples. The absolute depth of a given soil horizon will likely vary across a given field site and so flexibility is granted by allowing 10% of samples to be taken slightly above the minimum depth defined in rule 11.2.9 b, if necessary. When orienting NFZ depth along soil horizons, the CO<sub>2</sub> Removal Supplier should consider the following rationales:

- a. Topsoil sampling (horizon A), reflects nutrient and organic carbon fluxes, biological activity, and short-term weathering material reactions in the NFZ.
- b. Sub-soil sampling (horizon B), reflects nutrient leaching and more stable carbon pools.
- 11.2.11 The depth of the Near Field Zone (NFZ) has different implications for sampling for different quantification approaches (section 11.2):
  - (a) For approaches based on bulk-soil sampling (CAT<sub>WM</sub>, CAT<sub>Ti</sub>), the NFZ depth shall represent the lower end of the depth range within which the weathering signal is integrated, whereas the upper end of that range is the soil surface.
  - (b) For approaches based on soil-water sampling (CAT<sub>porewater</sub>, BIC<sub>porewater</sub>), the NFZ depth shall represent the depth from which pore water is sampled (e.g., lysimeter depth).
  - (c) For approach CAT<sub>sat</sub>, which extracts water from soil core samples, samples shall be taken in a way that allows the isolation of different vertical layers for later comparison of their cation concentrations. One or more layers taken above the NFZ depth represent the NFZ, whereas one or more layers below the NFZ depth represent the FFZ.
  - (d) For the resin-based approach (CAT<sub>resin</sub>), the resin shall be installed at a depth equalling the NFZ depth.
- In some situations and for some approaches, it may be desirable to take additional samples below the NFZ depth at the beginning and end of the monitoring period ( $t_0$  and  $t_1$ ), in order to avoid missing the weathering signal. Weathering signal determined on this basis may be taken into account to calculate C<sub>stored</sub>.

# 11.3 Quantification approaches

As of this writing (October 2025), there is no consensus on the best approach for quantification of gross CDR (C<sub>stored</sub>) through ERW, but several approaches have been suggested (table 6.1) and successfully applied in scientific studies of ERW (Amann et al., 2020, 2022; Dietzen et al., 2018; Haque et al., 2019, 2020; Jariwala et al., 2022; Khalidy et al., 2021; McDermott et al., 2024; Milliken et al., 2025).

C<sub>stored</sub> can be measured by tracking either the starting materials (reagents) or the end products of the weathering reaction (figure 1.1). As weathering reactions (i.e. hydrolysis and dissolution of weathering material) progress, the resulting products are transported from the weathering zone, i.e. the near field zone (NFZ), to deeper underground layers, and eventually into rivers, and ultimately the ocean, collectively denoted as the far field zone (FFZ). An effective quantification approach for C<sub>stored</sub> (and C<sub>baseline-[field]</sub>) is one that can accurately quantify the rate at which the weathering signal leaves the NFZ while using an appropriate weathering signal, i.e., a parameter that represents an accurate proxy for inorganic carbon.

**AGGREGATED QUANTIFICATION:** It is well known that high spatial variability of soil composition can significantly affect the accuracy and precision of CDR quantification resulting from enhanced weathering activities. This effect can be particularly pronounced at smaller scales (e.g., when quantifying CDR at the scale of individual plots as opposed to an aggregated value for an entire homogeneous stratum), as statistically aggregating (i.e., averaging) data over several plots can reveal effects that are obscured at the individual plot scale by noisy data.

In the context of carbon accounting, this type of data aggregation has been extensively applied in soil organic carbon management, demonstrating that aggregation across multiple plots can improve the accuracy of estimated carbon sequestration (Bradford et al., 2023; Potash et al., 2025). For enhanced rock weathering in particular, a similar analysis conducted recently by (Suhrhoff, Khan, et al., 2025) suggests that "aggregation across multiple fields substantially increases the robustness and accuracy of soil-based CDR, reducing both the average error and the risk of over-crediting, particularly when combined with adequate in-field sampling densities".

It is important to note that to ensure proper robustness, data aggregation practices need to be planned in advance (to avoid biased selection of data e.g, by exclusion from the analysis plots demonstrating no discernible CDR). Further, aggregation should be conducted over subsets of similar plots (i.e. similar in relevant properties, such as soil and feedstock composition, application amounts, etc.)—rather than randomly chosen plots—to produce a meaningful aggregate signal and to avoid, for example, disproportionately biasing the aggregated result towards large fields with most applied feedstock (Suhrhoff, Khan, et al., 2025).

For this methodology, it is strongly recommended that CO<sub>2</sub> Removal Suppliers utilize statistical data aggregation at the level of the homogeneous strata to increase the robustness of quantification and reduce uncertainties (i.e., rather than quantifying the CO<sub>2</sub> removal separately for each individual plot, measurement data should be averaged across a given homogeneous stratum to derive an aggregated result for the amount of CO<sub>2</sub> sequestered in that stratum). Note that aggregation across a stratum is also employed in the validation process for C<sub>stored</sub>, described in rule 11.3.1 b.

**Table 11.6.** Overview of sample treatment and analytical tools used for measurements in each approach.

Approach	Sample treatment	Analytical tools
	HF as in ISO 14869-3:2017. Aqua regia (HNO <sub>3</sub> +	Inductively Coupled Plasma Optical Emission Spectroscopy (ICP-OES), Inductively Coupled Plasma Mass Spectrometry (ICP-MS), Atomic Absorption Spectroscopy (AAS).
A2 - CAT <sub>Ti</sub>	material, e.g., dissolution with HCl + HNO <sub>3</sub> + HF as in ISO 14869-3:2017. Aqua regia (HNO <sub>3</sub> +	Inductively Coupled Plasma Optical Emission Spectroscopy (ICP-OES), Inductively Coupled Plasma Mass Spectrometry (ICP-MS), Atomic Absorption Spectroscopy (AAS).
A3 - CAT <sub>porewater</sub>		Inductively Coupled Plasma Optical Emission Spectroscopy (ICP-OES), Inductively Coupled Plasma Mass Spectrometry (ICP-MS), Atomic Absorption Spectroscopy (AAS), ex-situ ion selective electrodes.
BICporewater	analytical method used, but typically involves filtration.	DIC can be measured using infrared gas analysis, gas chromatography (GC), or coulometry. Titrations are used for total alkalinity (TA) measurements. Both TA and DIC require post-measurement corrections, see rule 11.3.7.
	the resin with a strong acid (e.g., NH <sub>4</sub> Cl/HCl).	Inductively Coupled Plasma Optical Emission Spectroscopy (ICP-OES), Atomic Absorption Spectroscopy (AAS). Some tools might have sensors for automated signals.
	water, equilibration at low temperature,	Inductively Coupled Plasma Optical Emission Spectroscopy (ICP-OES), Atomic Absorption Spectroscopy (AAS).
A7 - SICsoil	Method-dependent	Calcimetry, dry combustion.

- 11.3.1 The CO<sub>2</sub> Removal Supplier shall quantify the gross amount of carbon stored (C<sub>stored</sub>) (equation 5.1) based on data from two different measurement approaches (i.e. the quantification approach and verification approach), as further detailed in subrules a-c.
  - (a) The CO<sub>2</sub> Removal Supplier shall select the quantification approach and the validation approach in accordance with the following restrictions.
    - (i) The quantification and validation approaches shall be selected amongst the measurement approaches listed in table 6.1 and further described in section 11.3.
    - (ii) The quantification and validation approaches shall be of different types, i.e. they shall neither both be soil-based approaches (A1 and A2) nor shall they both be water-based approaches (A3-A6; see table 6.1).

- (iii) Approach A5 (CAT<sub>resin</sub>) shall not be utilized as a quantification approach and may only be utilized as a validation approach.
- (iv) Approach A7 (SIC<sub>soil</sub>) shall not be utilized as either a quantification approach or a validation approach. Rather, it is an optional approach that may be used independently of the other approaches to quantify additional carbon removal in the form of secondary carbonates (i.e., used on its own or added to removals resulting from one of the other quantification approaches run in parallel, and subject to restrictions detailed in rule 11.3.9).
- (v) The CO<sub>2</sub> Removal Supplier shall assign one and only one quantification approach for each homogeneous stratum.
- (vi)The CO<sub>2</sub> Removal Supplier shall assign one and only one validation approach for each homogeneous stratum in the validation set (see subrule b).
- (b) To validate the value for C<sub>stored</sub>, at, the CO<sub>2</sub> Removal Supplier shall adhere to the following procedure:
  - (i) The CO<sub>2</sub> Removal Supplier shall randomly select at least 50% of the homogeneous strata to be monitored with the validation approach in addition to the quantification approach (the remaining strata may be monitored with the quantification approach only). The strata thus selected are called the validation set.
  - (ii) For each stratum in the validation set, the CO<sub>2</sub> Removal Supplier shall derive values for the mean C<sub>stored</sub> in that stratum using both approaches (i.e., a pair of values, termed C<sub>stored</sub>, validation and C<sub>stored</sub>, quantification, for each stratum in the validation set).
  - (iii) The validation is considered passed if, for each stratum in the validation set, the two mean values C<sub>stored</sub>, validation and C<sub>stored</sub>, quantification are not different at the 99% confidence level based on the two-tailed Welch's t-test for unequal variances (or, equivalently, that the two-sided 99% confidence interval for the difference in means, calculated based on Welch's t-test, contains the value 0). Otherwise, the validation is considered failed.
  - (iv)If the validation is passed, the final value for C<sub>stored</sub> (i.e. the total aggregated value across all strata) shall be the value obtained using the quantification method.

- (v) If the validation fails, the CO<sub>2</sub> Removal Supplier shall provide explanation and justification for the discrepancy, which shall be subjected to the examination of the Issuing Body for potential approval as is or additional validation requirements.
- (c) The sampling requirements in section 11.2 (including but not limited to the minimum sampling density in table 11.2) apply separately to both the quantification and the validation method.
- 11.3.2 The Issuing Body may, in its sole discretion, approve the use of updated or revised equations for selected measurement approaches described in section 11.3 (i.e. updates or revisions to eqs. 11.14-11.50) subject to the following restrictions.
  - (a) Updates or revisions may be approved to incorporate new or updated scientific research pertaining to the measurement approaches described in this methodology, or to incorporate alternate but equivalent mathematical descriptions of the described approaches.<sup>115</sup>
  - (b) Updates or revisions shall be based on relevant peer-reviewed scientific research.
  - (c) The CO<sub>2</sub> Removal Supplier shall present evidence of equivalent or improved results (see subrules d-e) between the approach described in this methodology and the proposed update or revision (e.g. comparison of approaches for a subset of samples).
  - (d) Updates or revisions reflecting a significant alteration of the measurement approaches described in this methodology shall not be approved (i.e. this process shall not be utilized to approve entirely new measurement approaches).
  - (e) Updates or revisions shall not result in, nor be reasonably expected to result in, reduced conservativeness, accuracy, or precision in the quantification of carbon removal.

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<sup>&</sup>lt;sup>115</sup> For example, in the CAT<sub>Ti</sub> method, such updates or revisions might result from new scientific research pertaining to guidance on mobile/immobile element mass balance, or to utilize an equivalent method calculation based on the fraction of feedstock weathered, as detailed in Reershemius et al. (2023).

# Approach 1 - CAT<sub>WM</sub>

The CATwM approach assesses the extent of weathering by quantifying the loss of chemical elements from the weathering material (feedstock) in the NFZ. Cation concentration decrease in soil samples after feedstock application serves as a proxy for weathering products that have left the NFZ, indicating CO<sub>2</sub> sequestration.

For this approach, soil samples (section 11.2) are taken at least at the beginning ( $t_0$ ) and end ( $t_1$ ) of the monitoring period. Cations are then extracted from these samples by full-acid digestion and subsequently quantified by e.g., ICP-OES or ICP-MS (table 11.6).

Major cations that are typically present in weathering materials and can be used as weathering reaction proxies include Ca<sup>2+</sup>, Mg<sup>2+</sup>, K<sup>+</sup>, and Na<sup>+</sup>. For pure silicate feedstock, each positive charge in a weathered cation corresponds to one sequestered CO<sub>2</sub> molecule —consequently, due to their different charges, each mole of calcium or magnesium (with two positive charges) sequesters two moles of CO<sub>2</sub>, while potassium and sodium (with one positive charge each) sequester one mole of CO<sub>2</sub>. Importantly, any carbonates contained in the feedstock change this ratio between cation charge and carbon sequestered, because some carbon is released from the carbonate mineral itself during weathering. For example, for calcite weathering, only 1 mole of carbon is sequestered per mole of Ca<sup>2+</sup> released (eq. 1.4).

#### **Calculations**

After sample analysis, cation content is typically given in  $mg_{CAT}/L_{sample}$ . This value must be normalized to the mass of soil used in the digestion to obtain a mass concentration in  $mg_{CAT}/g_{soil}$  or ppm.

The CO<sub>2</sub> sequestration is estimated from the decrease of weathering material within the NFZ as indicated by the decrease in the major cation proxy during a monitoring period lasting from the beginning of the monitoring period ( $t_0$ , just after feedstock application) to its end ( $t_1$ ) in application and control sites as follows:

$$F1 = BD_{soil} \times d \times A_{ext} \tag{11.14}$$

$$F2 = \frac{Mw_{CO2}}{Mw_{CAT}} \times (n - f) \tag{11.15}$$

$$C_{stored} = \Delta CAT_{application} = (CAT_{t0} - CAT_{t1})_{application} \times F1 \times F2$$
 (11.16)

$$C_{baseline-[field]} = \Delta CAT_{control} = (CAT_{t0} - CAT_{t1})_{control} \times F1 \times F2$$
 (11.17)

$$\Delta CAT_{WM} = \Delta CAT_{application} - \Delta CAT_{control}$$
 (11.18)

Variable	Description	Unit
Aext	The field area to which weathering feedstock was applied that is represented by the evaluated sample or set of samples, i.e., the area to which the weathering signal may be extrapolated to, i.e., the area within a homogeneous stratum to which weathering feedstock was applied. Note that therefore the value of Aext will be the same for both Cstored (application sites) and Cbaseline-[field] (control sites)	$m^2$
$BD_{soil}$	Bulk density of soil (measured)	g <sub>soil</sub> /m <sup>3</sup>
d	Sampling depth = the depth the proxy signal is integrated over	m
$Mw_{CO2}$	Molecular weight of CO <sub>2</sub> = 44.01 g/mol	gco2/mol
$Mw_{CAT}$	Molecular weight of the measured cation	gcat/mol
п	Ionic charge of the cation considered ( $n = 2$ for Ca and Mg, $n = 1$ for K and Na)	unitless
f	The fraction of carbonate in feedstock expressed as equivalents of calcite (CaCO <sub>3</sub> ) <sup>116</sup>	percentage
F1	Factor equaling the amount of soil ( $g_{soil}$ ) in the extrapolation area ( $A_{ext}$ ) taking into account the depth over which the sample integrated ( $d$ ); multiplying with this factor therefore extrapolates the weathering signal per gram of soil to the field area this signal represents	<b>O</b> soil
F2	Factor converting the weathering signal in grams cations to a signal in grams CO <sub>2</sub> and correcting for the effect of feedstock carbon content on CDR potential.	0 .0
$CAT_i$	Concentration of the selected major cation proxy at $i = t_0$ or $i = t_1$	gcation / gsoil
$\Delta CAT_{application}$	Gross amount of carbon dioxide stored as carbonate and bicarbonate ions as measured as decrease in the major cation proxy within the NFZ of application sites (weathering signal) over the monitoring period, i.e., between to and to	
$\Delta CAT_{control}$	Amount of carbon dioxide stored as carbonate and bicarbonate ions on control sites as measured as decrease in the major cation proxy within the NFZ of control sites (weathering signal) over the monitoring period, i.e., between to and t <sub>1</sub> . Control sites represent the baseline of natural weathering that would have occurred also on application sites in the absence of the ERW activity	gCO <sub>2</sub>
$\Delta CAT_{WM}$	Baseline-corrected decrease in the NFZ-concentration of the cation proxy converted to amount of CO <sub>2</sub> removed during the monitoring period as quantified by the CAT <sub>WM</sub> approach	gCO2

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<sup>&</sup>lt;sup>116</sup>Expression of carbonate concentration as calcite (CaCO<sub>3</sub>) is common practice in soil analytics (e.g., FAO. 2020. Standard operating procedure for soil calcium carbonate equivalent. Titrimetric method. Rome) and is used here for simplicity in defining factor *f*.

**NEGATIVE OR INCONCLUSIVE WEATHERING SIGNALS:** When using the CAT<sub>WM</sub> approach, CDR by enhanced weathering is indicated if the following two conditions are met:

- 1.  $\Delta$ CAT<sub>application</sub> > 0: There should be a statistically significant net loss of chemical elements from the NFZ between the initial ( $t_0$ ) and final ( $t_1$ ) sampling periods in the application sites.
- 2. ΔCAT<sub>WM</sub> > 0: The weathering signal should be statistically significantly higher in the application sites compared to control sites, confirming that the measured change is due to actual material weathering.

A lack of these signals (i.e., a case where  $CAT_{application} < 0$  and/or  $\Delta CAT_{WM} < 0$ ) might indicate a lack of CDR and will be accounted for in this way with respect to carbon crediting. However, we note that such discrepancies could also result from other factors, such as

- a lack of similarity between control and application sites,
- addition or subtraction of weathering material by runoff,
- measurement errors, or
- other uncertainty and variability drivers.

Similar considerations will apply to a lack of signal from the other quantification approaches. Thus, all measurements should be evaluated and reported as part of the output audit, regardless of whether the conditions for crediting based on CATwm quantification are met. Comprehensive evaluation and reporting, including cases where no measurable change occurs, is essential for future avoidance of any false negatives, transparency, interpretation of variability, and comparability across sites and monitoring periods.

#### **Applicable loss terms**

Given that this approach measures the full removal of a proxy cation from the NFZ rather than directly quantifying carbonic acid weathering, discounts have to be made for non-carbonic acid dissolution (Lossacid) and cation uptake into plant biomass (Lossplant, rule 6.3.5) in addition to FFZ losses. The loss pathways Lossadsorb, Losscarbonate, and Losssilicate are implicitly accounted for by this approach if soil samples integrate over the entire depth of the NFZ and are treated with full-acid digestion.

- 11.3.3 The CO<sub>2</sub> Removal Supplier may use the CAT<sub>WM</sub> approach to quantify C<sub>stored</sub> according to eqs. 11.14-11.18 and taking into account subrules a-g:
  - (a) **Sample type:** Samples for CAT<sub>WM</sub> analysis shall be of type "Soil" and be obtained using an appropriate soil sampling technique and equipment.
  - (b) **Sampling depth:** The CAT<sub>WM</sub> analysis shall quantify the cation content in the entire soil sample core between the soil surface and the NFZ depth.

- (i) in cases where it is necessary to subdivide the full core into separate layers to enable detectability of the weathering signal, control site samples shall be treated identically
- (c) **Sample treatment:** Cations from soil samples for CAT<sub>WM</sub> analysis shall be extracted with total digestion methods (e.g., dissolution with HCl + HNO<sub>3</sub> + HF as in ISO 14869-3:2017), or alternatively by aqua regia digestion (i.e. dissolution with HNO<sub>3</sub> + HCl as in ISO 54321:2020) provided that both of the following conditions are met:
  - (i) aqua regia can be demonstrated to digest the vast majority (>90%) of utilized feedstock, and
  - (ii) a subset of measurements (at least 10% of samples for C<sub>stored</sub> at a given time point) are done after full digestion (ISO 14869-3:2017) to account for any secondary silicate losses potentially overlooked with the aqua regia approach.
- (d) **Analytical measurements:** Analysis of bulk soil cation concentrations shall be performed utilizing one of the following methods:
  - (i) inductively coupled plasma optical emission spectroscopy (ICP-OES), or
  - (ii) inductively coupled plasma mass spectrometry (ICP-MS), or
  - (iii) atomic absorption spectroscopy (AAS).
- (e)  $t_0$  measurements: The CO<sub>2</sub> Removal Supplier shall utilize either of the following approaches to determine the soil cation concentration immediately following feedstock application (i.e. at time  $t_0$ ):
  - (i) direct measurements of cation concentration in the soil-feedstock mix in field samples taken shortly after feedstock application.
  - (ii) separate measurements of cation concentrations in pre-application soil and dry feedstock (corrected for moisture content), respectively, combined with an estimate of spreading rate that is demonstrably accurate and reliably even as evidenced by agricultural logs including georeferenced spreading data.
- (f) The **carbon content of the utilized feedstock** shall be measured with an eligible method (table 3.1) in order to correct for the reduced CO<sub>2</sub> sequestration efficiency of carbonates compared to silicate minerals via factor *f* in eq. 11.15.
- (g) **Losses:** The CO<sub>2</sub> Removal Supplier shall account for all of the following loss terms:
  - (i) non-carbonic acid weathering (Lossacid, rule 6.3.4),

- (ii) plant uptake of major cations (Lossplant, rule 6.3.5),
- (iii) losses from surface freshwater systems (Lossrivers, rule 6.3.9), and
- (iv) losses from marine systems (Lossocean, rule 6.3.10).

# Approach 2 - CAT<sub>Ti</sub>

The CAT<sub>Ti</sub> approach is similar to the CAT<sub>WM</sub> approach in many respects and is described in recent scientific publications (Reershemius et al., 2023; Suhrhoff et al., 2024, 2025). This approach also uses soil samples (section 11.2) to assess the extent of weathering by quantifying the loss of major cations from the NFZ after feedstock addition. In addition to evaluating cation loss, immobile trace elements are used in CAT<sub>Ti</sub> to determine the percentage of the feedstock that has dissolved relative to the total amount applied.

The same set of chemical elements is used as weathering reaction proxies, including major cations such as Ca<sup>2+</sup>, Mg<sup>2+</sup>, K<sup>+</sup>, and Na<sup>+</sup>. Additionally, non-mobile (or less mobile relative to the aforementioned ones) minor trace elements such as Ti<sup>2+</sup>, Ni<sup>2+</sup>, Rb<sup>2+</sup> serve as additional proxies that document the lack of movement of the non-mobile part of the weathering material (Reershemius et al., 2023; Suhrhoff et al., 2024; Suhrhoff, Reershemius, et al., 2025). This ensures that any change in the major cations measured in parallel is due to weathering rather than physical loss of unweathered material (e.g., due to runoff).

CAT<sub>Ti</sub> requires the analysis of soil samples and/or feedstock cation composition using analytical instruments like ICP-MS or ICP-OES after full-acid digestion (table 11.6). The precise protocol for this approach as presented in eqs. 11.19-11.27 below, assumes the following minimum set of measurements:

- Major and trace cation content of feedstock prior to deployment,
- Major and trace cation content of field site soil samples taken prior to feedstock deployment (t<sub>0</sub>),
- Major and trace cation content of field site soil samples taken at the end of the monitoring period ( $t_1$ ).

#### **Alternative evaluation method**

Instead of using feedstock analysis to determine the ratio of cations to immobile trace elements, CO<sub>2</sub> removal suppliers using the CAT<sub>Ti</sub> approach can utilize the element ratios and cation concentrations found in soil samples taken shortly after feedstock application ( $t_0$ ), which represent a mix of soil and feedstock. This requires a different set of equations than those presented in eqs. 11.19-11.27 based on measuring the following parameters:

• Major and trace cation content of field site soil samples taken immediately after feedstock application ( $t_0$ )

• Major and trace cation content of field site soil samples taken at the end of the monitoring period ( $t_1$ )

If the post-application soil samples are being used for t<sub>0</sub>, then the calculations do not need to account for pre-application trace elements or prior monitoring periods. The weathering rate can be calculated based on the change in cation concentration relative to any changes in concentration of trace elements in the soil during the monitoring period.

#### Calculations for the CAT<sub>Ti</sub> evaluation method using pre-application t<sub>0</sub> measurements

After sample analysis (using the method described in table 11.6), cation content is typically given in  $mg_{CAT}/L_{sample}$ . This value must be normalized to the mass of soil used in the digestion to obtain a mass concentration in  $mg_{CAT}/g_{soil}$  or ppm.

The CO<sub>2</sub> sequestration is estimated from the decrease in concentration of mobile weathering material relative to the concentration of the immobile trace elements. The estimation of the decrease in the major cation proxy in the NFZ during the monitoring period is evaluated as follows:

$$R_{wm} = \frac{cAT_{wm}}{TI_{wm}} \tag{11.19}$$

$$TI_{ms} = TI_{t1} - TI_{to} (11.20)$$

$$CAT_{ms} = CAT_{t1} - CAT_{to} (11.21)$$

$$R_{ms} = \frac{cAT_{ms}}{TI_{ms}} \tag{11.22}$$

$$WR_{t1} = \frac{R_{wm} - R_{ms}}{R_{wm}} \tag{11.23}$$

$$\Delta CAT_{application} = WR_{t1} \times TI_{ms} \times R_{wm} \times F1 \times F2$$
 (11.24)

$$C_{stored} = \Delta CAT_{application} - \Delta CAT_{prior}$$
 (11.25)

$$C_{baseline-[field]} = \Delta CAT_{control} = (CAT_{t0} - CAT_{t1})_{control} \times F1 \times F2$$
 (11.26)

$$\Delta CAT_{Ti} = \Delta CAT_{application} - \Delta CAT_{control}$$
 (11.27)

Variable	Description	Unit
F1	Factor equaling the amount of soil ( $g_{soil}$ ) in the extrapolation area ( $A_{ext}$ ) taking into account the depth over which the sample integrated ( $d_{ext}$ ) multiplying with this factor therefore extrapolates the weathering signal per gram of soil to the field area this signal represents. See eq. 11.14.	);
F2	Factor converting the weathering signal in grams cations to a signal i grams CO <sub>2</sub> and correcting for the effect of feedstock carbon content o CDR potential. See eq. 11.15.	
$CAT_{t0}$	Major cation concentration in soil prior to feedstock application just before the beginning of the monitoring period ( $t_0$ ).	st gcation/gsoil
$CAT_{t1}$	Major cation concentration in the soil at the end of the monitoring perio $(t_1)$ .	d gcation/gsoil

Variable		Unit
$TI_{t0}$	Trace cation concentration in soil prior to feedstock application just before the beginning of the monitoring period ( $t_0$ ).	
$TI_{t1}$	Trace cation concentration in the soil at the end of the monitoring period $(t_1)$ .	mol/g <sub>soil</sub>
$CAT_i$	Concentration in the soil of the selected major cation proxy for $i = wm$ or $i = ms$ $i = wm$ : the cation concentration in the weathering material feedstock $i = ms$ : the cation concentration in the soil at $t_1$ after subtracting the baseline $t_0$ concentration	gcation / gsoi
$TI_i$	Concentration in the soil of the selected immobile trace elements for $i = wm$ or $i = ms$ $i = wm$ : the immobile trace element concentration in the weathering material feedstock $i = ms$ : the immobile trace element concentration in the soil added as part of the feedstock (i.e., at $t_1$ after subtracting the $t_0$ concentration)	mol/g <sub>soil</sub>
$R_i$	Ratio of concentrations of the major cation proxies to the relatively immobile trace elements $i = wm$ : Relative concentrations in the weathering material feedstock $i = ms$ : Relative concentrations in the soil	unitless
$WR_i$	Estimated weathering rate of the applied soil amendments based on comparing the concentrations of the trace elements and major cations in the soil at the end of the monitoring period, relative to the ratios found in the pre-application feedstock	unitless
$\Delta CAT_{application}$	Gross amount of carbon dioxide stored as carbonate and bicarbonate ions as measured as decrease in the major cation proxy within the NFZ of application sites (weathering signal) over the monitoring period, i.e., between $t_0$ and $t_1$ .	gCO2
$\Delta CAT_{control}$	Amount of carbon dioxide stored as carbonate and bicarbonate ions on control sites as measured as decrease in the major cation proxy within the NFZ of control sites (weathering signal) over the monitoring period, i.e., between $t_0$ and $t_1$ . Control sites represent the baseline of natural weathering that would have occurred also on application sites in the absence of the ERW activity.	gCO2
$\Delta CAT_{prior}$	Gross amount of carbon dioxide stored as carbonate and bicarbonate ions claimed during all prior monitoring periods. This value is 0 during the first monitoring period. This value is equal to the $\Delta CAT_{application}$ value from the previous monitoring period.	
$\Delta CAT_{Ti}$	Baseline-corrected decrease in the NFZ-concentration of the cation proxy converted to amount of CO <sub>2</sub> removed during the monitoring period as quantified by the CAT <sub>Ti</sub> approach.	

Given that this approach measures the full removal of a proxy cation from the NFZ rather than directly quantifying carbonic acid weathering, additional discounts have to be made for non-carbonic acid dissolution (Lossacid) and cation uptake into plant biomass (Lossplant, rule 6.3.5). The loss pathways Lossadsorb, Losscarbonate, and Losssilicate are implicitly accounted for by this approach if soil samples integrate over the entire depth of the NFZ and are treated with full-acid digestion (see table 11.6). The FFZ loss terms Lossrivers and Lossocean need to be accounted for.

- 11.3.4 The CO<sub>2</sub> Removal Supplier may use the CAT<sub>Ti</sub> approach to quantify C<sub>stored</sub> according to eqs. 11.19-11.27 and taking into account subrules a-h:
  - (a) **Sample type:** The CAT<sub>Ti</sub> analysis shall be performed based on soil samples and be obtained using an appropriate soil sampling technique and equipment.
  - (b) **Sampling depth:** The CAT<sub>Ti</sub> analysis shall quantify the cation content in the entire soil sample core between the soil surface and the NFZ depth.
    - (i) in cases where it is necessary to subdivide the full core into separate layers to enable detectability of the weathering signal, control site samples shall be treated identically
  - (c) **Sample treatment:** Cations from soil samples for CAT<sub>Ti</sub> analysis shall be extracted with total digestion methods (e.g., dissolution with HCl + HNO<sub>3</sub> + HF as in ISO 14869-3:2017), or alternatively by aqua regia digestion (i.e. dissolution with HNO<sub>3</sub> + HCl as in ISO 54321:2020) provided that both of the following conditions are met:
    - (i) aqua regia can be demonstrated to digest the vast majority (>90%) of utilized feedstock, and
    - (ii) a subset of measurements (at least 10% of samples for Cstored at a given time point) are done after full digestion (ISO 14869-3:2017) to account for any secondary silicate losses potentially overlooked with the aqua regia approach.
  - (d) Analytical measurements: Analysis of bulk soil cation concentrations shall be performed utilizing one of the following methods:
    - (i) inductively coupled plasma optical emission spectroscopy (ICP-OES), or
    - (ii) inductively coupled plasma mass spectrometry (ICP-MS), or
    - (iii) atomic absorption spectroscopy (AAS).

- (e) **Measurement points**: The CO<sub>2</sub> Removal Supplier shall utilize either of the following approaches to determine the decrease in cation concentration after feedstock application while observing the behavior of a trace cation as a proxy for feedstock loss to physical processes:
  - (i) The main approach described in eqs. 11.19-11.27 requires the following minimum set of measurements:
    - Major and trace cation concentration in feedstock prior to deployment
    - Major and trace cation content in field site soil samples taken prior to feedstock deployment (t<sub>0</sub>)
    - Major and trace cation content of field site soil samples taken at the end of the monitoring period (t1)
  - (ii) An alternative approach requires appropriate adjustment of eqs. 11.19-11.27 to the following minimum set of measurements:
    - Major and trace cation content of field site soil samples taken immediately after feedstock application (t<sub>0</sub>)
    - Major and trace cation content of field site soil samples taken at the end of the monitoring period (t1)
- (f) The **carbon content of the utilized feedstock** shall be measured with an eligible method (table 3.1) in order to correct for the reduced CO<sub>2</sub> sequestration efficiency of carbonates compared to silicate minerals via factor *f* in eq. 11.15.
- (g) **Losses:** The CO<sub>2</sub> Removal Supplier shall account for all of the following loss terms:
  - (i) non-carbonic acid weathering (Lossacid, rule 6.3.4),
  - (ii) plant uptake of major cations (Lossplant, rule 6.3.5),
  - (iii) losses from surface freshwater systems (Lossrivers, rule 6.3.9), and
  - (iv) losses from marine systems (Lossocean, rule 6.3.10).
- (h) **Subsequent monitoring periods:** In order to monitor the same area over multiple monitoring periods, including subsequent deployments of weathering materials, using the CAT<sub>Ti</sub> type quantification approach following eqs. 11.9-11.17, the initial pre-application  $t_0$  values shall be used. All prior  $C_{stored}$  values in the field area shall be subtracted from the  $C_{stored}$  values for the current monitoring period.

# **Approach 3 - CAT**porewater

In this approach the accumulated cations in soil porewater are measured in soil water samples (see section 11.2) taken at the base of the NFZ. Samples are then analyzed using analytical instruments like ICP-MS or ICP-OES (table 11.6).

Similar to approach 1 (CATwM),  $C_{stored}$  can be calculated individually for the different cation proxies (Ca<sup>2+</sup>, Mg<sup>2+</sup>, K<sup>+</sup>, and Na<sup>+</sup>), but the inclusion of several cations in the total  $C_{stored}$  quantification should be justified by site-specific context and supporting data.

#### **Calculations**

CO<sub>2</sub> sequestration is estimated from the concentration of the selected cation proxy in soil water that has accumulated in the sampling container (i.e., in the process of leaching from the NFZ) during a monitoring period in application and control sites as follows:

$$F_{sw} = P - ET - RO \tag{11.28}$$

$$F3 = \frac{F_{sw}}{V_{sample}} \times A_{ext} \tag{11.29}$$

$$C_{stored} = \Delta CAT_{application} = \sum CAT_{application} \times F3 \times F2$$
 (11.30)

$$C_{baseline-[field]} = \Delta CAT_{control} = \sum CAT_{control} \times F3 \times F2$$
 (11.31)

$$\Delta CAT_{porewater} = \Delta CAT_{application} - \Delta CAT_{control}$$
 (11.32)

Variable	Description	Unit
P	Volume of precipitation received per area of field.	L/m <sup>2</sup>
ET	Evapotranspiration per area of field.	L/m <sup>2</sup>
RO	Runoff estimate per area of field, calculated according to eq. 11.33.	L/m <sup>2</sup>
$F_{sw}$	Vertical water flux through the soil column.	L/m <sup>2</sup>
Aext	The field area to which weathering feedstock was applied that is represented by the evaluated sample or set of samples, i.e., the area to which the weathering signal may be extrapolated to, i.e., the area within a homogeneous stratum to which weathering feedstock was applied. Note that therefore the value of A <sub>ext</sub> will be the same for both C <sub>stored</sub> (application sites) and C <sub>baseline-[field]</sub> (control sites).	5 0 m <sup>2</sup>
$V_{sample}$	Soil water sample volume	m <sup>3</sup>
F3	Factor relating the net volume of water per area of field received from precipitation (corrected for evaporation and runoff) and the volume of soil water captured by the sampling devices to the area of field that the sample (or set of samples) represents; multiplying with this factor therefore extrapolates the weathering signal per volume of soil water to the field area this signal represents treating the volume of soil water captured as representative of the (likely larger) volume of water that has in fact passed through the soil during the monitoring period.	r f unitless
F2	Factor converting the signal in grams cations to a signal in grams CO <sub>2</sub> and correcting for the effect of feedstock carbon content on CDR potential. See eq 11.15.	

Variable	Description	Unit
$\sum CAT_i$	Amount of the cation proxy in the combined soil water (of volume $V_{sample}$ ) that has accumulated over the monitoring period (at $i = control\ site$ or application $site$ ). Note that water accumulated in soil sampling devices can and should be sampled more than once during a monitoring period.	<b>7</b> 0.00
	Gross amount of carbon dioxide stored as carbonate and bicarbonate ions as measured as export of the major cation proxy from the NFZ of application sites (weathering signal) over the monitoring period.	
$\Delta CAT_{control}$	Amount of carbon dioxide stored as carbonate and bicarbonate ions on control sites as measured as export of the major cation proxy from the NFZ of control sites (weathering signal) over the monitoring period. Control sites represent the baseline of natural weathering that would have occurred also on application sites in the absence of the ERW activity.	gCO2
$\Delta CAT_{porewater}$	Baseline-corrected decrease in the NFZ-concentration of the cation proxy converted to amount of $CO_2$ removed during the monitoring period as quantified by the $CAT_{porewater}$ approach.	

The loss pathway non-carbonic acid weathering (Lossacid) needs to be corrected for. The loss pathways Lossplant, Lossadsorb, Losscarbonate, and Losssilicate are implicitly accounted for by this approach if soil water is sampled at the base of the NFZ. The FFZ loss terms Lossrivers and Lossrivers need to be accounted for.

REMARK ON HOW TO ESTIMATE THE WATER VOLUME INFILTRATING THE SOIL **OVER A GIVEN PERIOD OF TIME:** For soil-water based C<sub>stored</sub> quantification approaches, we need to take into account a parameter we call soil water flux  $(F_{SW})$ , measured in units of volume of water per area and time (L m<sup>-2</sup> yr<sup>-1</sup>). To calculate it, we need an estimate of the following components: Precipitation, Evapotranspiration, and Runoff. Precipitation (P) is usually measured using a rain gauge and expressed in units of millimetres (mm) of height or depth. To convert these dimensions to volume of water per collection area 1 mm of precipitation equals 1 L/m<sup>2</sup>. Evapotranspiration (ET) is typically measured in millimetres of water (i.e. volume of water moved per unit area of the Earth's surface) in a set unit of time, where, again, 1 mm converts to 1  $L/m^2$ . Finally, runoff (RO) of precipitation describes water that precipitates above a given field area but does not percolate into the soil and instead is lost to the given area because it flows across its surface. It is again measured in mm and can be 1:1 converted to units of L/m<sup>2</sup>. Runoff can be determined using the runoff curve number (CN) developed by the USDA Natural Resources Conservation Service, an empirical parameter that can be combined with precipitation to estimate direct runoff as follows (Ponce & Hawkins, 1996):

$$RO = \frac{[CN \times (P+2) - 200]^2}{CN \times [CN(P-8) + 800]} \text{ for } P > (200/CN), \text{ otherwise: } RO = 0$$
 (11.33)

Using P, ET, and RO, we can calculate  $F_{sw}$  according to eq. 11.28.

11.3.5 The CO<sub>2</sub> Removal Supplier may use the CAT<sub>porewater</sub> approach to quantify C<sub>stored</sub> according to eqs. 11.15, 11.28-11.32 and taking into account subrules a-f:

- (a) **Sample type:** Samples for CAT<sub>porewater</sub> analysis shall be of type "Water" and be obtained using an appropriate soil water sampling technique and equipment.
- (b) **Sampling depth:** Soil water for CAT<sub>porewater</sub> analysis shall be collected at the base of the NFZ.
- (c) **Analytical measurements:** Analysis of dissolved cation concentrations shall be performed utilizing one of the following methods:
  - (i) inductively coupled plasma optical emission spectroscopy (ICP-OES), or
  - (ii) inductively coupled plasma mass spectrometry (ICP-MS), or
  - (iii) atomic absorption spectroscopy (AAS).
- (d) **Soil hydrology:** The parameters for calculating vertical water flow through the soil column ( $F_{sw}$ , eq. 11.28) shall be estimated on the basis of site-specific data and appropriate models as follows:
  - (i) **Precipitation (P):** Site-specific data for P shall be obtained from the public meteorological station nearest to the relevant field site, a private measurement station closer to the field site, or reliable database applications for the precise geographical location (e.g., ERA5-Land, Open-Meteo).
  - (ii) Evapotranspiration (ET): Site-specific data for ET shall be obtained from appropriate meteorological datasets (e.g., ERA5-Land; Muñoz-Sabater et al., 2021) in one of the following ways:
    - Site- and time-specific potential evaporation data from such datasets may be used directly under the simplifying and conservative assumption that potential evaporation equals actual ET.
    - As an alternative to this conservative assumption, actual ET may
      be estimated more accurately using appropriate methods and
      approaches, e.g., the Penman-Monteith approach or the
      Hargreaves-Samani approach (Rodrigues & Braga, 2021)
      combined with appropriate crop coefficients (Allen et al., 1998),
      and/or modeling (e.g., Hydrus-1D) to account for soil dryness.
  - (iii) **Runoff (RO):** Runoff shall be estimated by one the following means:
    - Solve the curve number (CN) equation (eq. 11.33) for direct runoff, using input values for site- and time-specific precipitation as described above and for site-specific CN as derived in one of the following ways:

- Derived from a CN table on the basis of site-specific information (Cronshey, 1986), or
- Derived from the high-resolution, global map of CN values by Jaafar et al. (2019) or an equivalent one.
- A hydrological box model, such as the box model included in the SMEW biogeochemical-hydrological model (Bertagni et al., 2024).
- A numerical model solving Richards equation, e.g., Hydrus-1D.
   When using Hydrus-1D, at least the following modeling elements shall be applied:
  - Site-specific input parameters for precipitation and evapotranspiration (from empirical sources, see above) as well as site-specific soil parameters, including soil density and soil texture (table 9.2)
  - Appropriate boundary condition settings, including ponding/runoff enabled and consideration of site-specific water table depth for bottom boundary
  - Appropriate root uptake function with root uptake set to occur only within the NFZ depth range
  - Estimate van Genuchten-Mualem soil hydraulic parameters (Schaap et al., 2001) and solve Richards equation
  - Time resolution: hourly steps or more resolved
  - Vertical resolution: 1 cm or less in the top 10 cm
- (e) The **carbon content of the utilized feedstock** shall be measured with an eligible method (table 3.1) in order to correct for the reduced CO<sub>2</sub> sequestration efficiency of carbonates compared to silicate minerals via factor f in eq. 11.15.
- (f) **Losses:** The CO<sub>2</sub> Removal Supplier shall account for all of the following loss terms:
  - (i) non-carbonic acid weathering (Lossacid, rule 6.3.4),
  - (ii) losses from surface freshwater systems (Lossrivers, rule 6.3.9), and
  - (iii) losses from marine systems (Lossocean, rule 6.3.10).

# Approach 4 - BICporewater

In the BIC<sub>porewater</sub> approach, accumulated bicarbonate and carbonate ions, the primary dissolved products of carbonic-acid weathering, are measured in soil water samples (see section 10.6) taken at the base of the NFZ. Two chemical proxies can be used for this approach: total alkalinity (TA) and dissolved inorganic carbon (DIC). Each method provides different insights and has distinct limitations (Mills et al., 2024).

**TA** measures a solution's capacity to neutralize acid and is defined as the excess of proton acceptors (e.g.,  $HCO_3-$ ,  $CO_3^2-$ , OH-) over proton donors (H<sup>+</sup>).

$$TA = [HCO_3^-] + 2[CO_3^2] + [B(OH)_4] + [OH] - [H] + (any other relevant ions)$$
 (11.34)

As illustrated in eq. 11.34, TA increases with the release of bicarbonate ions during silicate weathering. TA is relatively stable across environmental conditions, making it a more robust indicator of long-term carbon sequestration. However, TA also has drawbacks as a proxy for CDR in soils. While reliable in carbonate-buffered systems like seawater, TA measurements in soil porewater are complicated by non-carbonate acid-base species, such as phosphates, ammonium, and especially organic acids, which contribute to alkalinity without reflecting atmospheric CO<sub>2</sub> removal (Bijma et al., 2025). Thus, interpreting TA as a proxy for CDR in soils requires caution and context-specific calibration and correction.

**DIC** is the total amount of inorganic carbon species in solution, hence the sum of  $CO_2$  (aq),  $HCO_3^-$ , and  $CO_3^{2-}$ :

$$DIC = [CO_{2(aq)}] + [HCO_3^-] + [CO_3^{2-}]$$
(11.35)

DIC is not conserved under open-system conditions. It varies with pH, temperature, and  $CO_2$  partial pressure (pCO<sub>2</sub>). For example, if soil warms or acidifies,  $CO_2$ (aq) can degas into the atmosphere, reducing DIC without reversing the weathering reaction. TA, by contrast, remains stable in this case, as proton balances shift without a net loss of alkalinity. Still, neither DIC nor TA alone provides a complete picture of carbon removal; both must be interpreted alongside system boundaries,  $CO_2$  sources, and geochemical context.

#### Approach 4a - BIC<sub>porewater</sub> (Total alkalinity - TA)

For total alkalinity measurement of a water sample, a known volume of the sample is titrated with a standardized strong acid, typically 0.02--0.1~N HCl or  $\text{H}_2\text{SO}_4$ , while monitoring the pH. The titration proceeds until the solution reaches a pH of approximately 4.5, at which point all carbonate species, primarily bicarbonate (HCO<sub>3</sub>-) and carbonate (CO<sub>3</sub><sup>2</sup>-), are protonated to carbonic acid (H<sub>2</sub>CO<sub>3</sub>), which rapidly decomposes into CO<sub>2</sub>(aq) and water. This CO<sub>2</sub>(aq) is rapidly degassed from the solution, especially if the sample is stirred or exposed to air, effectively removing the carbonate species as gas.

Given that TA is a measure of the total buffering capacity of a solution, it accounts for all titratable bases (i.e., proton acceptors). Thus, other weak acid/base conjugates besides bicarbonate and

carbonate present in soil waters can contribute to TA (table 11.7). To accurately measure CO<sub>2</sub> sequestration using total alkalinity, the contribution of other weak acid/base conjugates has to be identified, quantified, and corrected for to isolate the alkalinity specifically derived from carbonic acid weathering. In particular, organic alkalinity can have a large influence in sol water. It can be quantified by titration after CO<sub>2</sub> removal by acidification and subsequent re-alkalinization (using NaOH) of a sample (Kerr et al., 2023; Song et al., 2023). It should be noted that Kerr et al.'s "OrgAlk" titration protocol will capture not only organic alkalinity but also other non-carbonate alkalinity such as alkalinity from phosphates, which is desirable in the context of correcting TA for non-carbonate alkalinity of any type as part of the BIC<sub>porewater</sub> approach. In addition to their organic-alkalinity measurement protocol, Kerr et al. (2023) provide an open-source, Python-based calculator that can be used for organic-alkalinity correction. Additionally, the pH needs to be measured and a geochemical modeling software (e.g., PHREEQC) used in order to assess the relative contributions of HCO<sub>3</sub>- and CO<sub>3</sub>- to alkalinity. The CO<sub>2</sub> sequestration is estimated from the difference of accumulated bicarbonate species in leachate waters from the NFZ between the application site(s) and the control site(s) over a monitoring period.

**Table 11.7.** Key weak acid/base conjugates that can contribute to total alkalinity (TA) at pH ranges relevant for soils.

Species	Conjugate base form	pKa (approximately)	Relevant pH Range
Bicarbonate	HCO₃⁻	6.3	5.5 – 8.5
Carbonate	CO <sub>3</sub> <sup>2-</sup>	10.3	> 9.5
Fulvic and humic acids	R-COO- / R-O-	4 – 7	5 – 8
Dihydrogen Phosphate	H <sub>2</sub> PO <sub>4</sub> -	2.15	< 5
Hydrogen Phosphate	HPO <sub>4</sub> <sup>2-</sup>	7.2	6 – 8.5
Hydrogen sulfide	HS-	7.0	~6.5 – 8

#### Approach 4b - BIC<sub>porewater</sub> (Dissolved inorganic carbon - DIC)

This method quantifies the total concentration of inorganic carbon species in soil water, including aqueous carbon dioxide ( $CO_2(aq)$ ), bicarbonate ( $HCO_3^-$ ), and carbonate ( $CO_3^{2-}$ ). Among these,  $CO_2(aq)$  does not represent durable carbon sequestration and must be excluded from crediting because it is highly transient under open-system conditions such as near-surface soils, where it can readily degas to the atmosphere. Therefore, care must be taken to minimize  $CO_2$  exchange between sampled soil water and the atmosphere after sampling by keeping temperature low and constant and minimizing contact with the atmosphere.

To isolate the bicarbonate and carbonate fractions, the measured DIC must be corrected by estimating and removing the  $CO_2(aq)$  component. This can be done using carbonate speciation calculations based on measured DIC, pH, and temperature.

#### Calculations for approaches 4a and 4b

CO<sub>2</sub> sequestration is estimated from the concentration of the accumulated bicarbonate/carbonate proxy in soil water that has accumulated in the sampling container (i.e., in the process of leaching from the NFZ) during a monitoring period in application and control sites as per the equations below. The equations below assume that the analytical data are in units of charge equivalents (unitless, for approach 4a) and grams carbon (gc, for approach 4b):

$$F4_{ALK} = Mw_{CO2} \times n$$
 (for approach 4a) (11.36)

$$F4_{DIC} = \frac{{}^{Mw_{CO2} \times n}}{{}^{Mw_C}} \quad (for approach 4b)$$
 (11.37)

$$C_{stored} = \Delta BIC_{application} = \sum BIC_{application} \times F3 \times F4$$
 (11.38)

$$C_{baseline-[field]} = \Delta BIC_{control} = \sum BIC_{control} \times F3 \times F4$$
 (11.39)

$$\Delta BIC_{porewater} = \Delta BIC_{application} - \Delta BIC_{control}$$
 (11.40)

Variable	Description	Unit
Mw <sub>co2</sub>	Molecular weight of CO <sub>2</sub> = 44.01 g/mol	gco2/mol
$Mw_{C}$	Molecular weight of carbon = 12.01 g/mol	gc/mol
F3	Factor relating the net volume of water per area of field received from precipitation (corrected for evaporation and runoff) and the volume of soil water captured by the sampling devices to the area of field that the sample (or set of samples) represents; multiplying with this factor therefore extrapolates the weathering signal per volume of soil water to the field area this signal represents, treating the volume of soil water captured as representative of the (likely larger) volume of water that has in fact passed through the soil during the monitoring period. See eqs. 11.28 and 11.29.	unitless
n	n represents the mean charge of DIC in the sample as determined by pH measurement and geochemical modeling/calculation, see above.	unitless
F4 <sub>ALK</sub>	Factor converting charge-equivalents (from alkalinity measurements) to grams CO <sub>2</sub> sequestered, assuming that one charge-equivalent can bind one mole of bicarbonate.	<b>g</b> CO2
F4dic	Factor converting grams of inorganic carbon (from DIC measurements) to grams CO <sub>2</sub> .	gco2/gc
F4	Approach 4a: substitute F4ALK, Approach 4b: substitute F4DIC	
$\sum BIC_i$	Amount of the (bi)carbonate proxy in the combined soil water (of volume $V_{\text{sample}}$ ) that has accumulated over the monitoring period (at $i = control$ site or application site). Note that water accumulated in soil sampling devices can and should be sampled more than once during a monitoring period.	A-4a: unitless
$\Delta BIC_{application}$	Gross amount of carbon dioxide stored as carbonate and bicarbonate ions measured as export of the (bi)carbonate proxy from the NFZ of application sites (weathering signal) over the monitoring period.	

Variable	Description	Unit
$\Delta BIC_{control}$	Amount of carbon dioxide stored as carbonate and bicarbonate ions on control sites as measured as export of the major cation proxy from the NFZ of control sites (weathering signal) over the monitoring period. Control sites represent the baseline of natural weathering that would have occurred also on application sites in the absence of the ERW activity.	gCO2
$\Delta BIC_{porewater}$	Baseline-corrected decrease in the NFZ-concentration of the (bi)carbonate proxy converted to amount of CO <sub>2</sub> removed during the monitoring period as quantified by the BIC <sub>porewater</sub> approach.	

The loss pathways Loss<sub>plant</sub>, Loss<sub>adsorb</sub>, Loss<sub>carbonate</sub>, Loss<sub>acid</sub>, and Loss<sub>silicate</sub> are implicitly accounted for by this approach if soil water is sampled at the base of the NFZ. The FFZ loss terms Loss<sub>rivers</sub> and Loss<sub>rivers</sub> need to be accounted for.

- 11.3.6 The CO<sub>2</sub> Removal Supplier may use the BIC<sub>porewater</sub> approach to quantify C<sub>stored</sub> according to eqs. 11.28, 11.29, and 11.36-11.40, and taking into account subrules a-f:
  - (a) **Sample type:** Samples for CAT<sub>porewater</sub> analysis shall be of type "Water" and be obtained using an appropriate soil water sampling technique and equipment. Samples should be collected using tension lysimeters or soil solution samplers that minimize degassing.
  - (b) Sampling depth: Soil water for CAT<sub>porewater</sub> analysis shall be collected at the base of the NFZ.
  - (c) Analytical TA measurements (Approach 4a): total alkalinity shall be analyzed by acid titration protocols designed for TA (e.g., ISO 9963-1:1994). In order to correct for non-carbonate alkalinity, the TA measurements shall be corrected for the following parameters:
    - (i) **organic alkalinity:** direct measurements of organic alkalinity ("OrgAlk" titration) and subsequent correction of TA for organic alkalinity shall be conducted as described by Kerr et al. (2023). Small deviations from this protocol (e.g., in titration increments, reagent concentration) shall be allowed if properly justified. It is recommended to modify Kerr et al.'s Python calculator in a way to disable the subtraction of phosphate-alkalinity from the "OrgAlk" titration results, in which case the requirements of subrule ii. may be ignored.

- (ii) **phosphates**, but only in cases where soil phosphate concentrations exceed the analytical uncertainty of the TA measurements, e.g., due to phosphate fertilization. Where required, phosphate shall be measured by spectrophotometry (ISO 6878:2004) or ion chromatography (ISO 10304-1:2007) and subtracted from TA taking into account phosphate speciation based on the pH determined at the beginning of the titration.
- (d) Analytical DIC measurements (Approach 4b): DIC shall be analyzed by infrared-gas analysis (IRGA), coulometry, or gas chromatography (GC) after acidification inside gas-tight vials. Then the measured DIC value shall be converted into an estimate of [bicarbonate + carbonate] using appropriate geochemical modeling tools (e.g., CO2SYS, PHREEQC) as well as the following parameters measured in samples or in-situ in parallel to DIC:
  - (i) soil pH,
  - (ii) soil temperature, and
  - (iii)ionic strength (unless demonstrably <0.01 mol/L) measured as electrical conductivity (ISO 11265:2025), calculated by summing up major ions from cation (e.g., ICP-OES) and anion (e.g., ion chromatography) analyses, or total dissolved solids (e.g., weighed evaporation residue, gravimetry).
- (e) **Soil hydrology:** The parameters for calculating vertical water flow through the soil column ( $F_{sw}$ , eq. 11.28) shall be estimated on the basis of site-specific data and appropriate models as described in subrule 11.3.6 d.
- (f) **Losses:** The CO<sub>2</sub> Removal Supplier shall account for all of the following loss terms:
  - (i) losses from surface freshwater systems (Lossrivers, rule 6.3.9), and
  - (ii) losses from marine systems (Lossocean, rule 6.3.10)

# Approach 5 - CAT<sub>resin</sub>

Ion exchange resins (polymer beads widely used in environmental monitoring) work by adsorbing cations (positively charged ions) from the surrounding soil solution in a process similar to how roots or clay particles retain nutrients. When a cation exchange resin is placed in soil, it does not directly attract cations from solid soil particles. Instead, the cations must be dissolved in soil pore water to be adsorbed by the resin. The negatively charged functional groups on the resin attract and bind cations from the water. As cations bind to the resin, it releases an equivalent charge of counterions (H<sup>+</sup> or Na<sup>+</sup>) to maintain charge balance.

Cation exchange resins can capture Ca<sup>2+</sup>, Mg<sup>2+</sup>, K<sup>+</sup>, Na<sup>+</sup>, Al<sup>3+</sup>, Fe<sup>3+</sup>, and other positively charged ions from soil water after they are placed in the soil. However, a variety of different types of resins exist for different purposes and use cases. For example, sulfonic acid (-SO<sub>3</sub><sup>-</sup>) resins are strong-acid resins working across a broad pH range (typically pH 1–14), phosphonic acid (-PO<sub>3</sub>H<sup>-</sup>) resins are specialized for metal ion binding, whereas carboxyl (-COO<sup>-</sup>) resins are weak-acid based and typically lose efficiency at low pH values (<4-5). After their use and subsequent recovery from the soil, cations need to be extracted from the resins using suitable extractants (e.g., NH<sub>4</sub>Cl/HCl mixture; Santos et al., 2024) and then analyzed using appropriate tools (table 11.6).

Given that resins provide a cumulative quantification of cation adsorption, CO<sub>2</sub> sequestration is estimated from the cations accumulated on the resins from fluxes across the bottom boundary of the NFZ over the course of a monitoring period as follows:

$$C_{stored} = \Delta CAT_{application} = \frac{CAT_{application}}{A_{resin}} \times F2 \times A_{ext}$$
 (11.41)

$$C_{baseline[field]} = \Delta CAT_{control} = \frac{CAT_{control}}{A_{resin}} \times F2 \times A_{ext}$$
 (11.42)

$$\Delta CAT_{resin} = \Delta CAT_{application} - \Delta CAT_{control}$$
 (11.43)

Variable	Description	Unit
	The field area to which weathering feedstock was applied that is represented by a given site sampled by the resin, i.e., the area to which the weathering signal	
	may be extrapolated to, i.e., the area within a homogeneous stratum to which weathering feedstock was applied. Note that therefore the value of Aext will be the same for both Cstored (application sites) and Cbaseline-[field] (control sites).	
Aresin	The surface area of the resin that is in contact with and can interchange ions with the surrounding soil water.	$m^2$
F2	Factor converting the weathering signal in grams cations to a signal in grams CO2 and correcting for the effect of feedstock carbon content on CDR potential. See eq. 11.15	
	Amount of the selected major cation proxy collected by the resin throughout the monitoring period in $i = application$ site or $i = control$ site.	<b>g</b> cation
	Gross amount of carbon dioxide stored as carbonate and bicarbonate ions as measured as export of the major cation proxy from the NFZ of application sites (weathering signal) over the monitoring period.	

Variable	Description	Unit
$\Delta CAT_{control}$	Amount of carbon dioxide stored as carbonate and bicarbonate ions on control sites as measured as export of the major cation proxy from the NFZ of control sites (weathering signal) over the monitoring period. Control sites represent the baseline of natural weathering that would have occurred also on application sites in the absence of the ERW activity.	gCO2
$\Delta CAT_{resin}$	Baseline-corrected decrease in the NFZ-concentration of the cation proxy converted to amount of CO <sub>2</sub> removed during the monitoring period as quantified by the CAT <sub>porewater</sub> approach.	

#### Limitations of this approach

Under dry soil conditions, resins may desiccate, limiting their ability to capture cations. A recent study (Santos et al., 2024) showed that acid-extraction after resin recovery from the soil can dissolve any ERW feedstock stuck to the resin, thereby artificially inflating cation measurements. Such biased measurements need to be avoided by careful resin recovery and placement of the resin below the depth to which feedstock is mixed into the soil. Generally, as of this writing (October 2025), peer-reviewed evidence for the efficacy of cation exchange resins in quantifying CDR in ERW is lacking. Because of the discussed limitations and the lack of scientific studies demonstrating the effectiveness of this approach for CDR quantification in ERW, the CAT<sub>resin</sub> approach may only be used as a validation method under this methodology.

- 11.3.7 The CO<sub>2</sub> Removal Supplier may use the CAT<sub>resin</sub> approach to validate C<sub>stored</sub> according to eqs. 11.41-11.43 and taking into account subrules a-g:
  - (a) **Sample type:** Samples for CAT<sub>resin</sub> analysis shall be of type "Water" and be obtained using appropriate cation exchange resins.
  - (b) **Sampling depth:** The CAT<sub>resin</sub> analysis shall quantify the cation flux across the base of the NFZ by placing the resins at the NFZ depth.
  - (c) The **experimental design** of the CAT<sub>resin</sub> measurements shall comply with the following requirements.
    - (i) The CO<sub>2</sub> Removal Supplier shall determine an appropriate type of utilized resin based on its efficiency under site-specific conditions (especially soil texture, dryness) and the project-specific cation(s) used for evaluation.
    - (ii) The resin shall be placed at the NFZ depth to sample cations from across the NFZ and avoid direct contact with feedstock.

- (iii)To constrain the volume of influence<sup>117</sup> on the resins, the CO<sub>2</sub> Removal Supplier shall utilize resin cores with a pre-defined diameter and length, which are separated from the soil matrix by an impermeable divider along the length of the core.
- (iv) The justification for the experimental design shall be documented and reported as part of the Production Facility Audit.
- (d) **Extraction:** if applicable (i.e., if ex-situ analysis as in subrule c-i. to c-iii. is applied), appropriate techniques shall be applied to extract cations from the resins, e.g., NH<sub>4</sub>Cl/HCl extraction as described by Santos et al. (2024).
- (e) **Analytical measurements:** Analysis of sample cation content shall be performed utilizing one of the following methods:
  - (i) inductively coupled plasma optical emission spectroscopy (ICP-OES), or
  - (ii) inductively coupled plasma mass spectrometry (ICP-MS), or
  - (iii) atomic absorption spectroscopy (AAS), or
  - (iv)appropriately tested and calibrated, integrated sensors.
- (f) The **carbon content of the utilized feedstock** shall be measured with an eligible method (table 3.1) in order to correct for the reduced CO<sub>2</sub> sequestration efficiency of carbonates compared to silicate minerals via factor *f* in eq. 11.15.
- (g) **Losses:** The CO<sub>2</sub> Removal Supplier shall account for all of the following loss terms:
  - (i) non-carbonic acid weathering (Lossacid, rule 6.3.4) except if the CO<sub>2</sub> removal supplier can demonstrate that the utilized resins do not react with non-carbonic acid weathering derived cations,
  - (ii) losses from surface freshwater systems (Lossrivers, rule 6.3.9), and
  - (iii) losses from marine systems (Lossocean, rule 6.3.10).

<sup>&</sup>lt;sup>117</sup> The volume of influence on the resin refers to the volume of soil from which ions can be exchanged and collected by the resin. As resins might accumulate ions not only from the water percolating through it, but also by (lateral) diffusion, constraining the volume of influence (e.g., by preventing lateral diffusion into the resin with impermeable side walls) is important for the robust quantification of the cation flux.

# Approach 6 - CAT<sub>sat</sub>

CAT<sub>sat</sub>, as applied to ERW, is a novel approach for extracting porewater from soil cores by centrifugation. Centrifugation-based porewater extraction techniques have long been used for soil science applications, but the approach described here adds the component of saturating the soil core with deionized water (DIW), which has several advantages in the context of ERW (Skov et al., *submitted*, and citations therein).

While this approach is based on analyzing the dissolved constituents of soil-water flushed out with DIW, the sampling approach underlying CAT<sub>sat</sub> is the same as for the soil-based approaches A1 and A2. Compared to other soil-water based approaches, this has the advantage that the ability to take a sample at any point in time does not depend on sufficiently high soil moisture, which can avoid data gaps and biases as well as operational difficulties. Furthermore, this approach eliminates the need for installing soil-water sampling equipment, which can improve ease of collaboration with agricultural partners.

In order to use the CAT<sub>sat</sub> approach for measuring CDR by ERW (i.e., the export of base cations from the NFZ to deeper soil layers, see rule 2.3.1), samples need to be taken in a way that allows the isolation of different vertical soil layers for later comparison of their cation concentrations. One or more intervals or layers on top represent the NFZ, while the remaining layers below can be used to record cations that have been exported from the NFZ.

In the approach described by Skov et al. (*submitted*), soil core samples are pre-weighed, then placed into bags and saturated with 60-100 mL (depending on soil sample volume) deionized water (DIW). After removing air from the bags, the samples are left to equilibrate at 4°C. After 24 hours, the sample is centrifuged at 1000 rpm for 30 minutes and the resulting supernatant is filtered to obtain a water sample that can be analyzed for its cation (and anion) concentration. Dry-weight of the soil samples after oven-drying (105°C, 24 hours) can be used to assess soil moisture and density.

The analytical procedure for CAT<sub>sat</sub> is similar to CAT<sub>porewater</sub> (A3) as both approaches measure dissolved cations in soil water. Thus, dissolved cation analyses by ICP-MS, ICP-OES, or AAS are required.

The approach described here markedly differs from similar approaches (Jones et al., 2025) in the experimental step of saturating a soil core with DIW. Conceptually, this saturation allows for the quantification of the readily leachable ions in the pore water solution that would have been flushed out of the NFZ into deeper soil layers by the next rain event. Importantly, the saturation step also allows for the efficient extraction of porewater at lower centrifugation speed (Skov et al., *submitted*). By contrast, the higher centrifugation speed employed by Jones et al. (2025) resulted in significantly higher extraction of cations compared to parallel lysimeter extraction, which was attributed by these researchers to the extraction of cations from micropores. While such micropore-derived cations may well be the result of ERW, it is unclear whether they are sufficiently mobile to be subject to exporting from the NFZ as a consequence of rain events in the near future. Therefore, the CAT<sub>sat</sub> approach

requires moderate centrifugation speeds, which in most cases will require the addition of DIW in the sample treatment process.

#### **Calculations**

CO<sub>2</sub> sequestration is estimated from the concentration of the selected cation in soil water extracted from soil samples after centrifugation. The soil moisture content and known volume of DIW added must be used to correct the input concentrations for any experimental dilution of the soil water with DIW. The cation concentration (CAT) entered into the following equation then needs to be normalized to the dry weight of the soil it represents (units g<sub>CAT</sub>/g<sub>soil</sub>):

$$C_{stored} = \Delta CAT_{application} = \sum_{i} (CAT_{peak(i)} - CAT_{min(i)})_{application} \times F1 \times F2$$
 (11.44)

$$C_{baseline-[field]} = \Delta CAT_{control} = \sum_{i} (CAT_{peak(i)} - CAT_{min(i)})_{control} \times F1 \times F2$$
 (11.45)

$$\Delta CAT_{porewater} = \Delta CAT_{application} - \Delta CAT_{control}$$
(11.46)

Variable	Description	Unit
F1	Factor equaling the amount of soil (g <sub>soil</sub> ) in the extrapolation area (A <sub>ext</sub> ) taking into account the depth over which the sample integrated (d); multiplying with this factor therefore extrapolates the weathering signal per gram of soil to the field area this signal represents. See eq. 11.14	g <sub>soil</sub>
F2	Factor converting the signal in grams cations to a signal in grams CO <sub>2</sub> and correcting for the effect of feedstock carbon content on CDR potential. See eq. 11.15	
$CAT_{peak(i)}$	Concentration of the cation proxy at a local or absolute maximum $i$ during the monitoring period.	gCAT/gsoil
$CAT_{min(i)}$	Concentration of the cation proxy at a local or absolute minimum $i$ following the local or absolute maximum $i$ .	gCAT/gsoil
$\sum_{i} (CAT_{peak(i)} - CAT_{min(i)})$	This term represents the sum (or integrated flux) of cations transported from the NFZ to the FFZ as determined by cation decrease following cation peaks in the NFZ.	
$\Delta CAT_{application}$	Gross amount of carbon dioxide stored as carbonate and bicarbonate ions as measured as export of the major cation proxy from the NFZ of application sites (weathering signal) over the monitoring period, i.e., between $t_0$ and $t_1$ .	
$\Delta CAT_{control}$	Amount of carbon dioxide stored as carbonate and bicarbonate ions on control sites as measured as export of the major cation proxy from the NFZ of control sites (weathering signal) over the monitoring period, i.e., between $t_0$ and $t_1$ . Control sites represent the baseline of natural weathering that would have occurred also on application sites in the absence of the ERW activity.	gc02

The loss pathways non-carbonic acid weathering (Lossacid) and cation uptake into plant biomass (Lossplant, rule 6.3.5) needs to be corrected for. The loss pathways Lossadsorb, Losscarbonate, and Losssilicate are implicitly accounted for by this approach since cations removed by these loss processes will not find their way into the sample unless they are so loosely sorbed (Lossadsorb) or bound in such soluble minerals (Losscarbonate) that the next rain event would have had the same dissolving effect as the DIW treatment. The FFZ loss terms Lossrivers and Lossrivers need to be accounted for.

### Requirements for CAT<sub>sat</sub>

- 11.3.8 The CO<sub>2</sub> Removal Supplier may use the CAT<sub>sat</sub> approach to quantify C<sub>stored</sub> according to eqs. 11.14-11.15 and 11.44-11.46 and taking into account subrules a-g:
  - (a) **Sample type:** Samples for CAT<sub>sat</sub> analysis shall be of type "Water" but shall be obtained using an appropriate soil sampling technique and equipment.

#### (b) Measurement timepoints:

- (i) *to* samples shall be taken either shortly before or shortly after feedstock application to the soil.
- (ii)  $t_{peak}$  samples are those taken at times that are identified as corresponding most closely to local or absolute cation concentration maxima; note that the likelihood of closely approximating all occurring  $t_{peak}$  time points will increase with sampling frequency during the monitoring period.
- (iii)  $t_{min}$  samples are those taken at times that are identified as corresponding most closely to local or absolute cation concentration minima; note that the likelihood of closely approximating all occurring  $t_{min}$  time points will increase with sampling frequency during the monitoring period.
- (iv)  $t_1$  samples shall be defined as the final sample taken at the end of a monitoring period.
- (c) **Quantification of weathering and cation export:** The CAT<sub>sat</sub> analysis shall quantify weathering and NFZ-export by measuring the cation concentration in at least two (2) vertical layers of the soil sample core with the interface between two layers situated at the NFZ depth (rule 11.2.10).
  - (i) Weathering (rule 2.3.1 a) shall be quantitatively demonstrated by measured cation increase within the layer(s) representing the NFZ relative to corresponding  $t_0$  samples and in application sites compared to control sites.
  - (ii) Cation export of the weathering proxy from the NFZ (rule 2.3.1 b) shall be quantitatively demonstrated in at least one of the following ways:

- by a measured decrease in the NFZ cation concentration subsequent to previously measured cation increase (i.e., a cation peak) in the NFZ relative to to or—in cases where more than one peak and cation export event occurs during a single monitoring period—a previous documented cation concentration minimum (happening after to) within the monitoring period; or
- by a measured cation increase in layer(s) below the NFZ (relative to cation concentrations at *t*<sub>0</sub> below the NFZ); note that this approach requires an appropriate adjustment to eqs. 11.44-11.46, which are designed to solve for cation loss from the NFZ rather than cation increase below the NFZ.
- (iii) Multiple cation peaks and minima may occur in and below the NFZ. The cation decrease after each peak within the NFZ or the cation increase below the NFZ after each minimum—both implying cation export from the NFZ (subrule ii.)—may be summed up to quantify total cation export across the monitoring period.

#### (d) Sample treatment:

- (i) Samples may be treated (saturated with DIW) in order to allow for effective water extraction by centrifugation but this step may also be skipped as long as control sites and application site samples are treated the same and the centrifugation speed requirement (see subrule iv.) is followed;
- (ii) Incubation of soil samples saturated with DIW shall occur at constant temperature below the natural soil temperature (recommendation: 4°C);
- (iii) Centrifugation speed used to obtain water samples from the supernatant shall not exceed 1000 rpm and centrifugation time shall not exceed 30 minutes;
- (iv) The centrifugation supernatant shall be obtained by filtration with filter pore size not smaller than 0.20  $\mu$ m nor larger than 0.45  $\mu$ m.
- (e) **Analytical tools:** Analysis of sample cation content shall be performed utilizing one of the following methods:
  - (i) inductively coupled plasma optical emission spectroscopy (ICP-OES), or
  - (ii) inductively coupled plasma mass spectrometry (ICP-MS), or
  - (iii) atomic absorption spectroscopy (AAS).

- (f) The **carbon content of the utilized feedstock** shall be measured with an eligible method (table 3.1) in order to correct for the reduced CO<sub>2</sub> sequestration efficiency of carbonates compared to silicate minerals via factor *f* in eq. 11.15.
- (g) **Losses:** The CO<sub>2</sub> Removal Supplier shall account for all of the following loss terms:
  - (i) non-carbonic acid weathering (Lossacid, rule 6.3.4),
  - (ii) plant uptake of major cations (Lossplant, rule 6.3.5),
  - (iii) losses from surface freshwater systems (Lossrivers, rule 6.3.9), and
  - (iv) losses from marine systems (Lossocean, rule 6.3.10).

# Approach 7 - SICsoil

As discussed in section 1.6, the products of silicate feedstock weathering can re-precipitate in the form of solid carbonates under certain conditions. Such secondary carbonate mineral formation could be viewed as a loss term due to the production of 1 mol  $CO_2$  previously sequestered as bicarbonate as a result of silicate feedstock weathering per mol of formed  $CaCO_3$  (eq. 1.4) as well as the danger of future dissolution of such carbonates by non-carbonic acids, which would release another mol of  $CO_2$  per mol  $CaCO_3$ . However, under the reasonable assumption that soil conducive to producing pedogenic carbonates is unlikely to change its conditions (specifically changing from high pH to low pH) even on long time scales so drastically that carbonates within it start to net-dissolve, secondary (pedogenic) carbonates can be regarded as safely stored carbon ( $C_{\text{stored}}$ ) if they are accounted for as 1 mol  $CO_2$  stored per 1 mol  $CaCO_3$  formed (see eq. 1.4). Additionally, this methodology allows crediting on the basis of secondary carbonate formation only in soils with natural pH levels  $\geq$ 6.5 (see rule 11.3.9 a), where carbonate dissolution by non-carbonic acid weathering is negligible (Dietzen & Rosing, 2023). A small feedstock carbon-content is recommended for detectability of signal increase between  $t_0$  and  $t_1$  when using SIC<sub>soil</sub>.

The main and direct approach for quantifying  $C_{\text{stored}}$  as  $CaCO_3$  is measuring soil inorganic carbon (SIC) concentrations using one of the methods described in table 11.6. Excess SIC resulting from the ERW activity can be estimated by measuring SIC increase over the duration of a monitoring period (i.e., from  $t_0$  until  $t_1$ ) in application sites relative to associated control sites (eqs. 11.47-11.50).

In addition to quantification by SIC measurements, new CaCO<sub>3</sub> formation as a consequence of ERW activity can be validated using isotope measurements. More negative ("lighter") stable isotope signatures of carbon ( $\delta^{13}$ C) and oxygen ( $\delta^{18}$ O) would be expected in CaCO<sub>3</sub> formed from atmospheric CO<sub>2</sub> compared to lithogenic (geological origin) carbonates (Dietzel et al., 1992; Krishnamurthy et al., 2003; Washbourne et al., 2015). Percentage share of lithogenic vs pedogenic carbonates in soil samples can be estimated on the basis of such data following assumptions and methods described by Washbourne et al. (2015). Thus, a statistically significant shift toward higher pedogenic carbonate content (i.e., more negative  $\delta^{13}$ C and  $\delta^{18}$ O values) would clearly validate a formation of secondary

carbonates as a result of the ERW activity. However, in cases where the ERW activity adds secondary carbonate minerals to a background of soil dominated already by pedogenic carbonates, such a shift might not be clearly distinguishable between control and application sites or between  $t_0$  and  $t_1$  within application sites, due to an existing background of low stable isotope signatures. In such cases, the stable isotope approach could still be used to validate the additional carbonates quantified by SIC concentration measurements if it can be demonstrated that the absolute  $\delta^{13}$ C and  $\delta^{18}$ O values are on the low end of the range reported in figure 3 of Washbourne et al. (2015), i.e.,  $\delta^{13}$ C (PDB) <~-20‰ and  $\delta^{18}$ O (PDB) <~-15‰ in both  $t_0$  and  $t_1$  of the application site samples as well as in the control site samples.

Alternatively or in addition to stable isotope analyses, radiocarbon (14C) dating can distinguish modern soil carbonates from lithogenic ones. Due to atmospheric variation in radiocarbon levels, this method can in principle resolve the age of modern soil carbonates with a resolution of decades. This could make it a useful addition to stable isotope measurements in validating that carbonates have been added to soil as a consequence of the ERW activity by demonstrating significant content of modern carbonate in the soil sample (Washbourne et al., 2015). As for the stable isotope approach described above, the effect may only be distinguishable compared to a background of soil dominated by geological carbonate but the combination of the two approaches may still strengthen evidence for validating significant pedogenic carbonate formation.

The CO<sub>2</sub> sequestration is quantified from an increase in soil inorganic carbon (SIC) in units  $g_c/g_{soil}$  over a monitoring period from the time just after feedstock application ( $t_0$ ) to the end of the monitoring period ( $t_1$ ):

$$F5 = \frac{Mw_{CO2}}{Mw_C} \times m \tag{11.47}$$

$$C_{stored} = \Delta SIC_{application} = (SIC_{t1} - SIC_{t0})_{application} \times F1 \times F5$$
 (11.48)

$$C_{baseline-[field]} = \Delta SIC_{control} = (SIC_{t1} - SIC_{t0})_{control} \times F1 \times F5$$
 (11.49)

$$\Delta SIC_{WM} = \Delta SIC_{application} - max(0, \Delta SIC_{control})$$
(11.50)

Note that in eq. 11.50, if the value of  $\Delta SIC_{control}$  is negative, it has to be replaced by zero. The reason is that it is not possible to determine whether this control-site SIC loss was due to carbonate weathering by carbonic acid (implying CDR by bicarbonate formation) or non-carbonic acids (implying CO<sub>2</sub> formation/emissions, eq. 1.4). Therefore, setting  $\Delta SIC_{control} = 0$  is the conservative assumption in this case.

Variable	Description	Unit
Aext	The field area to which weathering feedstock was applied that is represented	
	by the evaluated sample or set of samples, i.e., the area to which the weathering	5
	signal may be extrapolated to, i.e., the area within a homogeneous stratum to	$m^2$
	which weathering feedstock was applied. Note that therefore the value of Aex	t
	will be the same for both Cstored (application sites) and Cbaseline-[field] (control sites)	
$BD_{soil}$	Bulk density of soil (measured).	g <sub>soil</sub> /m <sup>3</sup>

Variable	Description	Unit
d	Sampling depth = the depth the proxy signal is integrated over	m
$Mw_{CO2}$	Molecular weight of CO <sub>2</sub> = 44.01 g/mol	gco2/mol
$Mw_C$	Molecular weight of carbon (12.01 g/mol). Note that if the measurement output (e.g., from calcimetry) provides the concentration of CaCO <sub>3</sub> rather than carbon, the CaCO <sub>3</sub> concentration first needs to be converted to carbon concentration.	gc/mol
m	Stoichiometric factor reflecting the carbon sequestration capacity in mol CO <sub>2</sub> per mol of formed CaCO <sub>3</sub> : $n = 1$ , see eq. 1.4.	unitless
F1	Factor equaling the amount of soil ( $g_{soil}$ ) in the extrapolation area ( $A_{ext}$ ) taking into account the depth over which the sample integrated ( $d$ ); multiplying with this factor therefore extrapolates the weathering signal per gram of soil to the field area this signal represents. See eq. 11.14.	
F5	Factor converting the signal in grams of carbon to a signal in grams of CO <sub>2</sub> .	gc02/gc
$SIC_i$	SIC concentration at $i = t_0$ or $i = t_1$ . Note that SIC <sub>t0</sub> is sampled after feedstock application to correct for any carbonate component contained in the feedstock.	$g_{ m c}$ / $g_{ m soil}$
$\Delta SIC_{application}$	Gross amount of carbon dioxide stored as carbonate mineral as measured as SIC concentration increase within the NFZ of application sites (weathering signal).	
$\Delta SIC_{control}$	Amount of carbon dioxide stored as carbonate mineral on control sites as measured as SIC concentration increase within the NFZ of control sites, representing the baseline carbonate mineral formation that would have occurred also on application sites in the absence of the ERW activity.	
∆SIC <sub>WM</sub>	Baseline-corrected increase in precipitated carbonate minerals (measured as SIC) during the monitoring period as quantified by the SICwm approach and converted to amount of CO <sub>2</sub> removed.	

Given that the measurement directly reflects the sequestered carbon from CO<sub>2</sub>, no NFZ loss terms apply to this quantification type and given that the storage site for the carbonate minerals quantified by SIC<sub>soil</sub> is the soil rather than the ocean, the FFZ loss terms Loss<sub>rivers</sub> and Loss<sub>rivers</sub> do not need to be accounted for either.

- 11.3.9 The CO<sub>2</sub> Removal Supplier may use the SIC<sub>soil</sub> approach, i.e., using SIC concentration measurements to quantify C<sub>stored</sub> as CaCO<sub>3</sub> within the NFZ according to eqs. 11.14 and 11.47-11.50 under the conditions described in subrules a-j:
  - (a) **Sample type:** Samples for CAT<sub>WM</sub> analysis shall be obtained using an appropriate soil sampling technique and equipment.
  - (b) **Soil pH eligibility:** SIC<sub>soil</sub> shall only be eligible in soils with mean pH levels of at least pH 6.5 (Dietzen & Rosing, 2023) prior to the first feedstock application of a given Crediting Period (on a homogeneous-stratum level and as determined by pre-application soil characterization, see rule 9.3.5).

- (c) **Sampling depth:** The SIC<sub>soil</sub> analysis shall quantify the cation content in the entire soil sample core between the soil surface and the NFZ depth.
- (d) **Analytical measurements:** eligible SIC concentration measurements include:
  - (i) calcimetry (ISO 10693:1995), or
  - (ii) dry combustion (ISO 10694:1995).
- (e) **Significant signal**: Significantly elevated SIC concentrations shall only be interpreted as a signal for C<sub>stored</sub> as CaCO<sub>3</sub> and used as the basis for its quantification if the following conditions are met:
  - (i) SIC increase between  $t_0$  and  $t_1$  measured in application site samples is both statistically significant and larger than any such increase measured in corresponding control site samples.
  - (ii) Successful validation by an isotope-based approach (subrules g-h).
- (f) *t*<sub>0</sub> **measurements**: Time point *t*<sub>0</sub> samples shall be collected after feedstock application. This ensures that the subtraction of SIC<sub>t0</sub> from SIC<sub>t1</sub> inherently corrects for any carbonates contained in the carbonate feedstock added to the application sites.
- (g) **Validation:** In order to validate the interpretation of C<sub>stored</sub> as CaCO<sub>3</sub> on the basis of SIC concentration measurements (subrules d-f), the CO<sub>2</sub> Removal Supplier shall additionally use measurements of carbon and oxygen stable isotopes in carbonates from a subset of representative soil samples to demonstrate the atmospheric carbon content of the additionally formed carbonates. This validation shall be fulfilled by demonstrating a statistically significant shift toward more negative  $\delta^{13}$ C and  $\delta^{18}$ O values between  $t_0$  and  $t_1$  on application sites that is also statistically significantly larger than any such shifts observed at corresponding control sites. Conceptually, such a shift will occur from the specific  $\delta^{13}$ C and  $\delta^{18}$ O values found in the soil after feedstock application ( $t_0$ ) toward the conceptual end members at  $\delta^{13}$ C (PDB) <~-20‰ and  $\delta^{18}$ O (PDB) <~-15‰ (Washbourne et al., 2015).
- (h) **Alternative validation approach:** Alternatively or in addition to stable isotope measurements, the CO<sub>2</sub> Removal Supplier may use radiocarbon (<sup>14</sup>C) analyses from a subset of representative soil samples to validate the signal for C<sub>stored</sub> as CaCO<sub>3</sub> by determining the age of the soil inorganic carbon. Significantly reduced soil carbonate age between application site *t*<sub>0</sub> and *t*<sub>1</sub> samples that is also statistically significantly larger than any such age decrease observed in corresponding control sites may validate C<sub>stored</sub> as CaCO<sub>3</sub> quantified as per subrule e.

- (i) **Approach combination:** If the C<sub>stored</sub> as CaCO<sub>3</sub> can be properly quantified and validated in accordance with subrules a-h, this C<sub>stored</sub> value may be added to the CORC quantification either independently (as the only way of quantifying C<sub>stored</sub> during a given monitoring period) or in addition to C<sub>stored</sub> quantified on the basis of one of the other eligible approaches (rule 11.3.1) as long as subrule j is followed.
- (j) Correction of NFZ-exported carbon: If C<sub>stored</sub> as bicarbonate, alkalinity, or cations exported from the NFZ (i.e., via one of the other eligible quantification approaches in table 11.6) is quantified either in the same monitoring period or in a monitoring period after C<sub>stored</sub> is quantified as CaCO<sub>3</sub>, SIC concentrations shall be measured in parallel to each measurement quantifying C<sub>stored</sub> as bicarbonate/alkalinity/cations exported from the NFZ. C<sub>stored</sub> measured as bicarbonate/alkalinity/cation export from the NFZ must be corrected for (i.e., discounted by) any decrease in SIC observed between measurement time points. For example, for 1 mol of SIC decrease between two measurement time points, C<sub>stored</sub> (from bicarbonate/cation export) needs to be corrected for (i.e., decreased by) 1 mol bicarbonate or 1 charge-equivalent cation or alkalinity.

# 12 ERW simulation models

#### 12.1 Guidelines for ERW models

Enhanced Rock Weathering is an inherently slow process that can have a project duration of several years or decades and quantification of the term  $C_{stored}$  is associated with large uncertainties. The combination of models<sup>118</sup> and measurements could provide a pathway to decrease these uncertainties without increasing the sampling density. Therefore, this methodology encourages CO<sub>2</sub> Removal Suppliers to undertake site-specific modeling of their ERW activity in addition to quantification by experimental monitoring. Such efforts can serve extrapolation of C<sub>stored</sub> quantified by measurements to reduce the necessary sampling density.

Modeling ERW implies the accounting for a wide range of geochemical, physical, and biological parameters and processes. Various modeling approaches of different types have been suggested in the literature (table 12.1) but to date (Oct 2025), no scientific consensus exists on the best approach to simulate the enhanced weathering process (Kanzaki et al., 2025). As different models can vary significantly with respect to the data required, inputs, outputs, and theoretical approaches, one purpose of this section is to set guidelines to steer the simulation process towards reliable results. It is important to note that this section 12 discusses process-based models simulating relevant (bio)geochemical, hydrological, physical, and biological processes of ERW in the soil, as opposed to statistical models, process-based models simulating carbon losses in the FFZ (surface-waters and the ocean, see section 6.2), or simple sets of calculations. Thus, the output of these models pertains mostly to C<sub>stored</sub>, and some models may also have the capacity to quantify NFZ based losses (C<sub>loss</sub>), i.e., Loss<sub>acid</sub>, Loss<sub>plant</sub>, Loss<sub>adsorb</sub>, and/or Loss<sub>silicate</sub>.

Table 12.1 provides an overview of available models for ERW that are published as part of peer-reviewed studies. At this time, SCEPTER, SMEW, and KELLAND may be seen as among the more widely used models. Differences between these models could provide reasons to prefer one over the other depending on specific conditions. SCEPTER and KELLAND are one-dimensional (1D) reactive-transport models, simulating geochemical, biological, and physical processes across a vertical gradient as well as time. By contrast, the coupled ecohydrology-biogeochemistry model SMEW has no depth dimension, assuming that all relevant processes occur in a well-mixed upper soil layer (Bertagni et al., 2024; Cipolla et al., 2021a, 2021b) but it features a dynamic soil moisture regime that captures cation accumulation and flushing dynamics relevant to validate against monitoring measurements. SCEPTER (unlike KELLAND) contains functions that simulate tillage and other types of soil mixing. It can also trace soil organic matter and integrate climatic variables (temperature, water). However, the current version 1.0 of SCEPTER (Kanzaki et al., 2024) can

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<sup>&</sup>lt;sup>118</sup> In this methodology the words 'model', 'simulation', etc. are to be understood in a wide sense including not only the equations and/or computer programs they are composed of, but also the subsequent data analysis and interpretation of the results by experts.

simulate neither plant uptake of cations and nutrients nor secretion of organics, whereas the other two models can simulate biologically mediated cation and carbon fluxes. Finally, the KELLAND model seems best equipped among the three to simulate the effect of nitrogen fertilizers on ERW.

An ERW model usually provides several outputs from which an estimate of the amount of carbon stored is determined. Simulated estimates require validation via in-situ measurements to determine the accuracy of the simulation in predicting weathering behavior over time. Model validation is based on comparing the measurements of a weathering signal and the result predicted by the simulation, and depending on specifics of the selected approach, several different quantities can be measured for validation purposes (see section 11.2).

**MODELLING PROCESS:** Modeling CO<sub>2</sub> removal from an ERW activity requires expertise in accounting for a wide range of geochemical, physical, and biological parameters and processes. While the precise workflow associated with modelling can differ based on the computational model utilized as well as the implementation details of the ERW activity itself, the general steps can be coarsely outlined as follows.

- Model construction: constructing a site-specific ERW model requires significant effort. It includes defining in detail the biogeochemical processes involved and how these are simulated, as well as a detailed specification of all the necessary input and output parameters, rate constants, and other details of the model. This step (and also subsequent modelling process steps) further requires various checks on the robustness and sensitivity of the model to ensure that it is performing as intended (see also rule 12.2.10).
- Model input and calibration: a given ERW model is likely to contain a significant number of input parameters that describe the various biogeochemical processes included. While some parameters can be straightforwardly determined from empirical measurements (e.g. soil pH, chemical composition of the feedstock), others (e.g., reaction rates in field conditions, etc.) may need to be approximated and constrained based on information from the scientific literature. Therefore, it is usually also necessary to calibrate (i.e. fit or tune) such parameters in order to obtain model outputs that reflect empirical observations from the site. Data from pre-application soil analysis, previous monitoring periods on the same homogeneous stratum, or even the current monitoring period on the same stratum may be used for this, as long as the (sub)set of data does not overlap with the data used for model validation (see rule 12.2.6 g).
- Model run: the calibrated model is run on site-specific input data to predict the behavior of the chemical weathering reactions, transport of weathering products and other relevant processes. The outputs of the model can include e.g. the (dynamic) concentrations of weathering products moving in and through the soil column, from which the associated CO<sub>2</sub> removal can be determined.
- Model output validation: the outputs of the model must include directly experimentally verifiable weathering signals, and outputs from the model must be validated against site-specific data from the same monitoring period and homogeneous stratum, see rule 12.2.6.

**Table 12.1**. Examples of published models for quantifying CDR in Enhanced Rock Weathering.

Model name/ reference	Model type	Simulated processes
Kelland (Kelland et al., 2020; A. L. Lewis et al., 2021; Vienne et al., 2022)	PHREEQC- based 1D reactive transport model	<ul> <li>Vertical fluid and dissolved ion transport through soil column</li> <li>Silicate mineral weathering rates: mineral dissolution and (secondary) precipitation</li> <li>CO<sub>2</sub> equilibration and carbonate chemistry</li> <li>Effect of nitrogen fertilizers</li> <li>Effect of respiration and plant uptake on cation and carbon balance</li> <li>Cation sorption/exchange</li> </ul>
SMEW (Bertagni et al., 2024; Cipolla et al., 2021a, 2021b)	Coupled ecohydrology- biogeochemistry model	<ul> <li>Soil moisture dynamics (informed by rainfall, evaporation, and transpiration, leakage)</li> <li>Silicate mineral weathering rates: mineral dissolution and (secondary) precipitation</li> <li>CO<sub>2</sub> equilibration and carbonate chemistry</li> <li>Biological (degradation, respiration, plant uptake) carbon cycling</li> <li>Dissolved mineral (silicate, cation) fluxes</li> <li>Cation sorption/exchange</li> </ul>
SCEPTER (Kanzaki et al., 2022; Baek et al., 2023; Kanzaki et al., 2024)	1D reactive transport model	<ul> <li>Vertical fluid and dissolved ion transport through soil column</li> <li>Silicate mineral weathering rates: mineral dissolution and (secondary) precipitation</li> <li>CO<sub>2</sub> equilibration and carbonate chemistry</li> <li>Soil mixing (by organisms or tillage)</li> <li>Grain-size driven changes in feedstock surface area as weathering proceeds</li> <li>CO<sub>2</sub> introduction into the soil profile through gas phase transport and organic carbon respiration</li> <li>Cation sorption/exchange</li> </ul>
TOUGHREACT (Deng et al., 2023; Xu et al., 2011)	1D reactive transport model based on THOUGHREACT	<ul> <li>Vertical fluid and dissolved ion transport through soil column</li> <li>Silicate mineral weathering</li> <li>Microbial degradation of organic matter</li> <li>Cation exchange</li> <li>Kinetic mineral reactions</li> </ul>
(Beerling et al., 2020)	1D reactive transport model	<ul> <li>Vertical fluid and dissolved ion transport through soil column</li> <li>Silicate mineral weathering</li> <li>Carbonate speciation including secondary carbonate formation</li> <li>Influence of crop productivity</li> </ul>
(Kantzas et al., 2022)	1D reactive transport model coupled to climate model	<ul> <li>Vertical fluid and dissolved ion transport through soil column</li> <li>Silicate mineral weathering</li> <li>Effect of nitrogen fertilizer application</li> <li>(effects of different climate scenarios)</li> </ul>

## 12.2 Requirements for process-based ERW models

- 12.2.1 The CO<sub>2</sub> Removal Supplier may use process-based models to simulate the ERW process as an additional means to quantifying C<sub>stored</sub>. Results from such models may be used for site-specific extrapolation (see rule 12.2.7) of data from empirical measurements using a quantification method (rule 11.3.1), provided that rules 12.2.2–12.2.12 are met.<sup>119</sup>
- 12.2.2 **Eligible model types** for process-based simulation of the ERW process and quantification of C<sub>stored</sub> shall have the following attributes:
  - (a) Based on peer-reviewed models that are based on commonly accepted scientific concepts and theoretical background;
  - (b) The model shall be specifically designed for soil science applications suitable for quantifying CDR based on ERW (including but not limited to those in table 12.1);
  - (c) The parameterization (e.g. solubility, kinetic and thermodynamic data) shall be based on measurements reflecting conditions relevant to in-field applications as much as possible;
  - (d) The modeling approach shall be based on data-driven mechanistic functions (i.e., process-based) that take into account the relevant physico-biogeochemical processes of ERW (i.e., interactions between mineral, soil, biological organism, water, atmosphere, and meteorological drivers) rather than based fully on statistical predictions of empirical data;
  - (e) Non-eligible models in this context of quantifying C<sub>stored</sub> include entirely statistical models, models that do not take into account the specific biogeochemical processes of weathering, and simplistic models (e.g., restricted to first-order kinetics, collection of budget-type equations, etc.);
  - (f) While the choice is not restricted to them, the models described as KELLAND, SMEW, and SCEPTER models above and in table 12.1 provide examples of generally eligible model types.

<sup>&</sup>lt;sup>119</sup> Note that while all CO<sub>2</sub> Removal Suppliers shall respect the minimum sampling requirements (see section 11.2), utilization of calibrated and validated site-specific ERW models may allow a CO<sub>2</sub> Removal Supplier to reach a desired level of accuracy and precision with fewer overall measurements than would otherwise be necessary. Note further that while modelling introduces an additional uncertainty component, and hence decreases the amount of credits by increasing the factor of conservativeness defined in rule 10.5.3, this is balanced against the smaller costs of modelling compared to field measurements.

- 12.2.3 **Input and project specificity:** the input data for the model shall be based on site- and project-specific parameters from empirical measurements, including soil-physical and biogeochemical properties (e.g., those listed in table 9.2) of the relevant homogeneous stratum (see rule 12.2.6), properties of the utilized feedstock rock (e.g., mineralogical composition, specific surface area, particle size distribution, see rule 3.6.2), and the local climate (e.g., rainfall, air temperature). As new data become available on these parameters (e.g., based on results of the in-field monitoring and measurement activities conducted by the CO<sub>2</sub> Removal Supplier), the model shall be updated at the next appropriate juncture, e.g., for the next monitoring period. Site- and project specific data may be supplemented as necessary by values obtained from peer-reviewed scientific literature or relevant scientific datasets (e.g., soil maps, data from meteorological stations, reaction constants, enthalpies, activation energies, rainwater chemistry, etc.).
- 12.2.4 **Modelled phenomena**: the model shall at least simulate the following aspects of ERW:
  - (a) The most relevant biogeochemical processes occurring in the system, (including feedstock mineral dissolution and secondary mineral precipitation, CO<sub>2</sub> equilibration and carbonate chemistry, cation sorption and exchange, biological respiration), which shall be modeled on the basis of scientifically relevant thermodynamic and kinetic coefficients related to the reactions and include:
    - (i) Feedstock weathering (mineral dissolution), including the effects of the physical size of the mineral particles being spread (e.g. grain size, surface area, roughness, and changes to particle size due to mineral dissolution);
    - (ii) Secondary mineral precipitation;
    - (iii)CO<sub>2</sub> equilibration and carbonate chemistry;
    - (iv) Cation sorption and exchange;
    - (v) Biological respiration or, alternatively for models performing poorly in simulating respiration, imposition of a conservative (within a realistic range) soil pCO<sub>2</sub> level represented by a constant.
  - (b) The influence of key environmental parameters (e.g., moisture, pH, temperature, ion concentrations, etc.) on the modeled biogeochemical processes;
  - (c) Soil moisture dynamics and/or the transport of fluids and chemical species through the soil system.

Additionally, the model *should* simulate the following aspects of ERW:

- (d) Secondary effects affecting the dissolution of grains such as surface passivation effects;
- (e) Soil disturbances, e.g., due to tillage or bioturbation;

- (f) Plant cation uptake;
- (g) Non-carbonic acid weathering and the effect of (nitrogen) fertilizer;
- (h) Grain-size driven changes in feedstock surface area as weathering proceeds;
- (i) Soil organic carbon stocks.
- Model output: The site-specific process-based model shall provide at least an estimation of the expected weathering and the associated CO<sub>2</sub> removal (in tCO<sub>2</sub>e) as a function of time (i.e. year-to-year) over the monitoring period and the duration of the project (project time horizon). The model should also be able to output other supporting data, such as concentrations of the relevant chemical species, element mass transfer rates, weathering rates, soil organic carbon dynamics, rates of losses to plants, secondary mineral formation, cation adsorption, and non-carbonic acid weathering, etc. Provided that loss terms are modeled appropriately, the modeling output may be used to account for NFZ loss terms (in the term Closs of the CORC equation, eq. 5.1) for the areas covered by model extrapolation of empirical measurements.
- 12.2.6 **Model output validation**: In order to validate the model output, all of the following requirements shall be met:
  - (a) The simulation approach shall be transparent, and at least the core components should be publicly available;
  - (b) The CO<sub>2</sub> Removal Supplier shall provide a standard validation plan that includes an explicit timeframe for the detectability of the empirical validation technique and a plan for mitigating uncertainty due to spatial and temporal variability;
  - (c) The model shall be able to predict directly experimentally verifiable weathering signals such as pH, dissolved inorganic carbon, or major cation concentrations;
  - (d) The model shall be validated against data measured in-field within the same homogeneous stratum in accordance with the minimum sampling requirements defined in section 11.2 (see especially rule 11.2.7 and the associated tables 11.2-11.5);
  - (e) The model validation process shall include the explicit comparison of modelled values to empirically measured values (see subrules c and d), and the quantification of the difference between modelled and measured values in terms of a root mean square error evaluation or other goodness-of-fit-indicators suitable to evaluate the accuracy the model.

- (f) The CO<sub>2</sub> Removal Supplier shall utilize the outcome of the quantification of the difference between modelled and measured values (see subrule e) in the quantification of the total uncertainty associated with the model's outputs (see rule 12.2.8).
- (g) Data utilized for the purpose of calibrating the model<sup>120</sup> shall not be utilized for validation.
- 12.2.7 **Extrapolation:** Models validated with site-specific empirical data may be used for spatial and temporal extrapolation with the following constraints:
  - (a) Spatial extrapolation: models may be used to extrapolate across a single homogeneous stratum based on measurements taken in the evaluation area of that stratum. This implies that sampling in the non-evaluation portion of the application site may be replaced by extrapolation of evaluation-area measurements with an appropriate model.
  - (b) Temporal extrapolation (seasonal): models may be used to extrapolate across seasonal time frames only to the extent that they have been calibrated and validated with empirical data reflecting those seasonal differences (for example, a model calibrated with measurements conducted in the summer alone shall not be utilized for temporal extrapolation from summer to winter).
  - (c) Temporal extrapolation (inter-annual): models may be used to extrapolate from one year to the next but not across multiple years, i.e., model validation underlying the simulation of a given year shall be done on site-specific data that were taken no earlier than the previous year.
- 12.2.8 **Uncertainty**: the model shall quantify the uncertainty associated with its outputs (see section 10.5).
  - (a) The uncertainty assessment shall include quantification of uncertainties arising from the simulation itself (e.g. random errors due to inaccurate input parameters) as well as the treatment of modeled phenomena (e.g. biases inherent to the model, assessed through the comparison of measured and modeled values, see rule 12.2.6 f). See also rule 10.5.6 b.<sup>121</sup>

<sup>&</sup>lt;sup>120</sup> For the purposes of this methodology, calibrating an ERW model refers to the process of fitting or otherwise tuning or training one or several model inputs or parameters for the purpose of adapting the model to site-specific characteristics (e.g. local soil properties), particularly in cases where the direct experimental evaluation of the parameters in relevant field conditions is impossible or unfeasible (e.g. reaction rate constants).

<sup>&</sup>lt;sup>121</sup> Note that as explained in further detail in rule 10.5.6 b, uncertainty in ERW models can stem from various sources including inaccurate input parameters as well as the implementation of the model (e.g. simplifications and/or omissions

- (b) If models are used to contribute to the quantification of CORCs, the associated modelling uncertainty shall be included in the evaluation of the total uncertainty of the net CO<sub>2</sub> removal activity (i.e.  $u_c(CORC)$ ), see rule 10.5.3).
- 12.2.9 Statement and justification of model choice and assumptions:
  - (a) The CO<sub>2</sub> Removal Supplier shall provide justification for the selection of the process-based models used, including its spatial and temporal resolution, key physical parameters, and all assumptions applied in simulating relevant dynamics. This justification shall be subject to review and approval by an independent third party as part of the Production Facility Audit.
  - (b) The CO<sub>2</sub> Removal Supplier shall describe and justify all assumptions made within the simulation, defining the conditions under which each assumption is considered valid.
  - (c) All assumptions and references shall be included in the Monitoring Plan.
  - (d) All external references, including data sources, models, and supporting literature, shall be cited and their relevance to the simulation and project context thoroughly explained.
  - (e) All external references used in the simulation shall be clearly indicated and explained.
- 12.2.10 **Model inspection**: To establish that the model is internally robust and performing as intended, the CO<sub>2</sub> Removal Supplier shall perform and report the results of at least the following model inspections:<sup>122</sup>
  - (a) Sensitivity analyses of model performance covering ranges of uncertainty of important parameters (e.g., initial feedstock reactive surface area, kinetic coefficients, precipitation, etc.).
  - (b) Checks on internal robustness (e.g., butterfly effects, numerical instabilities).
  - (c) Sanity checks (including, but not limited to, ensuring that the simulated C<sub>stored</sub> does not exceed the theoretical maximum capacity for CO<sub>2</sub> removal given applied feedstock amounts, see rule 9.4.2).

in the modeled phenomena). For a robust quantification of uncertainty, all these sources need to be appropriately considered.

<sup>&</sup>lt;sup>122</sup> A careful inspection of model sensitivity and robustness by the CO<sub>2</sub> Removal Supplier can improve accuracy and reduce uncertainty, identify errors and nonsensical outputs, and recognize critical parameters or processes requiring particular attention.

- 12.2.11 **Model publication and availability**: The model code should be open source (i.e., any computer code and datasets comprising the model should, to the extent possible, be publicly available in data repositories).
- 12.2.12 **Timeline:** The model shall be completed by the time of the Production Facility Audit.
  - (a) Complete site-specific model validation data shall be provided by the time of the Output Audit.
  - (b) Prior to the Output Audit (if not combined with Facility Audit) and for the purpose of demonstrating eligibility and effectiveness of the model, preliminary model validation results may be used, such as an extrapolation based on experimentally determined weathering rates from measurements conducted in a relevant setting (e.g., from a previous pilot project).

## 13 Reporting Requirements

- 13.1.1 The CO<sub>2</sub> Removal Supplier shall prepare and make available an Output Report to provide evidence of the Production Facility performance for the monitoring period covering the scope of monitoring as described in rule 9.2.1 and demonstrates conformity of the Enhanced Rock Weathering activity with the requirements of this methodology, as well as the Puro Standard General Rules<sup>123</sup> and other Standard Requirements.<sup>124</sup>
- 13.1.2 The Output Report shall include supporting documented evidence for each monitoring period described in the Monitoring Plan, in accordance with ISO 14064-2:2019, clause 6.13 "Reporting the GHG project". 125
- 13.1.3 The Output Report shall include, as a minimum:
  - (a) The name of the CO<sub>2</sub> Removal Supplier and operational partners.
  - (b) A brief description of the Production Facility, including size, location, crediting period, type of carbon removal activity, and Puro-approved Methodology version being followed.
  - (c) The date of the report and the time covered by it (monitoring period).
  - (d) A CORC Summary with supporting detailed GHG calculations and evidence. The GHG emission reductions and removals are stated in tonnes of CO<sub>2</sub>e. The detailed information may be redacted to protect sensitive commercial information and comply with data providers' end-user license agreements.
  - (e) If applicable, a description of the GHG baseline and demonstration that the GHG emission removals are not over-estimated.
  - (f) The combined percentage uncertainty of measurement of the CORCs issued in the CORC Summary statement.
  - (g) As applicable, an assessment of permanence including any reversal event.

<sup>&</sup>lt;sup>123</sup> Available in the Puro Standard documents library.

<sup>124</sup> Ibid.

<sup>125</sup> ISO 14064-2:2019 Greenhouse gases, Part 2: Specification with guidance at the project level for quantification, monitoring and reporting of greenhouse gas emissions reductions or removal enhancements.

- (h) If required by the CO<sub>2</sub> Removal Supplier, changes to the Production Facility and Monitoring Plan shall be clearly stated, and evidence of conformity with Puro General Rules<sup>126</sup>, the requirements set in this methodology, and other Puro Standard<sup>127</sup> requirements shall be provided for validation by the third-party Validation and Verification Body.
- 13.1.4 Delays or changes in the reporting frequency shall be in conformity with Puro Standard General Rules.<sup>128</sup>
- 13.1.5 The CO<sub>2</sub> Removal Supplier shall have in place, maintain, and utilize an information system to keep records of all monitoring activities associated with the Enhanced Rock Weathering activity (see rule 5.2.8). In addition:
  - (a) These records shall include information on the parameter or process monitored (i.e. what was monitored and how), as well as results of any measurements performed.<sup>129</sup>
  - (b) The information shall be time-stamped and quantitative (where applicable).
  - (c) These records shall be available to the Auditor, for the Production Facility Audit and Output Audits.
  - (d) These records shall be kept for at least two years after the end of the crediting period or the last issuance of CORCs for this project activity, whatever occurs later.
- 13.1.6 Data derived from the ERW activity should be made available to the public, e.g., by data submission to public repositories.

 $<sup>^{\</sup>rm 126}$  Available in the Puro Standard documents library.

<sup>&</sup>lt;sup>127</sup> Ibid.

<sup>&</sup>lt;sup>128</sup> Available in the Puro Standard documents library.

<sup>&</sup>lt;sup>129</sup> Note also rule 5.2.8 on keeping records of events that affect the quantification of CORCs. Note that these records are at least partly separate, as not all monitoring activities or results thereof necessarily affect the number of CORCs.

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